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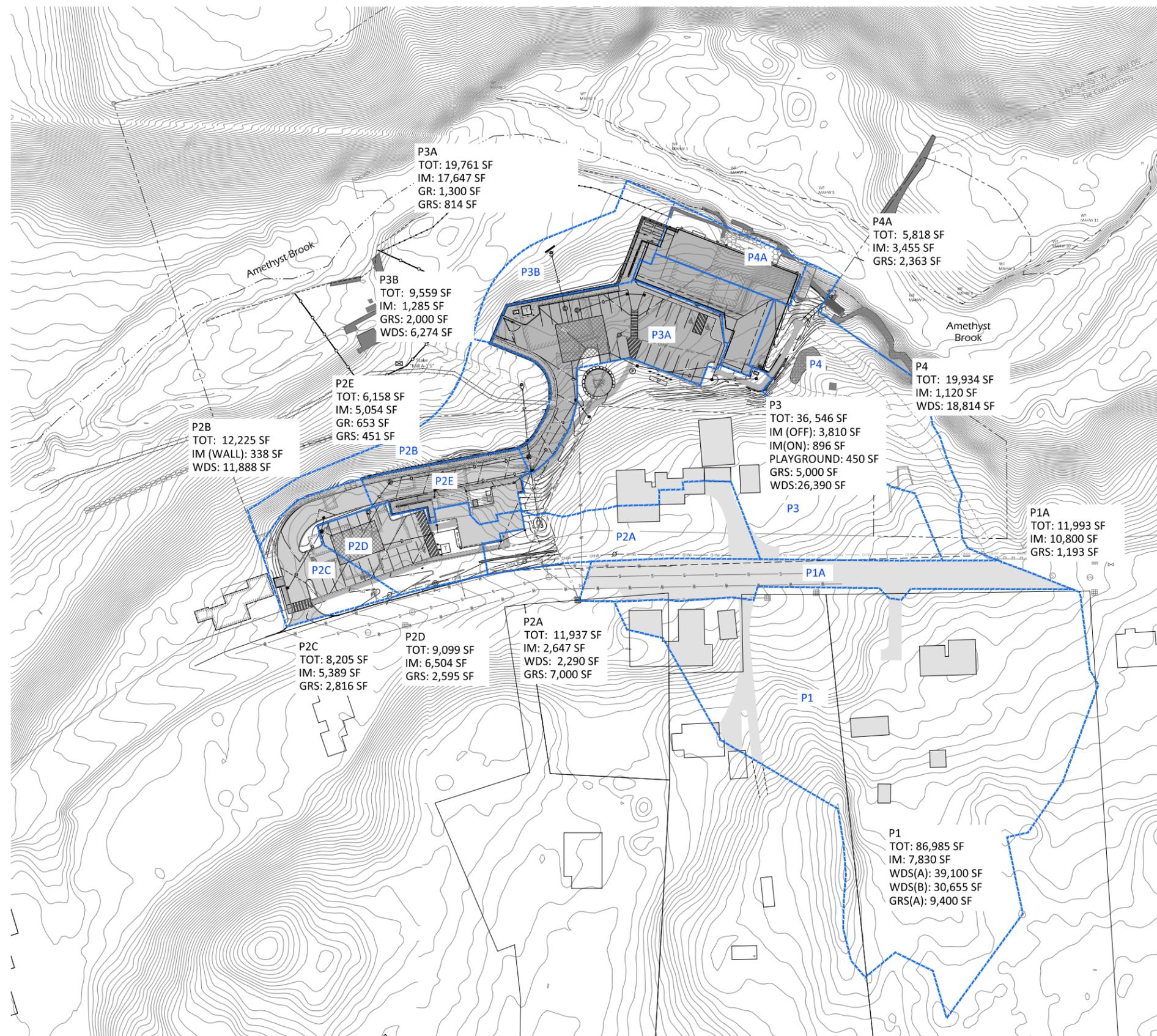
AMETHYST BROOK APARTMENTS
20-22 AMHERST ROAD
PELHAM, MA

PROPOSED DRAINAGE

Revisions

Date: December 11, 2020
Scale: 1"=100'
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Sheet Number
FIG 6



E:\PELHAM - 22 AMHERST ROAD\DESIGN PROCESS\ENGINEERING\DRAWINGS\22 PELHAM ROAD PROP. CONDITIONS REV.DWG PLOT DATE: 12/21/2020

Stormwater Management Report

**For
Amethyst Brook Apartments
20-22 Amherst Road
Pelham, MA**

December 21, 2020

Prepared by:



**Berkshire
Design
Group**

4 Allen Place, Northampton, Massachusetts 01060

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Plans:

20-22 Amherst Road, Pelham - Permit Set

Home City Development Inc. is proposing to create new residential housing units at 20-22 Amherst Road, Pelham, Massachusetts. The new units will be created through demolition and replacement of the existing farmhouse at 20 Amherst Street with a similar building and the demolition and replacement of the commercial building at 22 Amherst Road with a new three-story, multi-unit building. The existing driveways and parking areas will be reconfigured as part of the project.

Berkshire Design Group has prepared a Stormwater Management plan for the site in compliance with the Massachusetts Stormwater Handbook. This report summarizes the design of the system and documents how the design complies with those standards.

I. Introduction

The project includes two properties which will be redeveloped into multi-family housing. The property at 20 Amherst road includes a single-family home and barn as well as a large collapsed wood shed, gravel drive and garage. The 8.73-acre 22 Amherst Road property is comprised of a commercial building, garage buildings, parking and access driveway.

The single-family home at #20 Amherst road will be demolished and replaced with a new building comprised of 6 new residential units. The new building will be located on the eastern side of the lot and a parking area will be constructed at the location of the existing building. The existing barn, sheds and detached garage will be demolished. At 22 Amherst Road, all existing structures will be demolished and replaced with a new 3-story apartment building. A new access drive and parking lots will replace the existing. New utility services and stormwater improvements are also proposed.

The parcels are located on the north side of Amherst Road between Harkness Road and North Valley Road. The project location is shown in Figure 1. The project is situated on a steep hillside between Amherst Road and Amethyst Brook. The existing home at #20 Amherst Road occupies the higher portion of the lot adjacent to Amherst Road while the re-development at #22 Amherst Road is located at the base of the steep hillside above Amethyst Brook.

Soil Data

NRCS Soil Survey

The NRCS Soil Survey reports that the on-site soils consist of Hinckley loamy sand, hydrologic soil groups (HSG) A. The USGS Surficial Geology survey indicates that the parcel is located in thin till overlaid by alluvial fan deposits near the brook and coarse deposits near Amherst Road. The NRCS Soil Report for the site is attached in **Appendix A**.

Subsurface Exploration

A total of four test pits were completed at the Amherst Road site on December 1, 2020. The soil evaluation report is attached as **Appendix B**. The test pits indicated that the soils included deep gravelly and stony coarse sandy soils. Estimated seasonal high groundwater (ESHG) within test pits 1-3 at #20 Amherst Road was not observed and was therefore estimated as deeper than the test pit depths which varied from 6.7' to 9' from the surface. At #22, in Test Pit #4 estimated high groundwater was observed at 4.8 ft below the surface. For purposes of infiltration, A soils with a Rawls rate of 2.41 in/hour were assumed. The design of the underground storage and infiltration systems incorporated two feet of separation from ESHG from the test pit data. Since there was no indication of ESHG at #20, more than 2' above the deepest test pit elevation was used for design.

Site Limits

Site limits were based both on the parcel lines and redevelopment areas as well as the contributing drainage area to the south. Since runoff generally flows north towards Amethyst brook as sheet, shallow concentrated and channel flow, a study boundary was established on the north side of the project site to model pre and post peak runoff (see Figures 4 and 6).

II. Existing Conditions

An Existing Conditions Plan is shown on **Figure 2**. NRCS soils throughout the study area are shown on **Figure 3**. Existing hydrology which includes a significant area off-site is shown on **Figure 4**.

The existing hydrology was analyzed as four major drainage areas, E1 through E4, each including impervious areas, open space and wooded areas.

Drainage area E1 includes the area south of Amherst road which is conveyed through the proposed site. This area is comprised of approximately 400' of roadway, and several driveways, homes, garages and sheds located above the road on the hillside. The roadway area and contiguous impervious areas are modeled as a separate drainage sub-area (E1A) since this area will runoff quickly into the drainage system and create a peak runoff separate from the runoff from the hillside. Area E1 is tributary to an existing on-site swale which drains to a side channel of Amethyst Brook.

Drainage area E2 includes the western portion of the study area, the existing home at #20 Amherst road, barns, sheds and garage as well as a portion of the driveway to #22 Amherst Road access driveway and a portion of the #24 Amherst Road property and impervious area. This area is tributary to an existing drainage swale which drains to a side channel of Amethyst Brook.

Drainage area E3 includes the central portion of the study area. This area is modeled as three sub-areas to reflect existing conditions. Sub-area E3 includes a portion of #24 Amherst Road house, barn and garage roofs and the adjacent property to the north and east which sheet flows north toward the brook. Sub-area E3A is modeled separately because the large impervious area in this area will create an early peak flow. Sub-area E3B is also modeled separately because the garage roof appears to have a separate drainage system which outflows to the terrace below the garage.

Drainage area E4 includes the eastern portion of the study area. Again, this area is modeled as the uphill mostly pervious area (E4) and sub-area E4A, the portion of the factory roof, deck and courtyards which drain directly to the brook.

III. Proposed Conditions

The proposed conditions plan is provided on **Figure 5** and the proposed hydrology is shown on **Figure 6**. The proposed work maintains existing stormwater flow patterns and includes improvements to the existing drainage system off of Amherst Road, two underground storage systems for peak flow attenuation and recharge and hydrodynamic separators for TSS removal.

The proposed site is modeled with four drainage areas matching the patterns found in existing conditions.

In proposed conditions, off-site drainage areas E1 and E1A are unchanged. These areas are labeled P1 and P1A. As in existing conditions, these areas are tributary to an existing on-site swale which drains to a side channel of Amethyst Brook.

Area P2 includes the western portion of the study area and is modeled as five sub-areas to reflect the proposed development and stormwater improvements. As in existing conditions, most of area P2 is tributary to an existing drainage swale which drains to a side channel of Amethyst Brook. Sub-area P2A includes a portion of the house at #24 Amherst Road which drains west to the existing drainage system and sub-area P2B is the largely unchanged area below the proposed common drive. Sub-area P2C (the first 170 feet of the entrance drive) and sub-area P2D (the parking lot and front #20 roof) are conveyed to a stormwater detention/infiltration facility located under the parking lot. Finally, since sub-area P2E (140 feet of driveway and rear #20 roof) is down gradient of the stormwater facility in the upper parking lot, it is conveyed to the stormwater detention/infiltration facility located in the lower parking lot.

Drainage area P3 includes the central portion of the study area and is modeled as three sub-areas similarly to existing conditions. Sub-area P3 includes a portion of the house at #24 Amherst Road, barn and garage roofs and the adjacent property to the north and east which sheet flows north toward the brook. Sub-area P3A encompasses the driveway to #22, the parking area and the south side of the #22 roof. This area is directed to a stormwater detention/infiltration facility located under the lower parking area. The detention facility outflows to an existing outflow above Amethyst Brook. Sub-area P3B is the lower part of this drainage area and includes undeveloped areas and the western portion of the #22 building improvements. Stormwater runoff sheet flows off his area to Amethyst Brook.

Drainage area P4 includes the eastern portion of the study area. As in existing conditions, this area is modeled as the uphill mostly pervious area (P4) and sub-area P4A, a portion of the new apartment roof. The apartment roof includes several disconnected downspouts which will discharge north towards Amethyst brook.

Water Quality

Existing impervious areas at the site includes 27,430 sf of roofs, driveways and aprons and 1,201 sf of gravel driveways for a total of 28,640 sf of impervious areas. The proposed redevelopment includes 42,840 sf of building roofs, driveways, parking lots and walkways, an increase of 13,200 sf.

The proposed design provides treatment for impervious area by directing driveways and parking lots to hydrodynamic separators. Runoff from portions of roofs and walkways and other areas which cannot be captured and conveyed to the hydrodynamic separators are conveyed through disconnected downspouts to vegetated buffers or sheet flow through vegetated buffers towards Amethyst brook. Areas treated for water quality exceed new impervious areas created by this redevelopment project (see Section IV and Appendix E).

Based on the manufacturer's calculations, the hydrodynamic separators will provide greater than 90% removal of TSS.

IV. Calculations and Design

Water Quantity

Drainage calculations were performed on HydroCAD Stormwater Modeling System version 10.0 using Soil Conservation Service (SCS) TR-20 methodology. The SCS method is based on rainfall observations, which were used to develop the Intensity-Duration-Frequency relationship, or IDF

curve. The mass curve is a dimensionless distribution of rainfall over time, which indicates the fraction of the rainfall event that occurs at a given time within a 24-hour precipitation event. This synthetic distribution develops peak rates for storms of varying duration and intensities. The SCS distribution provides a cumulative rainfall at any point in time and allows volume-dependent routing runoff calculations to occur. These calculations are included in **Appendix C**. Rainfall values are taken from the latest Northeast Regional Climate Center (NRCC) and are listed in Table 1.

The watershed boundaries for calculation purposes are divided according to the proposed site grading and the parcel boundary. The curve numbers (CNs) for the existing and proposed sub-catchment area are based on the soil type and the existing and proposed cover conditions at the site. The time of concentration (Tc) for large sub-areas with extensive pervious areas is calculated using the lag method. Small sub-area Tcs are set at a minimum of 5 minutes.

Calculations were performed for the 2-, 10-, and 100-year frequency storms under existing and proposed conditions. The results of the calculations are presented in Table 1 below. **Appendix C** presents the HydroCAD output reports.

Table 1. Runoff Summary Table

Point of Analysis	2-Year Storm 3.07"	10-Year Storm 4.47"	100-Year Storm 7.68"
	Peak Flow Rate(cfs)	Peak Flow Rate(cfs)	Peak Flow Rate(cfs)
Existing	1.61	3.87	14.47
Proposed*	1.54	3.64	14.02

*Peak flow after storage/attenuation within underground storage chambers

Runoff from the site shows a decrease in peak flow for all storms between pre and post conditions.

Water Quality

Water quality at the proposed site is addressed with water quality units (hydrodynamic separators), followed by storage and infiltration. The proposed runoff from driveways, parking areas and a portion of the #20 roof (approximately 29,000 sf) is conveyed to water quality units for treatment prior to storage and infiltration.

Impervious areas (approximately 14,000 sf) which are not conveyed to water quality units include building roofs and some walkways. Runoff from roofs is either directed to storage facilities or discharged through disconnected downspouts to vegetated buffers. Vegetated swales are also included in the design to convey sidewalk runoff.

The Total Suspended Solids removal for the site provided by the water quality units is calculated by the manufacturer at over 90%.

Water quality volume is provided by storage within the underground detention systems below the lowest outlet pipe. Water quality volume is provided for 1" of runoff over the increased impervious area at the site (see cold water fisheries section below). Table 2 provides a summary of the water

quality calculations. The volume provided exceeds the calculated volume for the increased impervious area.

Table 2. Water Quality Volume

Existing Impervious Area (sf)	Proposed Impervious Area (sf)	Increase in Impervious Area (sf)	Water Quality Volume on increase (cf)	Water Quality Volume Provided in all facilities (cf)
28,640	41,840	13,200	1,100	1,170

Calculations supporting these conclusions are included in **Appendix E**.

Cold Water Fishery

The proposed redevelopment is within a cold water fishery requiring 80% TSS removal and treatment of the first inch of runoff. The proposed water quality units will provide 90% TSS removal of the runoff from the driveway and parking areas (see Appendix E). The improvements also include infiltration within the underground storage systems which provides temperature mitigation. Storage and detention within the underground storage chambers will also moderate the temperature of the runoff. Walkway areas treated with grass swales and flow through vegetated buffer areas and disconnected downspouts from some of the roofs completes the provided improvements.

Erosion & Sedimentation Control

The project plan set includes provisions for erosion control during construction. The project will be phased to limit the total land area disturbed at one time.

Erosion control barrier is included below all road and wall construction and around the new apartment construction. to prevent migration of sediment offsite or into resource areas during construction.

Straw wattles combined with silt fence are proposed for down-slope protection.

V. MADEP Stormwater Standards Compliance

The following section details how the project will meet the DEP Stormwater Management Policy’s ten stormwater management standards.

LID

The project is the redevelopment of the site of an old factory and associated driveway and parking by Amethyst Brook and a farmhouse off of Amherst Road. The project proposes to build multi-family housing at both sites and improve the driveway access. The possibility for LID is limited due to the steep terrain. Limited disturbance in the riverfront is also considered. Nevertheless, water quality is enhanced from existing conditions by conveying the majority of the impervious surfaces to water quality units which will significantly reduce TSS in the runoff from existing conditions since the existing parking lot and driveway has no water quality treatment. Grass swales, deep sump catch basins and a level spreader are also proposed at the site.

Standard 1 - Untreated Stormwater Discharge

The proposed project includes water quality units and underground detention/infiltration facilities designed to capture runoff from the impervious surfaces created and provide water quality treatment prior to discharge to the vegetated buffers and the brook. Existing outfalls, including the existing swale to Amethyst Brook and the drainage outlet from the existing garage are re-used.

Standard 2 - Post-Development Peak Discharge Rates

The proposed detention facilities provide attenuation of discharge rates such that post development discharge rates *are less than* pre-development peak discharge rates leaving the site.

These results are discussed in detail under “Peak Runoff Rate” in **Section IV**, above.

Standard 3 - Recharge to Groundwater

Recharge of the increased impervious area is provided within the proposed underground storage facilities based on the target depth factor of 0.6”. For the proposed increase in impervious area, the required recharge volume is 660 cf. The design includes capacity to recharge 1,170 cf which exceeds the required volume. Calculations of recharge are included within **Appendix D**.

Standard 4 – Water Quality

Impervious areas including driveways, parking areas and portions of roofs are captured by BMPs designed to remove 90% TSS.

The water quality volume is calculated based on 1”. For the proposed increase in impervious area, the required water quality volume is 1,100 cu. ft. The proposed facilities provide 1,170 cf thereby providing water quality for the additional impervious areas proposed.

Further discussion of this standard is included under “Water Quality” in Section III and in **Appendix E**.

Standard 5 - Higher Potential Pollutant Loads

This is not applicable to this project.

Standard 6 - Protection of Critical Areas

The project is located in a cold water fishery. TSS removal and water quality volume has been increased to meet the requirements of the cold water fishery. Underground storage, detention and infiltration provide runoff temperature moderation.

Standard 7 - Redevelopment Projects

This project is a redevelopment project and measures have been taken to improve existing conditions. Whereas the existing site has little provision for TSS removal, the proposed project includes water quality units designed to remove over 90% TSS from the majority of the proposed driveway and parking areas. Water quality volume is provided on the increased impervious areas proposed. Recharge volume exceeds the volume calculated for the increased impervious area by over 75%.

Standard 8 - Erosion/Sediment Control

Proposed erosion and sediment controls are shown on the drainage plan for the site.

Standard 9 - Operation/Maintenance Plan

An Operation and Maintenance Plan for the proposed project is included in **Appendix F**. It includes general controls for construction and long term maintenance of the R-Tank systems and Water Quality Units.

Standard 10 – Prohibition of Illicit Discharges

No Illicit Discharge Compliance Statement is included with this report. It will be the responsibility of the owner to submit a statement prior to the discharge of any stormwater to post-construction BMPs.

FIGURES



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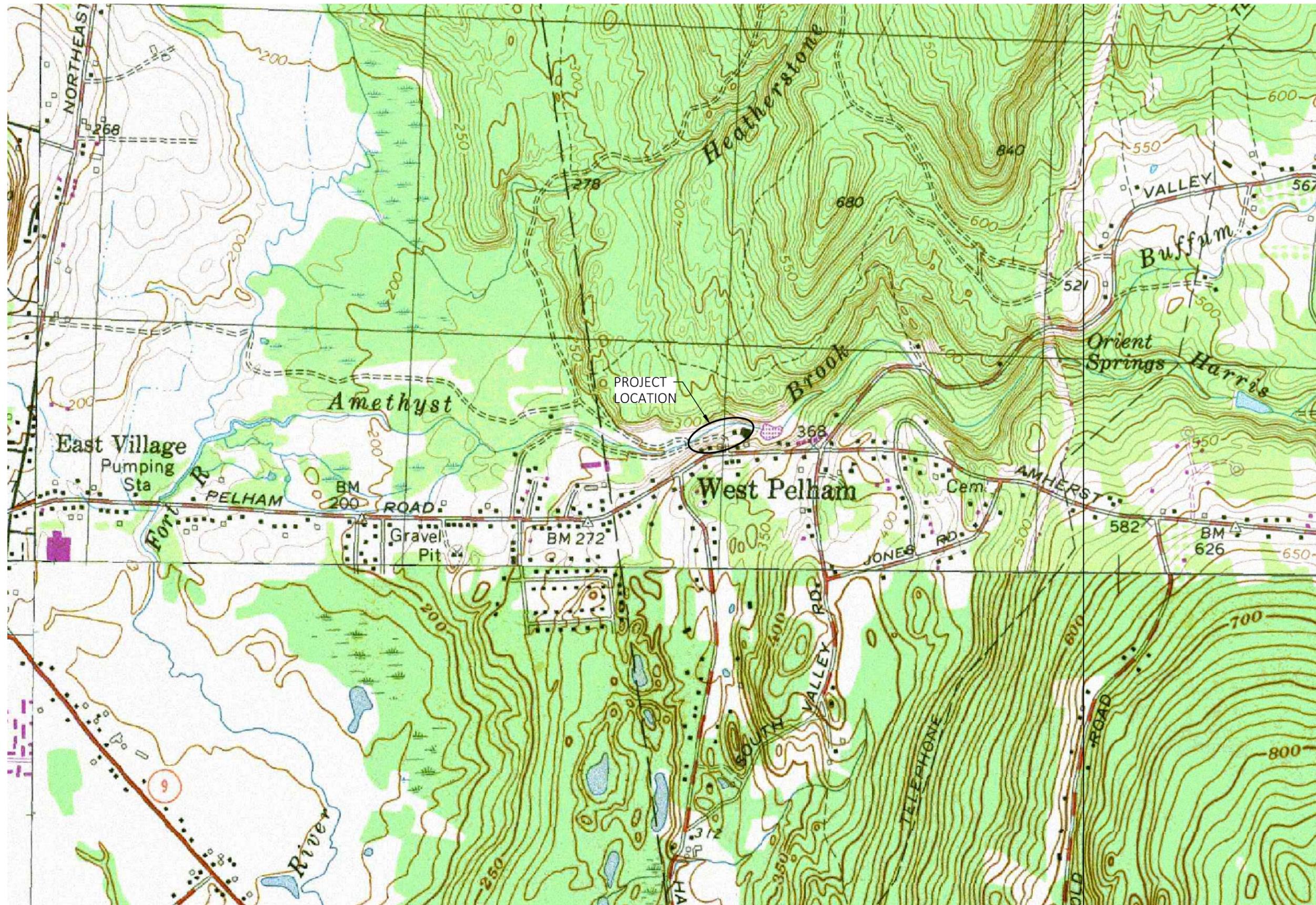
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FIG 1

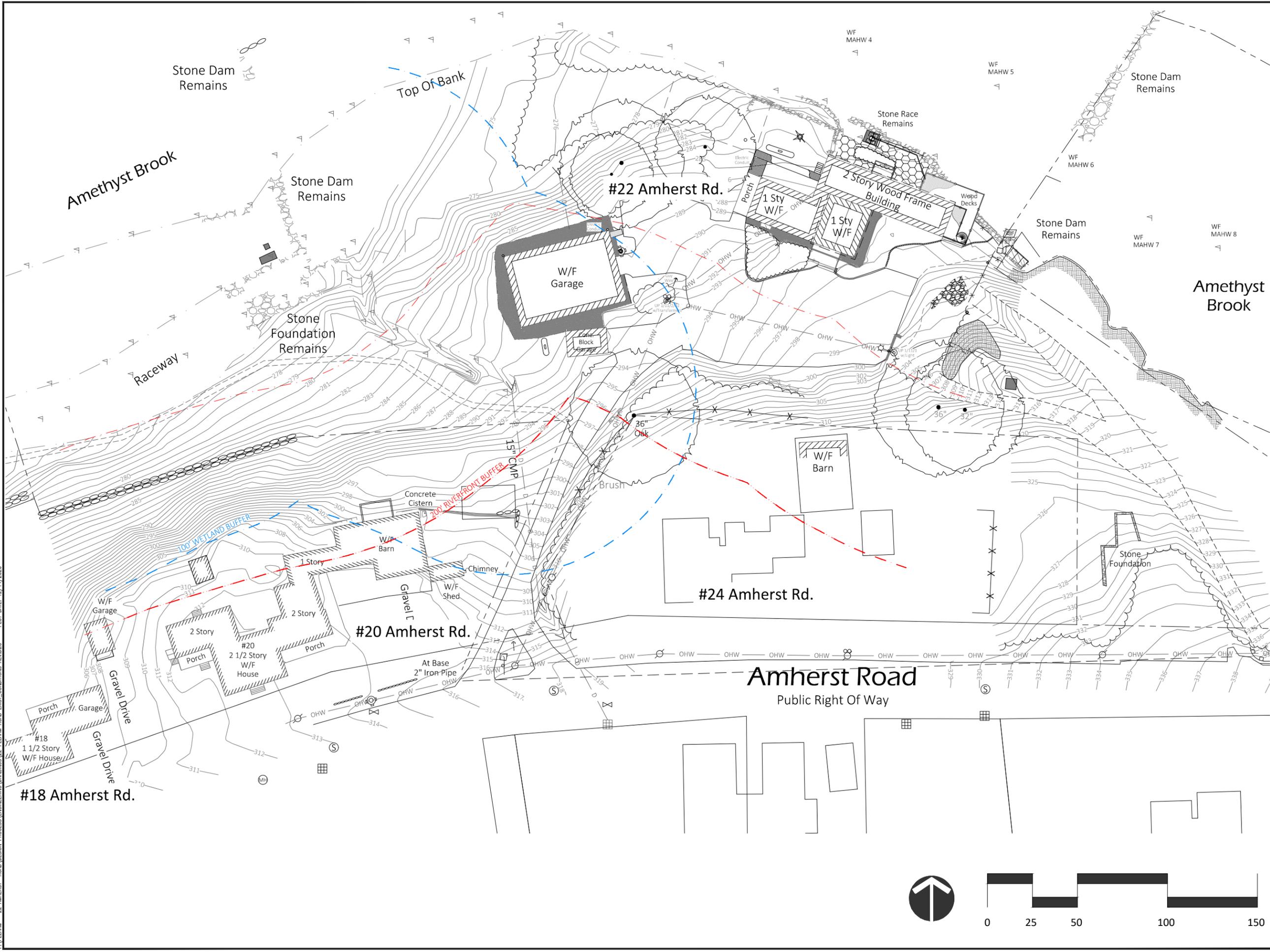


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EXISTING CONDITIONS PLAN

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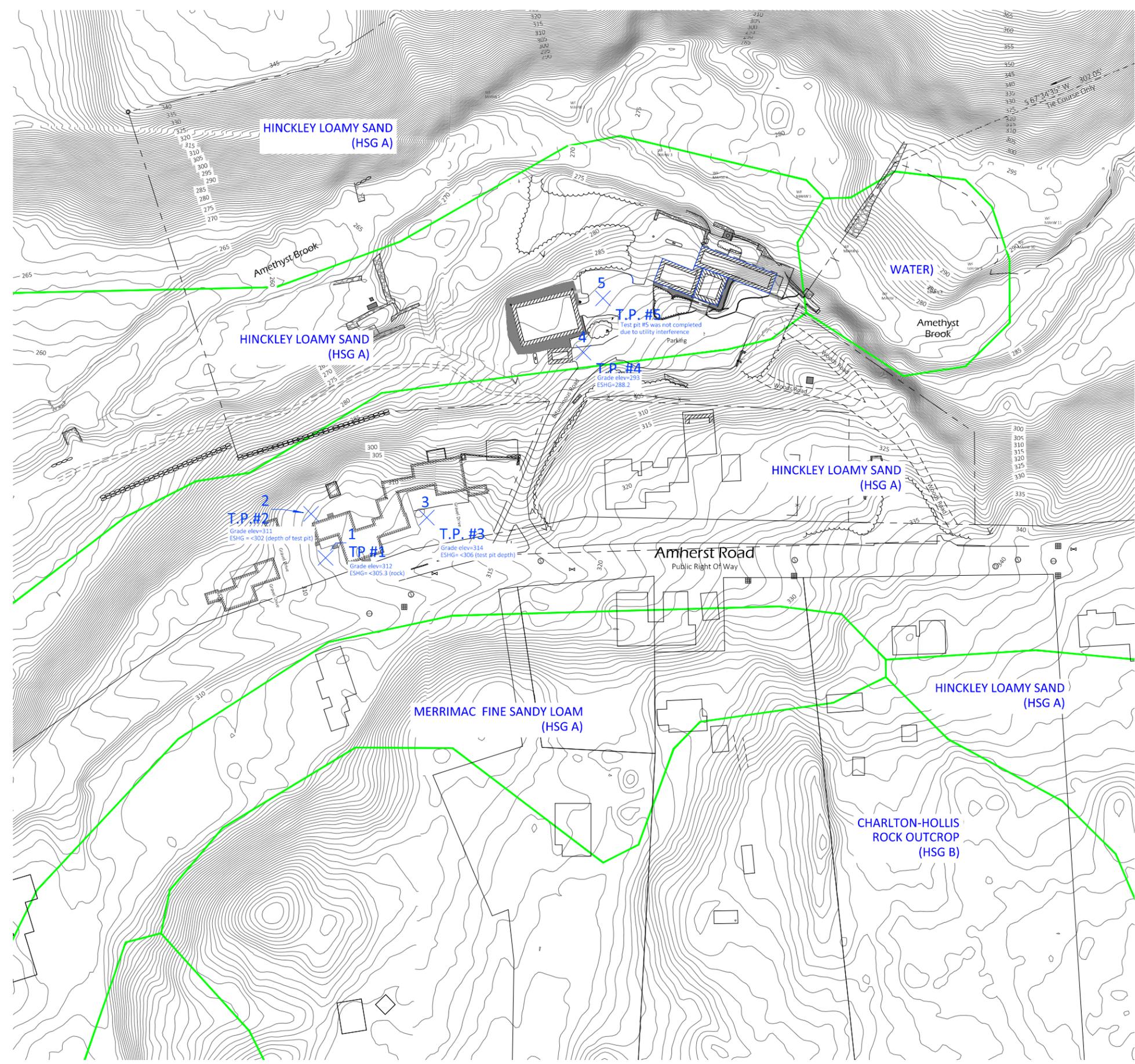
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DRAINAGE AREA SOILS

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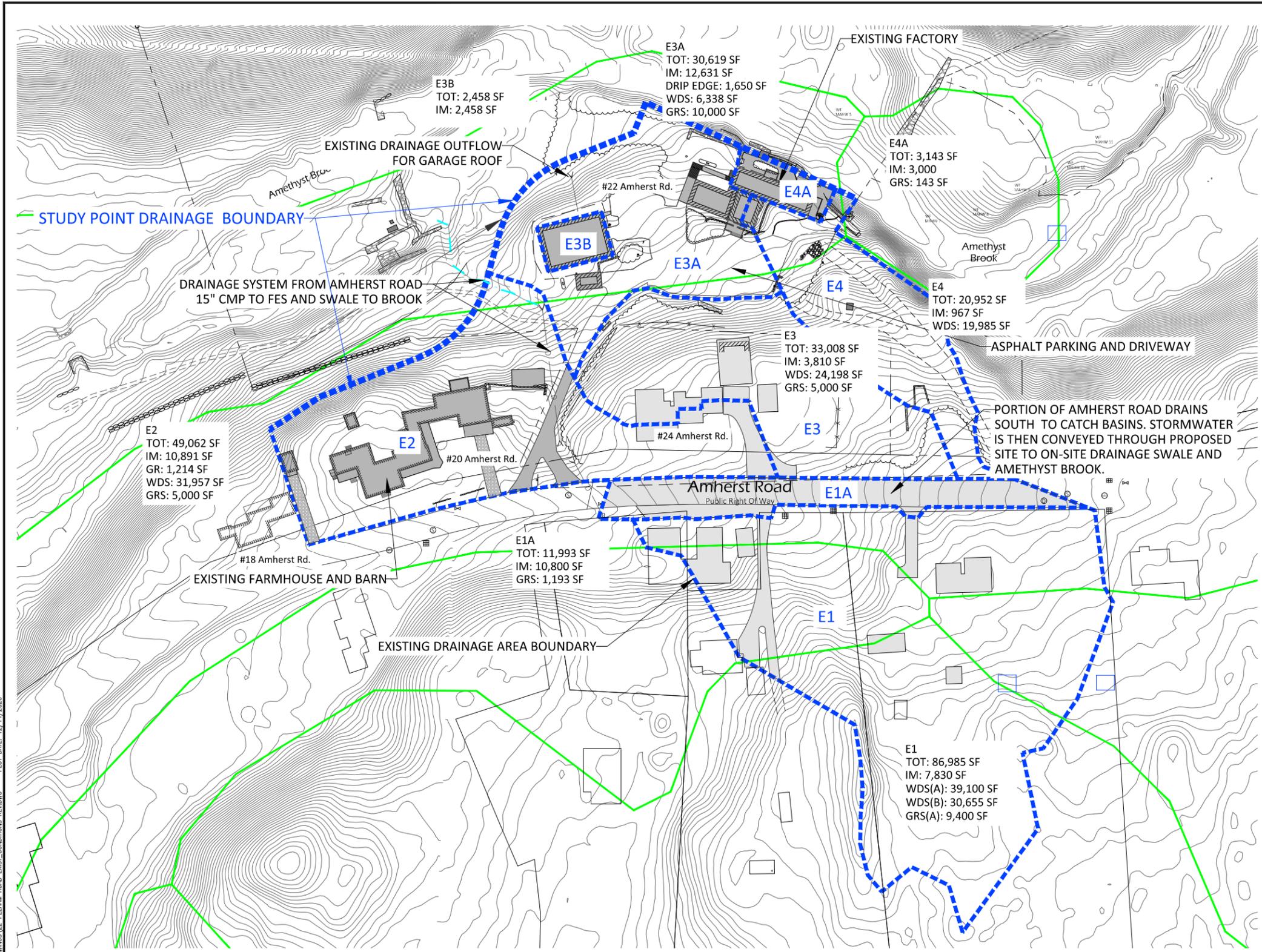
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AMETHYST BROOK APARTMENTS
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EXISTING HYDROLOGY

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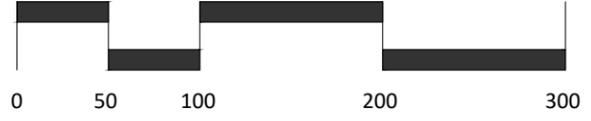
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■ OFF-SITE IMPERVIOUS AREA
■ ON-SITE IMPERVIOUS AREA

TOT = TOTAL AREA
IMP = IMPERVIOUS AREA
WDS = WOODED (FAIR)
GRS - OPEN SPACE (FAIR)

- NOTES:
- LIMITS OF IMPERVIOUS SURFACE LIMITS OFF SITE APPROXIMATED FROM AERIAL PHOTOGRAPHY AND MASS GIS.
 - SOILS ARE HSG A NORTH OF AMHERST ROAD. THE DRAINAGE AREA SOUTH OF AMHERST ROAD IS HSG A AND B.



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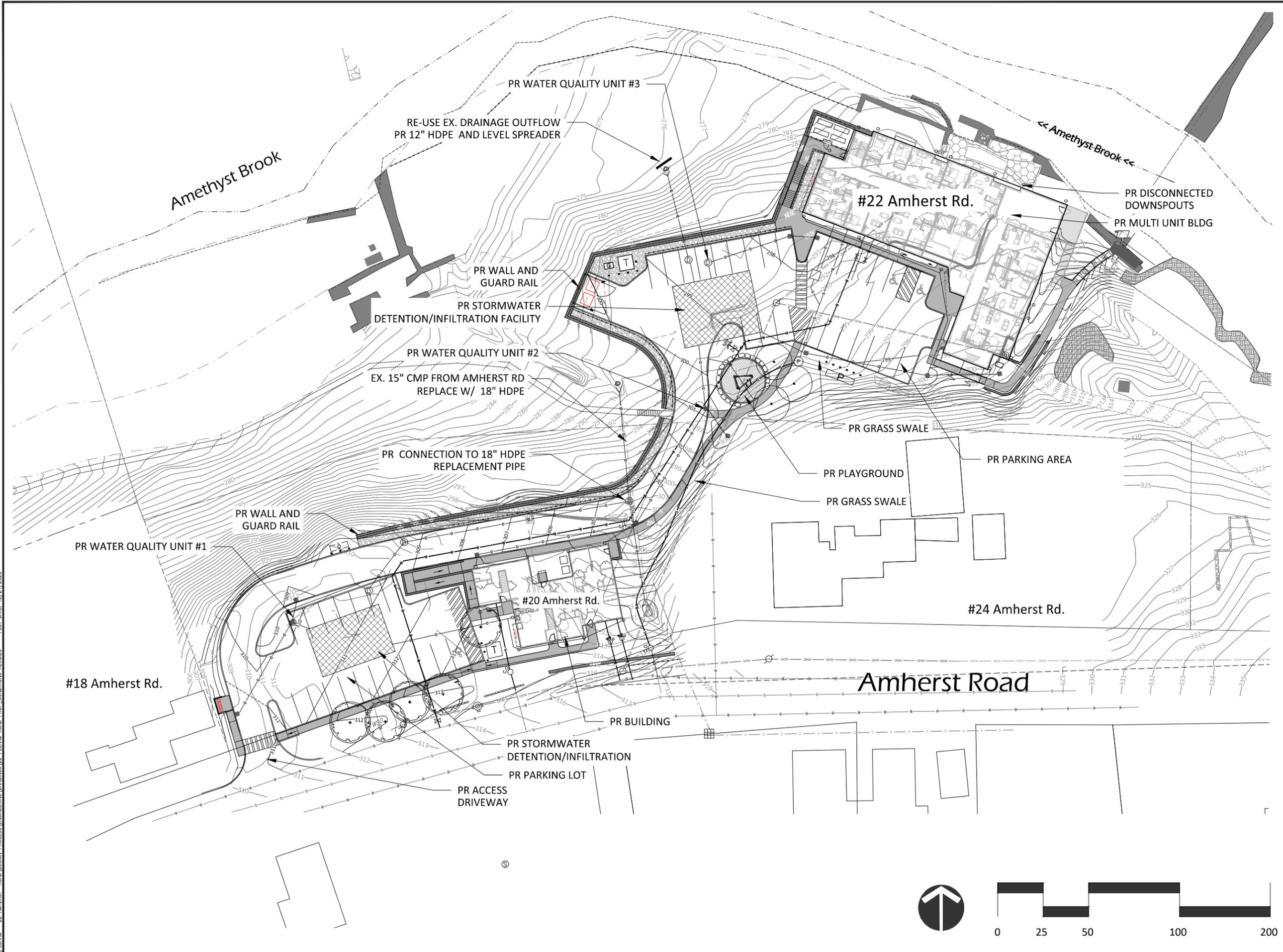
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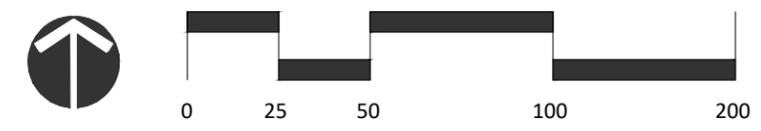
PROPOSED PLAN

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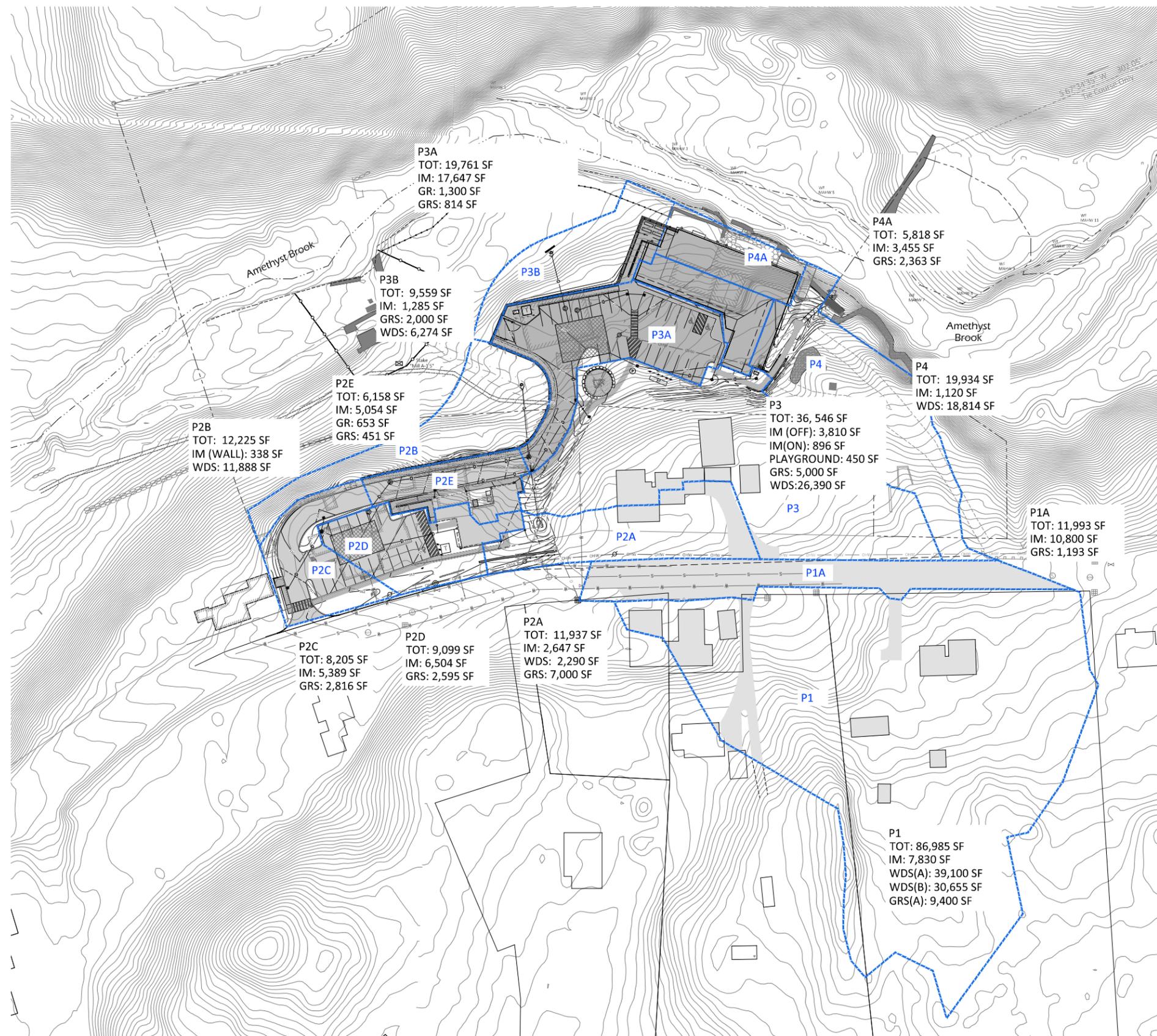
AMETHYST BROOK APARTMENTS
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PROPOSED DRAINAGE

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FIG 6



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Appendix A– NRCS Soils Report



United States
Department of
Agriculture

NRCS

Natural
Resources
Conservation
Service

A product of the National
Cooperative Soil Survey,
a joint effort of the United
States Department of
Agriculture and other
Federal agencies, State
agencies including the
Agricultural Experiment
Stations, and local
participants

Custom Soil Resource Report for Hampden and Hampshire Counties, Massachusetts, Eastern Part

22 Pelham Road



Preface

Soil surveys contain information that affects land use planning in survey areas. They highlight soil limitations that affect various land uses and provide information about the properties of the soils in the survey areas. Soil surveys are designed for many different users, including farmers, ranchers, foresters, agronomists, urban planners, community officials, engineers, developers, builders, and home buyers. Also, conservationists, teachers, students, and specialists in recreation, waste disposal, and pollution control can use the surveys to help them understand, protect, or enhance the environment.

Various land use regulations of Federal, State, and local governments may impose special restrictions on land use or land treatment. Soil surveys identify soil properties that are used in making various land use or land treatment decisions. The information is intended to help the land users identify and reduce the effects of soil limitations on various land uses. The landowner or user is responsible for identifying and complying with existing laws and regulations.

Although soil survey information can be used for general farm, local, and wider area planning, onsite investigation is needed to supplement this information in some cases. Examples include soil quality assessments (<http://www.nrcs.usda.gov/wps/portal/nrcs/main/soils/health/>) and certain conservation and engineering applications. For more detailed information, contact your local USDA Service Center (<https://offices.sc.egov.usda.gov/locator/app?agency=nrcs>) or your NRCS State Soil Scientist (http://www.nrcs.usda.gov/wps/portal/nrcs/detail/soils/contactus/?cid=nrcs142p2_053951).

Great differences in soil properties can occur within short distances. Some soils are seasonally wet or subject to flooding. Some are too unstable to be used as a foundation for buildings or roads. Clayey or wet soils are poorly suited to use as septic tank absorption fields. A high water table makes a soil poorly suited to basements or underground installations.

The National Cooperative Soil Survey is a joint effort of the United States Department of Agriculture and other Federal agencies, State agencies including the Agricultural Experiment Stations, and local agencies. The Natural Resources Conservation Service (NRCS) has leadership for the Federal part of the National Cooperative Soil Survey.

Information about soils is updated periodically. Updated information is available through the NRCS Web Soil Survey, the site for official soil survey information.

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How Soil Surveys Are Made

Soil surveys are made to provide information about the soils and miscellaneous areas in a specific area. They include a description of the soils and miscellaneous areas and their location on the landscape and tables that show soil properties and limitations affecting various uses. Soil scientists observed the steepness, length, and shape of the slopes; the general pattern of drainage; the kinds of crops and native plants; and the kinds of bedrock. They observed and described many soil profiles. A soil profile is the sequence of natural layers, or horizons, in a soil. The profile extends from the surface down into the unconsolidated material in which the soil formed or from the surface down to bedrock. The unconsolidated material is devoid of roots and other living organisms and has not been changed by other biological activity.

Currently, soils are mapped according to the boundaries of major land resource areas (MLRAs). MLRAs are geographically associated land resource units that share common characteristics related to physiography, geology, climate, water resources, soils, biological resources, and land uses (USDA, 2006). Soil survey areas typically consist of parts of one or more MLRA.

The soils and miscellaneous areas in a survey area occur in an orderly pattern that is related to the geology, landforms, relief, climate, and natural vegetation of the area. Each kind of soil and miscellaneous area is associated with a particular kind of landform or with a segment of the landform. By observing the soils and miscellaneous areas in the survey area and relating their position to specific segments of the landform, a soil scientist develops a concept, or model, of how they were formed. Thus, during mapping, this model enables the soil scientist to predict with a considerable degree of accuracy the kind of soil or miscellaneous area at a specific location on the landscape.

Commonly, individual soils on the landscape merge into one another as their characteristics gradually change. To construct an accurate soil map, however, soil scientists must determine the boundaries between the soils. They can observe only a limited number of soil profiles. Nevertheless, these observations, supplemented by an understanding of the soil-vegetation-landscape relationship, are sufficient to verify predictions of the kinds of soil in an area and to determine the boundaries.

Soil scientists recorded the characteristics of the soil profiles that they studied. They noted soil color, texture, size and shape of soil aggregates, kind and amount of rock fragments, distribution of plant roots, reaction, and other features that enable them to identify soils. After describing the soils in the survey area and determining their properties, the soil scientists assigned the soils to taxonomic classes (units). Taxonomic classes are concepts. Each taxonomic class has a set of soil characteristics with precisely defined limits. The classes are used as a basis for comparison to classify soils systematically. Soil taxonomy, the system of taxonomic classification used in the United States, is based mainly on the kind and character of soil properties and the arrangement of horizons within the profile. After the soil

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scientists classified and named the soils in the survey area, they compared the individual soils with similar soils in the same taxonomic class in other areas so that they could confirm data and assemble additional data based on experience and research.

The objective of soil mapping is not to delineate pure map unit components; the objective is to separate the landscape into landforms or landform segments that have similar use and management requirements. Each map unit is defined by a unique combination of soil components and/or miscellaneous areas in predictable proportions. Some components may be highly contrasting to the other components of the map unit. The presence of minor components in a map unit in no way diminishes the usefulness or accuracy of the data. The delineation of such landforms and landform segments on the map provides sufficient information for the development of resource plans. If intensive use of small areas is planned, onsite investigation is needed to define and locate the soils and miscellaneous areas.

Soil scientists make many field observations in the process of producing a soil map. The frequency of observation is dependent upon several factors, including scale of mapping, intensity of mapping, design of map units, complexity of the landscape, and experience of the soil scientist. Observations are made to test and refine the soil-landscape model and predictions and to verify the classification of the soils at specific locations. Once the soil-landscape model is refined, a significantly smaller number of measurements of individual soil properties are made and recorded. These measurements may include field measurements, such as those for color, depth to bedrock, and texture, and laboratory measurements, such as those for content of sand, silt, clay, salt, and other components. Properties of each soil typically vary from one point to another across the landscape.

Observations for map unit components are aggregated to develop ranges of characteristics for the components. The aggregated values are presented. Direct measurements do not exist for every property presented for every map unit component. Values for some properties are estimated from combinations of other properties.

While a soil survey is in progress, samples of some of the soils in the area generally are collected for laboratory analyses and for engineering tests. Soil scientists interpret the data from these analyses and tests as well as the field-observed characteristics and the soil properties to determine the expected behavior of the soils under different uses. Interpretations for all of the soils are field tested through observation of the soils in different uses and under different levels of management. Some interpretations are modified to fit local conditions, and some new interpretations are developed to meet local needs. Data are assembled from other sources, such as research information, production records, and field experience of specialists. For example, data on crop yields under defined levels of management are assembled from farm records and from field or plot experiments on the same kinds of soil.

Predictions about soil behavior are based not only on soil properties but also on such variables as climate and biological activity. Soil conditions are predictable over long periods of time, but they are not predictable from year to year. For example, soil scientists can predict with a fairly high degree of accuracy that a given soil will have a high water table within certain depths in most years, but they cannot predict that a high water table will always be at a specific level in the soil on a specific date.

After soil scientists located and identified the significant natural bodies of soil in the survey area, they drew the boundaries of these bodies on aerial photographs and

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identified each as a specific map unit. Aerial photographs show trees, buildings, fields, roads, and rivers, all of which help in locating boundaries accurately.

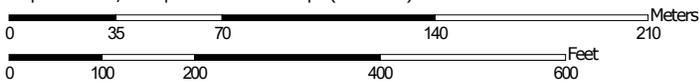
Soil Map

The soil map section includes the soil map for the defined area of interest, a list of soil map units on the map and extent of each map unit, and cartographic symbols displayed on the map. Also presented are various metadata about data used to produce the map, and a description of each soil map unit.

Custom Soil Resource Report Soil Map



Map Scale: 1:2,470 if printed on A landscape (11" x 8.5") sheet.



Map projection: Web Mercator Corner coordinates: WGS84 Edge tics: UTM Zone 18N WGS84

MAP LEGEND

Area of Interest (AOI)

 Area of Interest (AOI)

Soils

 Soil Map Unit Polygons

 Soil Map Unit Lines

 Soil Map Unit Points

Special Point Features

-  Blowout
-  Borrow Pit
-  Clay Spot
-  Closed Depression
-  Gravel Pit
-  Gravelly Spot
-  Landfill
-  Lava Flow
-  Marsh or swamp
-  Mine or Quarry
-  Miscellaneous Water
-  Perennial Water
-  Rock Outcrop
-  Saline Spot
-  Sandy Spot
-  Severely Eroded Spot
-  Sinkhole
-  Slide or Slip
-  Sodic Spot

-  Spoil Area
-  Stony Spot
-  Very Stony Spot
-  Wet Spot
-  Other
-  Special Line Features

Water Features

 Streams and Canals

Transportation

-  Rails
-  Interstate Highways
-  US Routes
-  Major Roads
-  Local Roads

Background

 Aerial Photography

MAP INFORMATION

The soil surveys that comprise your AOI were mapped at 1:25,000.

Warning: Soil Map may not be valid at this scale.

Enlargement of maps beyond the scale of mapping can cause misunderstanding of the detail of mapping and accuracy of soil line placement. The maps do not show the small areas of contrasting soils that could have been shown at a more detailed scale.

Please rely on the bar scale on each map sheet for map measurements.

Source of Map: Natural Resources Conservation Service
 Web Soil Survey URL:
 Coordinate System: Web Mercator (EPSG:3857)

Maps from the Web Soil Survey are based on the Web Mercator projection, which preserves direction and shape but distorts distance and area. A projection that preserves area, such as the Albers equal-area conic projection, should be used if more accurate calculations of distance or area are required.

This product is generated from the USDA-NRCS certified data as of the version date(s) listed below.

Soil Survey Area: Hampden and Hampshire Counties, Massachusetts, Eastern Part
 Survey Area Data: Version 14, Sep 13, 2019

Soil map units are labeled (as space allows) for map scales 1:50,000 or larger.

Date(s) aerial images were photographed: Sep 29, 2013—Oct 16, 2016

The orthophoto or other base map on which the soil lines were compiled and digitized probably differs from the background

MAP LEGEND

MAP INFORMATION

imagery displayed on these maps. As a result, some minor shifting of map unit boundaries may be evident.

Map Unit Legend

Map Unit Symbol	Map Unit Name	Acres in AOI	Percent of AOI
1	Water	0.7	2.2%
71B	Ridgebury fine sandy loam, 3 to 8 percent slopes, extremely stony	0.4	1.3%
103C	Charlton-Hollis-Rock outcrop complex, 8 to 15 percent slopes	6.8	21.9%
253B	Hinckley loamy sand, 3 to 8 percent slopes	6.9	22.2%
253C	Hinckley loamy sand, 8 to 15 percent slopes	0.1	0.3%
253D	Hinckley loamy sand, 15 to 25 percent slopes	13.5	43.3%
254B	Merrimac fine sandy loam, 3 to 8 percent slopes	2.7	8.8%
Totals for Area of Interest		31.2	100.0%

Map Unit Descriptions

The map units delineated on the detailed soil maps in a soil survey represent the soils or miscellaneous areas in the survey area. The map unit descriptions, along with the maps, can be used to determine the composition and properties of a unit.

A map unit delineation on a soil map represents an area dominated by one or more major kinds of soil or miscellaneous areas. A map unit is identified and named according to the taxonomic classification of the dominant soils. Within a taxonomic class there are precisely defined limits for the properties of the soils. On the landscape, however, the soils are natural phenomena, and they have the characteristic variability of all natural phenomena. Thus, the range of some observed properties may extend beyond the limits defined for a taxonomic class. Areas of soils of a single taxonomic class rarely, if ever, can be mapped without including areas of other taxonomic classes. Consequently, every map unit is made up of the soils or miscellaneous areas for which it is named and some minor components that belong to taxonomic classes other than those of the major soils.

Most minor soils have properties similar to those of the dominant soil or soils in the map unit, and thus they do not affect use and management. These are called noncontrasting, or similar, components. They may or may not be mentioned in a particular map unit description. Other minor components, however, have properties and behavioral characteristics divergent enough to affect use or to require different management. These are called contrasting, or dissimilar, components. They generally are in small areas and could not be mapped separately because of the scale used. Some small areas of strongly contrasting soils or miscellaneous areas are identified by a special symbol on the maps. If included in the database for a given area, the contrasting minor components are identified in the map unit

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descriptions along with some characteristics of each. A few areas of minor components may not have been observed, and consequently they are not mentioned in the descriptions, especially where the pattern was so complex that it was impractical to make enough observations to identify all the soils and miscellaneous areas on the landscape.

The presence of minor components in a map unit in no way diminishes the usefulness or accuracy of the data. The objective of mapping is not to delineate pure taxonomic classes but rather to separate the landscape into landforms or landform segments that have similar use and management requirements. The delineation of such segments on the map provides sufficient information for the development of resource plans. If intensive use of small areas is planned, however, onsite investigation is needed to define and locate the soils and miscellaneous areas.

An identifying symbol precedes the map unit name in the map unit descriptions. Each description includes general facts about the unit and gives important soil properties and qualities.

Soils that have profiles that are almost alike make up a *soil series*. Except for differences in texture of the surface layer, all the soils of a series have major horizons that are similar in composition, thickness, and arrangement.

Soils of one series can differ in texture of the surface layer, slope, stoniness, salinity, degree of erosion, and other characteristics that affect their use. On the basis of such differences, a soil series is divided into *soil phases*. Most of the areas shown on the detailed soil maps are phases of soil series. The name of a soil phase commonly indicates a feature that affects use or management. For example, Alpha silt loam, 0 to 2 percent slopes, is a phase of the Alpha series.

Some map units are made up of two or more major soils or miscellaneous areas. These map units are complexes, associations, or undifferentiated groups.

A *complex* consists of two or more soils or miscellaneous areas in such an intricate pattern or in such small areas that they cannot be shown separately on the maps. The pattern and proportion of the soils or miscellaneous areas are somewhat similar in all areas. Alpha-Beta complex, 0 to 6 percent slopes, is an example.

An *association* is made up of two or more geographically associated soils or miscellaneous areas that are shown as one unit on the maps. Because of present or anticipated uses of the map units in the survey area, it was not considered practical or necessary to map the soils or miscellaneous areas separately. The pattern and relative proportion of the soils or miscellaneous areas are somewhat similar. Alpha-Beta association, 0 to 2 percent slopes, is an example.

An *undifferentiated group* is made up of two or more soils or miscellaneous areas that could be mapped individually but are mapped as one unit because similar interpretations can be made for use and management. The pattern and proportion of the soils or miscellaneous areas in a mapped area are not uniform. An area can be made up of only one of the major soils or miscellaneous areas, or it can be made up of all of them. Alpha and Beta soils, 0 to 2 percent slopes, is an example.

Some surveys include *miscellaneous areas*. Such areas have little or no soil material and support little or no vegetation. Rock outcrop is an example.

Hampden and Hampshire Counties, Massachusetts, Eastern Part

1—Water

Map Unit Setting

National map unit symbol: vhz0
Mean annual precipitation: 32 to 50 inches
Mean annual air temperature: 45 to 50 degrees F
Frost-free period: 110 to 140 days
Farmland classification: Not prime farmland

Map Unit Composition

Water: 100 percent
Estimates are based on observations, descriptions, and transects of the mapunit.

71B—Ridgebury fine sandy loam, 3 to 8 percent slopes, extremely stony

Map Unit Setting

National map unit symbol: 2w69c
Elevation: 0 to 1,290 feet
Mean annual precipitation: 36 to 71 inches
Mean annual air temperature: 39 to 55 degrees F
Frost-free period: 140 to 240 days
Farmland classification: Not prime farmland

Map Unit Composition

Ridgebury, extremely stony, and similar soils: 80 percent
Minor components: 20 percent
Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Ridgebury, Extremely Stony

Setting

Landform: Ground moraines, drumlins, drainageways, depressions, hills
Landform position (two-dimensional): Toeslope, footslope
Landform position (three-dimensional): Head slope, base slope
Down-slope shape: Concave
Across-slope shape: Concave
Parent material: Coarse-loamy lodgment till derived from gneiss, granite, and/or schist

Typical profile

Oe - 0 to 1 inches: moderately decomposed plant material
A - 1 to 6 inches: fine sandy loam
Bw - 6 to 10 inches: sandy loam
Bg - 10 to 19 inches: gravelly sandy loam
Cd - 19 to 66 inches: gravelly sandy loam

Properties and qualities

Slope: 3 to 8 percent
Percent of area covered with surface fragments: 9.0 percent
Depth to restrictive feature: 15 to 35 inches to densic material

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Natural drainage class: Poorly drained
Runoff class: Very high
Capacity of the most limiting layer to transmit water (Ksat): Very low to moderately low (0.00 to 0.14 in/hr)
Depth to water table: About 0 to 6 inches
Frequency of flooding: None
Frequency of ponding: None
Salinity, maximum in profile: Nonsaline (0.0 to 1.9 mmhos/cm)
Available water storage in profile: Low (about 3.0 inches)

Interpretive groups

Land capability classification (irrigated): None specified
Land capability classification (nonirrigated): 7s
Hydrologic Soil Group: D
Hydric soil rating: Yes

Minor Components

Woodbridge, extremely stony

Percent of map unit: 10 percent
Landform: Hills, drumlins, ground moraines
Landform position (two-dimensional): Footslope, summit, backslope
Landform position (three-dimensional): Crest, side slope
Down-slope shape: Convex
Across-slope shape: Linear
Hydric soil rating: No

Whitman, extremely stony

Percent of map unit: 8 percent
Landform: Depressions
Down-slope shape: Concave
Across-slope shape: Concave
Hydric soil rating: Yes

Paxton, extremely stony

Percent of map unit: 2 percent
Landform: Hills, drumlins, ground moraines
Landform position (two-dimensional): Summit, shoulder, backslope
Landform position (three-dimensional): Crest, side slope
Down-slope shape: Convex, linear
Across-slope shape: Convex, linear
Hydric soil rating: No

103C—Charlton-Hollis-Rock outcrop complex, 8 to 15 percent slopes

Map Unit Setting

National map unit symbol: 2wzp1
Elevation: 0 to 1,390 feet
Mean annual precipitation: 36 to 71 inches
Mean annual air temperature: 39 to 55 degrees F
Frost-free period: 140 to 240 days

Custom Soil Resource Report

Farmland classification: Not prime farmland

Map Unit Composition

Charlton, extremely stony, and similar soils: 50 percent

Hollis, extremely stony, and similar soils: 20 percent

Rock outcrop: 10 percent

Minor components: 20 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Charlton, Extremely Stony

Setting

Landform: Ridges, hills

Landform position (two-dimensional): Backslope

Landform position (three-dimensional): Side slope

Down-slope shape: Linear, convex

Across-slope shape: Convex

Parent material: Coarse-loamy melt-out till derived from granite, gneiss, and/or schist

Typical profile

Oe - 0 to 2 inches: moderately decomposed plant material

A - 2 to 4 inches: fine sandy loam

Bw - 4 to 27 inches: gravelly fine sandy loam

C - 27 to 65 inches: gravelly fine sandy loam

Properties and qualities

Slope: 8 to 15 percent

Percent of area covered with surface fragments: 9.0 percent

Depth to restrictive feature: More than 80 inches

Natural drainage class: Well drained

Runoff class: Low

Capacity of the most limiting layer to transmit water (Ksat): Moderately low to high
(0.14 to 14.17 in/hr)

Depth to water table: More than 80 inches

Frequency of flooding: None

Frequency of ponding: None

Salinity, maximum in profile: Nonsaline (0.0 to 1.9 mmhos/cm)

Available water storage in profile: Moderate (about 8.7 inches)

Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 7s

Hydrologic Soil Group: B

Hydric soil rating: No

Description of Hollis, Extremely Stony

Setting

Landform: Ridges, hills

Landform position (two-dimensional): Backslope, shoulder, summit

Landform position (three-dimensional): Side slope, nose slope, crest

Down-slope shape: Convex

Across-slope shape: Linear, convex

Parent material: Coarse-loamy melt-out till derived from granite, gneiss, and/or schist

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Typical profile

O_i - 0 to 2 inches: slightly decomposed plant material
A - 2 to 7 inches: gravelly fine sandy loam
B_w - 7 to 16 inches: gravelly fine sandy loam
2R - 16 to 26 inches: bedrock

Properties and qualities

Slope: 8 to 15 percent
Percent of area covered with surface fragments: 9.0 percent
Depth to restrictive feature: 8 to 23 inches to lithic bedrock
Natural drainage class: Somewhat excessively drained
Runoff class: Very high
Capacity of the most limiting layer to transmit water (K_{sat}): Very low (0.00 to 0.00 in/hr)
Depth to water table: More than 80 inches
Frequency of flooding: None
Frequency of ponding: None
Salinity, maximum in profile: Nonsaline (0.0 to 1.9 mmhos/cm)
Available water storage in profile: Very low (about 2.7 inches)

Interpretive groups

Land capability classification (irrigated): None specified
Land capability classification (nonirrigated): 7s
Hydrologic Soil Group: D
Hydric soil rating: No

Description of Rock Outcrop

Setting

Landform: Hills, ridges
Parent material: Igneous and metamorphic rock

Typical profile

R - 0 to 79 inches: bedrock

Properties and qualities

Slope: 8 to 15 percent
Depth to restrictive feature: 0 inches to lithic bedrock
Runoff class: Very high
Capacity of the most limiting layer to transmit water (K_{sat}): Very low (0.00 to 0.00 in/hr)
Available water storage in profile: Very low (about 0.0 inches)

Interpretive groups

Land capability classification (irrigated): None specified
Land capability classification (nonirrigated): 8
Hydrologic Soil Group: D
Hydric soil rating: No

Minor Components

Woodbridge, extremely stony

Percent of map unit: 8 percent
Landform: Hills, drumlins, ground moraines
Landform position (two-dimensional): Backslope, footslope
Landform position (three-dimensional): Side slope
Down-slope shape: Convex

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Across-slope shape: Linear

Hydric soil rating: No

Canton, extremely stony

Percent of map unit: 5 percent

Landform: Hills, ridges, moraines

Landform position (two-dimensional): Backslope

Landform position (three-dimensional): Side slope

Down-slope shape: Linear, convex

Across-slope shape: Convex

Hydric soil rating: No

Chatfield, extremely stony

Percent of map unit: 5 percent

Landform: Hills, ridges

Landform position (two-dimensional): Summit, backslope, shoulder

Landform position (three-dimensional): Side slope, nose slope, crest

Down-slope shape: Convex

Across-slope shape: Linear, convex

Hydric soil rating: No

Ridgebury, extremely stony

Percent of map unit: 2 percent

Landform: Depressions, hills, drainageways, ground moraines, drumlins

Landform position (two-dimensional): Toeslope, footslope

Landform position (three-dimensional): Base slope, head slope

Down-slope shape: Concave

Across-slope shape: Concave

Hydric soil rating: Yes

253B—Hinckley loamy sand, 3 to 8 percent slopes

Map Unit Setting

National map unit symbol: 2svm8

Elevation: 0 to 1,430 feet

Mean annual precipitation: 36 to 53 inches

Mean annual air temperature: 39 to 55 degrees F

Frost-free period: 140 to 250 days

Farmland classification: Farmland of statewide importance

Map Unit Composition

Hinckley and similar soils: 85 percent

Minor components: 15 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Hinckley

Setting

Landform: Kame terraces, outwash deltas, kames, eskers, outwash terraces, outwash plains, moraines

Landform position (two-dimensional): Summit, backslope, footslope, shoulder

Landform position (three-dimensional): Nose slope, side slope, base slope, crest, tread, riser

Down-slope shape: Linear, convex, concave

Across-slope shape: Convex, linear, concave

Parent material: Sandy and gravelly glaciofluvial deposits derived from gneiss and/or granite and/or schist

Typical profile

Oe - 0 to 1 inches: moderately decomposed plant material

A - 1 to 8 inches: loamy sand

Bw1 - 8 to 11 inches: gravelly loamy sand

Bw2 - 11 to 16 inches: gravelly loamy sand

BC - 16 to 19 inches: very gravelly loamy sand

C - 19 to 65 inches: very gravelly sand

Properties and qualities

Slope: 3 to 8 percent

Depth to restrictive feature: More than 80 inches

Natural drainage class: Excessively drained

Runoff class: Very low

Capacity of the most limiting layer to transmit water (Ksat): Moderately high to very high (1.42 to 99.90 in/hr)

Depth to water table: More than 80 inches

Frequency of flooding: None

Frequency of ponding: None

Salinity, maximum in profile: Nonsaline (0.0 to 1.9 mmhos/cm)

Available water storage in profile: Very low (about 3.0 inches)

Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 3s

Hydrologic Soil Group: A

Hydric soil rating: No

Minor Components

Windsor

Percent of map unit: 8 percent

Landform: Eskers, outwash terraces, kames, kame terraces, outwash plains, moraines, outwash deltas

Landform position (two-dimensional): Summit, shoulder, backslope, footslope

Landform position (three-dimensional): Nose slope, side slope, base slope, crest, riser, tread

Down-slope shape: Linear, convex, concave

Across-slope shape: Convex, linear, concave

Hydric soil rating: No

Sudbury

Percent of map unit: 5 percent

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Landform: Kame terraces, outwash plains, moraines, outwash deltas, outwash terraces

Landform position (two-dimensional): Backslope, footslope

Landform position (three-dimensional): Side slope, base slope, head slope, tread

Down-slope shape: Concave, linear

Across-slope shape: Linear, concave

Hydric soil rating: No

Agawam

Percent of map unit: 2 percent

Landform: Kames, kame terraces, outwash plains, moraines, outwash deltas, eskers, outwash terraces

Landform position (two-dimensional): Summit, shoulder, backslope, footslope

Landform position (three-dimensional): Nose slope, side slope, base slope, crest, tread, riser

Down-slope shape: Linear, convex, concave

Across-slope shape: Convex, linear, concave

Hydric soil rating: No

253C—Hinckley loamy sand, 8 to 15 percent slopes

Map Unit Setting

National map unit symbol: 2svm9

Elevation: 0 to 1,480 feet

Mean annual precipitation: 36 to 71 inches

Mean annual air temperature: 39 to 55 degrees F

Frost-free period: 140 to 240 days

Farmland classification: Farmland of statewide importance

Map Unit Composition

Hinckley and similar soils: 85 percent

Minor components: 15 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Hinckley

Setting

Landform: Kame terraces, outwash plains, moraines, outwash deltas, kames, eskers, outwash terraces

Landform position (two-dimensional): Shoulder, toeslope, footslope, backslope

Landform position (three-dimensional): Nose slope, side slope, crest, head slope, riser

Down-slope shape: Linear, convex, concave

Across-slope shape: Convex, linear, concave

Parent material: Sandy and gravelly glaciofluvial deposits derived from gneiss and/or granite and/or schist

Typical profile

Oe - 0 to 1 inches: moderately decomposed plant material

A - 1 to 8 inches: loamy sand

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Bw1 - 8 to 11 inches: gravelly loamy sand
Bw2 - 11 to 16 inches: gravelly loamy sand
BC - 16 to 19 inches: very gravelly loamy sand
C - 19 to 65 inches: very gravelly sand

Properties and qualities

Slope: 8 to 15 percent
Depth to restrictive feature: More than 80 inches
Natural drainage class: Excessively drained
Runoff class: Very low
Capacity of the most limiting layer to transmit water (Ksat): Moderately high to very high (1.42 to 99.90 in/hr)
Depth to water table: More than 80 inches
Frequency of flooding: None
Frequency of ponding: None
Salinity, maximum in profile: Nonsaline (0.0 to 1.9 mmhos/cm)
Available water storage in profile: Low (about 3.1 inches)

Interpretive groups

Land capability classification (irrigated): None specified
Land capability classification (nonirrigated): 4e
Hydrologic Soil Group: A
Hydric soil rating: No

Minor Components

Merrimac

Percent of map unit: 5 percent
Landform: Eskers, outwash terraces, kames, moraines, outwash plains
Landform position (two-dimensional): Shoulder, backslope, footslope, toeslope
Landform position (three-dimensional): Side slope, head slope, nose slope, crest, riser
Down-slope shape: Convex
Across-slope shape: Convex
Hydric soil rating: No

Windsor

Percent of map unit: 5 percent
Landform: Outwash deltas, moraines, outwash terraces, eskers, kame terraces, kames, outwash plains
Landform position (two-dimensional): Shoulder, backslope, footslope, toeslope
Landform position (three-dimensional): Nose slope, side slope, crest, head slope, riser
Down-slope shape: Convex, concave, linear
Across-slope shape: Concave, linear, convex
Hydric soil rating: No

Sudbury

Percent of map unit: 5 percent
Landform: Moraines, outwash deltas, outwash terraces, kame terraces, outwash plains
Landform position (two-dimensional): Backslope, footslope
Landform position (three-dimensional): Base slope, tread
Down-slope shape: Concave, linear
Across-slope shape: Linear, concave
Hydric soil rating: No

253D—Hinckley loamy sand, 15 to 25 percent slopes

Map Unit Setting

National map unit symbol: 2svmc
Elevation: 0 to 1,460 feet
Mean annual precipitation: 36 to 71 inches
Mean annual air temperature: 39 to 55 degrees F
Frost-free period: 140 to 240 days
Farmland classification: Not prime farmland

Map Unit Composition

Hinckley and similar soils: 85 percent
Minor components: 15 percent
Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Hinckley

Setting

Landform: Outwash plains, moraines, outwash deltas, kame terraces, kames, eskers, outwash terraces
Landform position (two-dimensional): Backslope
Landform position (three-dimensional): Nose slope, side slope, crest, head slope, riser
Down-slope shape: Convex, linear, concave
Across-slope shape: Linear, convex, concave
Parent material: Sandy and gravelly glaciofluvial deposits derived from gneiss and/or granite and/or schist

Typical profile

Oe - 0 to 1 inches: moderately decomposed plant material
A - 1 to 8 inches: loamy sand
Bw1 - 8 to 11 inches: gravelly loamy sand
Bw2 - 11 to 16 inches: gravelly loamy sand
BC - 16 to 19 inches: very gravelly loamy sand
C - 19 to 65 inches: very gravelly sand

Properties and qualities

Slope: 15 to 25 percent
Depth to restrictive feature: More than 80 inches
Natural drainage class: Excessively drained
Runoff class: Low
Capacity of the most limiting layer to transmit water (Ksat): Moderately high to very high (1.42 to 99.90 in/hr)
Depth to water table: More than 80 inches
Frequency of flooding: None
Frequency of ponding: None
Salinity, maximum in profile: Nonsaline (0.0 to 1.9 mmhos/cm)
Available water storage in profile: Low (about 3.1 inches)

Interpretive groups

Land capability classification (irrigated): None specified
Land capability classification (nonirrigated): 6e
Hydrologic Soil Group: A
Hydric soil rating: No

Minor Components

Merrimac

Percent of map unit: 8 percent
Landform: Outwash terraces, eskers, kames, moraines, outwash plains
Landform position (two-dimensional): Backslope
Landform position (three-dimensional): Side slope, crest, head slope, nose slope, riser
Down-slope shape: Convex
Across-slope shape: Convex
Hydric soil rating: No

Windsor

Percent of map unit: 5 percent
Landform: Moraines, kame terraces, outwash terraces, eskers, kames, outwash plains, outwash deltas
Landform position (two-dimensional): Backslope
Landform position (three-dimensional): Nose slope, side slope, crest, head slope, riser
Down-slope shape: Convex, linear, concave
Across-slope shape: Linear, convex, concave
Hydric soil rating: No

Sudbury

Percent of map unit: 2 percent
Landform: Moraines, outwash deltas, kame terraces, outwash terraces, eskers, outwash plains
Landform position (two-dimensional): Backslope, footslope
Landform position (three-dimensional): Base slope, tread
Down-slope shape: Concave, linear, convex
Across-slope shape: Linear, concave, convex
Hydric soil rating: No

254B—Merrimac fine sandy loam, 3 to 8 percent slopes

Map Unit Setting

National map unit symbol: 2tyqs
Elevation: 0 to 1,290 feet
Mean annual precipitation: 36 to 71 inches
Mean annual air temperature: 39 to 55 degrees F
Frost-free period: 140 to 240 days
Farmland classification: All areas are prime farmland

Map Unit Composition

Merrimac and similar soils: 85 percent

Minor components: 15 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Merrimac

Setting

Landform: Eskers, outwash terraces, kames, moraines, outwash plains

Landform position (two-dimensional): Backslope, footslope, shoulder, summit

Landform position (three-dimensional): Side slope, crest, tread, riser

Down-slope shape: Convex

Across-slope shape: Convex

Parent material: Loamy glaciofluvial deposits derived from granite, schist, and gneiss over sandy and gravelly glaciofluvial deposits derived from granite, schist, and gneiss

Typical profile

Ap - 0 to 10 inches: fine sandy loam

Bw1 - 10 to 22 inches: fine sandy loam

Bw2 - 22 to 26 inches: stratified gravel to gravelly loamy sand

2C - 26 to 65 inches: stratified gravel to very gravelly sand

Properties and qualities

Slope: 3 to 8 percent

Depth to restrictive feature: More than 80 inches

Natural drainage class: Somewhat excessively drained

Runoff class: Very low

Capacity of the most limiting layer to transmit water (Ksat): Moderately high to very high (1.42 to 99.90 in/hr)

Depth to water table: More than 80 inches

Frequency of flooding: None

Frequency of ponding: None

Calcium carbonate, maximum in profile: 2 percent

Salinity, maximum in profile: Nonsaline (0.0 to 1.4 mmhos/cm)

Sodium adsorption ratio, maximum in profile: 1.0

Available water storage in profile: Low (about 4.6 inches)

Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 2s

Hydrologic Soil Group: A

Hydric soil rating: No

Minor Components

Sudbury

Percent of map unit: 5 percent

Landform: Outwash plains, terraces, deltas

Landform position (two-dimensional): Footslope

Landform position (three-dimensional): Tread, dip

Down-slope shape: Concave

Across-slope shape: Linear

Hydric soil rating: No

Custom Soil Resource Report

Hinckley

Percent of map unit: 5 percent

Landform: Outwash plains, kames, eskers, deltas

Landform position (two-dimensional): Summit, shoulder, backslope

Landform position (three-dimensional): Head slope, crest, side slope, nose slope, rise

Down-slope shape: Convex

Across-slope shape: Linear, convex

Hydric soil rating: No

Windsor

Percent of map unit: 3 percent

Landform: Dunes, deltas, outwash terraces, outwash plains

Landform position (two-dimensional): Shoulder

Landform position (three-dimensional): Tread, riser

Down-slope shape: Convex, linear

Across-slope shape: Convex, linear

Hydric soil rating: No

Agawam

Percent of map unit: 2 percent

Landform: Moraines, outwash plains, stream terraces, kames, eskers, outwash terraces

Landform position (three-dimensional): Rise

Down-slope shape: Convex

Across-slope shape: Convex

Hydric soil rating: No

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Custom Soil Resource Report

United States Department of Agriculture, Natural Resources Conservation Service. National soil survey handbook, title 430-VI. http://www.nrcs.usda.gov/wps/portal/nrcs/detail/soils/scientists/?cid=nrcs142p2_054242

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Appendix B – Test Pit Results



COLD SPRING ENVIRONMENTAL CONSULTANTS INC.

- 2IE Site Investigations
- Subsurface Investigations
- Pollution Remediation
- LSP on Staff
- Forensic Septic Investigations

- Percolation Tests
- Septic Designs
- Regulatory Compliance
- Recycling and Solid Waste
- Second Opinions

December 14, 2020

Lucy Conley, P.E.
The Berkshire Design Group, Inc,
4 Allen Place
Northampton, MA 01060

RE: Soil Evaluations 18-20 & 22 Amherst Road. Pelham, MA

Greetings,

The soil evaluations TP-1 through TP-4 were requested by you and performed by us on December 3, 2020 at the abovementioned property. The excavations were conducted at the locations that you provided on the site Plan, Excavation TP-5 was not completed as subsurface utility locations were interpreted as to close.

The soil evaluation attached (and photos) confirmed the existence of deep, Class A & B (Class 1 & 2) gravelly and stoney coarse sandy substrata to a depth of more than 9 feet below grade and shallow Estimated Seasonal High Groundwater conditions ranged from 58" (TP-4) to 108" (TP-2) below grade. Class 1 Coarse sandy stony stream terrace and outwash was observed in TP-1 through TP-4.

These conditions are consistent with the East to West Stream Terrace slopes along Fort Brook in this portion of Pioneer Valley. Form 11 Soil evaluations are attached. Mass Gis notes the Surficial Geology to consist of Stratified Glacial Deposits. NRCS Maps denote Hinkley Loamy Sand (253B) Soils.

Please feel free to contact me with any questions or further evaluation

Sincerely,

Cold Spring Environmental Consultants, Inc.

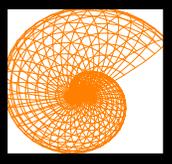
Alan E. Weiss, M.S., R.S., L.S.P.

Licensed Soil Evaluator # 2568, since 1995

Principal Hydrogeologist

Massachusetts Public Health Sanitarian Lic. #933

Attachments: Figures, Photos and Soil reports.



Cold Spring Environmental Consultants, Inc.

350 Old Enfield Road
Belchertown, MA 01007
<http://www.coldspringenvironmental.com>

Ph: 413.323.5957
Fax: 413.323.4916
email: acweis@charter.net

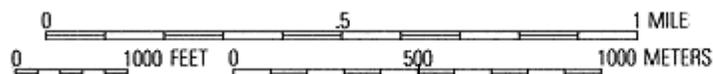
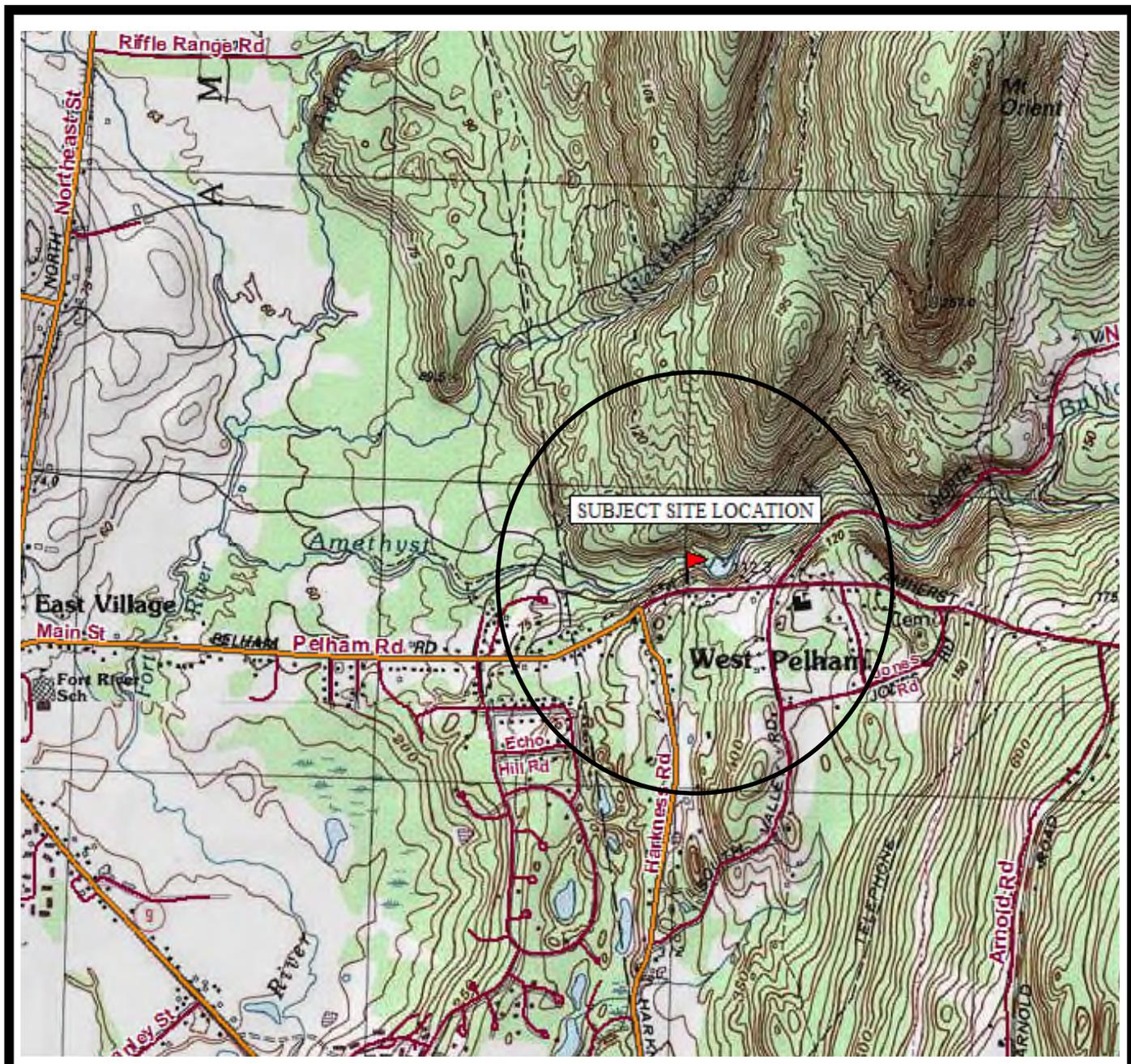


FIGURE 1—SITE LOCUS
18-22 Amherst Road
Pelham, MA

December, 2020

FROM USGS

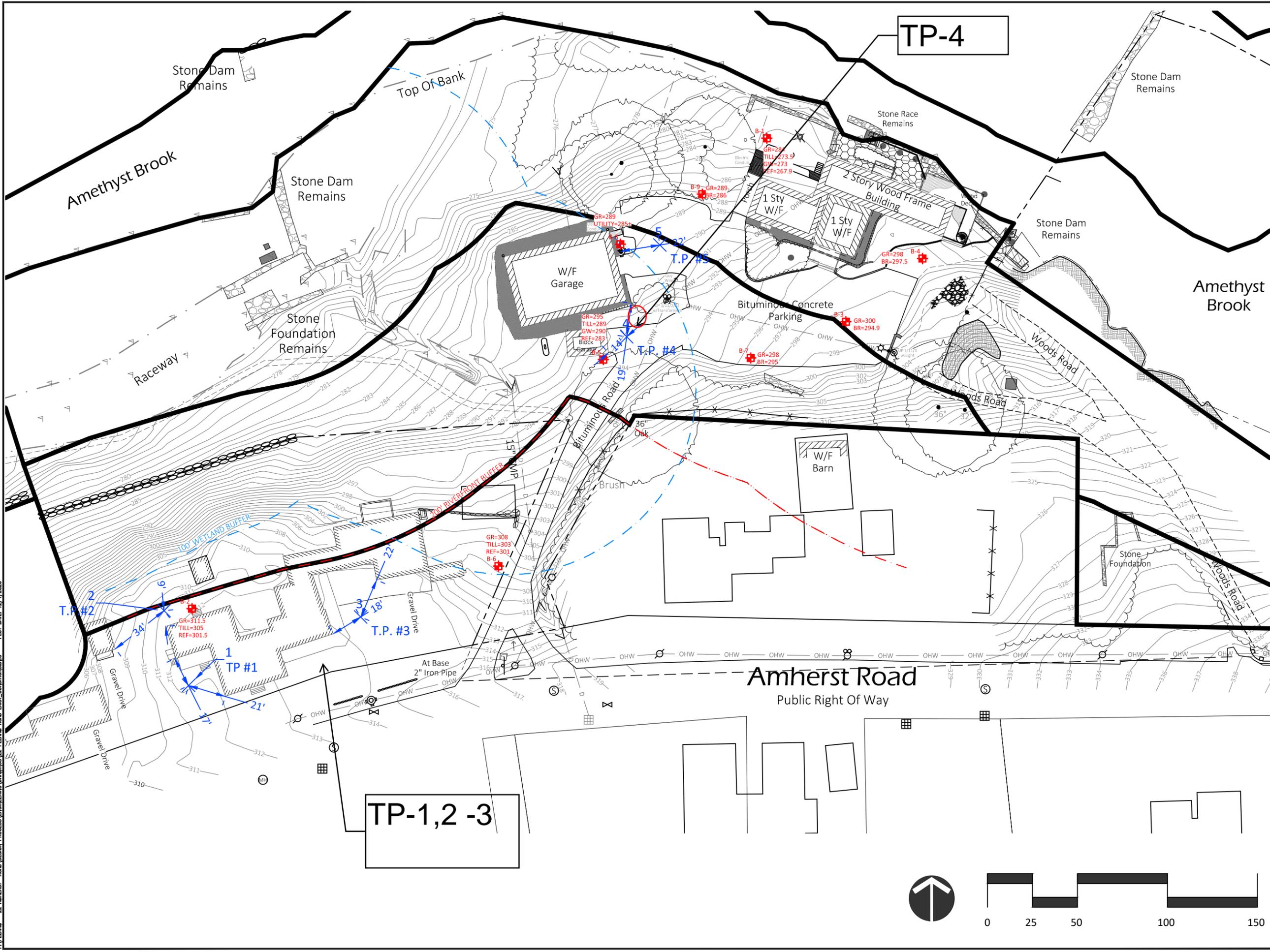
This drawing is not intended nor shall it be used for construction purposes unless the signed professional seal of a registered landscape architect, civil engineer or land surveyor employed by The Berkshire Design Group, Inc. is affixed above.
Do not scale drawing for quantity take-offs or construction. Use written dimensions only. If dimensions are incomplete, contact The Berkshire Design Group Inc. for clarification.
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AMETHYST BROOK APARTMENTS
20-22 AMHERST ROAD
PELHAM, MA

EXISTING CONDITIONS PLAN

Revisions	

Date:	APRIL 17, 2020	Sheet Number	FIG 2
Scale:	1"=50'		
Drawn By:	LMC		
Checked By:	MBD		



TP-4

TP-1,2 -3

F:\PELHAM - 22 AMHERST ROAD\DESIGN PROCESS\ENGINEERING\DRAWINGS\22 PELHAM ROAD EXIST CONDITIONS.DWG PLOT DATE: 12/1/2020



Commonwealth of Massachusetts

City/Town of Pelham

Form 11 - Soil Suitability Assessment for On-Site Sewage Disposal

A. Facility Information

C/O Berkshire Design Group

Owner Name

18-20 Amherst Road

Street Address

Pelham

City

MA

State

3-32

Map/Lot #

01002

Zip Code

B. Site Information

- (Check one) New Construction Upgrade Repair
- Soil Survey Available? Yes No If yes: Cal web USDA 253B
Source Soil Map Unit
Hinckley Loamy Sand
Soil Name
- Soil Limitations
- Surficial Geological Report Available? Yes No If yes: USGS current gis
Year Published/Source Publication Scale Map Unit
Stoney, Granular Stream Outwash
Geologic/Parent Material Stream Terrace
Landform
- Flood Rate Insurance Map
Above the 500-year flood boundary? Yes No Within the 100-year flood boundary? Yes No
Within the 500-year flood boundary? Yes No Within a velocity zone? Yes No
- Wetland Area: Wetlands Conservancy Program Map -
Map Unit Name
- Current Water Resource Conditions (USGS): Month/Year Range: Above Normal Normal Below Normal
- Other references reviewed: _____



Commonwealth of Massachusetts

City/Town of Pelham

Form 11 - Soil Suitability Assessment for On-Site Sewage Disposal

C. On-Site Review (minimum of two holes required at every proposed primary and reserved disposal area)

Deep Observation Hole Number: 1, 2 and 3 Date: 12.3.2020 Time: 1300 Weather: -

1. Location

Ground Elevation at Surface of Hole: shown Location (identify on plan): -

2. Land Use: grassy (e.g., woodland, agricultural field, vacant lot, etc.) no Surface Stones 2 Slope (%) deciduous mix Vegetation terrace Landform shown Position on Landscape (attach sheet)

3. Distances from: Open Water Body 100'+ feet Drainage Way 100'+ feet Possible Wet Area 50'+ feet Property Line 20'+ feet Drinking Water Well 100'+ feet Other - feet

4. Parent Material: Outwash Unsuitable Materials Present: Yes No

If Yes: Disturbed Soil Fill Material Impervious Layer(s) Weathered/Fractured Rock Bedrock

5. Groundwater Observed: Yes No If yes: Not Obs. Depth Weeping from Pit Not Obs. Depth Standing Water in Hole

Estimated Depth to High Groundwater: 80-108"+ inches elevation



Commonwealth of Massachusetts

City/Town of Pelham

Form 11 - Soil Suitability Assessment for On-Site Sewage Disposal

C. On-Site Review (continued)

Deep Observation Hole Number: 1 & 2

Depth (in.)	Soil Horizon/ Layer	Soil Matrix: Color- Moist (Munsell)	Redoximorphic Features (mottles)			Soil Texture (USDA)	Coarse Fragments % by Volume		Soil Structure	Soil Consistence (Moist)	Other
			Depth	Color	Percent		Gravel	Cobbles & Stones			
0-10"	A	10 YR 3.2				FSL			FRIABLE		mixed
10-28"	Bw	10 YR 5.6				FS				Old	System
28-80"	C1	2.5 y 5.6	-	-	-	CS	10	25	Granular	Bouldery	Outwash
Large	Rock	at 80"									
0-48"	fill	10 YR 5.8				FS					Disturbed
48-108"	C	2.5 Y 5.6	-	-	-	CS	10	25	Granular	Bouldery	Outwash

Additional Notes:



Commonwealth of Massachusetts

City/Town of Pelham

Form 11 - Soil Suitability Assessment for On-Site Sewage Disposal

C. On-Site Review (continued)

Deep Observation Hole Number: 3

Depth (in.)	Soil Horizon/ Layer	Soil Matrix: Color- Moist (Munsell)	Redoximorphic Features (mottles)			Soil Texture (USDA)	Coarse Fragments % by Volume		Soil Structure	Soil Consistence (Moist)	Other
			Depth	Color	Percent		Gravel	Cobbles & Stones			
0-12"	A	10 YR 3.2				FSL					
12-26"	B	10 YR 5.6				FS					
26-96"	C	2.5 y 5.6	-	-	-	CS	10	25	Granular	Bouldery	Outwash

Additional Notes:



Commonwealth of Massachusetts

City/Town of Pelham

Form 11 - Soil Suitability Assessment for On-Site Sewage Disposal

D. Determination of High Groundwater Elevation

1. Method Used:

- Depth observed standing water in observation hole A. not _____ inches B. not _____ inches
- Depth weeping from side of observation hole A. not _____ inches B. not _____ inches
- Depth to soil redoximorphic features (mottles) A. 80-108"+ _____ inches B. 80-108"+ _____ inches
- Groundwater adjustment (USGS methodology) A. _____ inches B. _____ inches

2.

Index Well Number _____ Reading Date _____ Index Well Level _____

Adjustment Factor _____ Adjusted Groundwater Level _____

E. Depth of Pervious Material

1. Depth of Naturally Occurring Pervious Material

a. Does at least four feet of naturally occurring pervious material exist in all areas observed throughout the area proposed for the soil absorption system?

- Yes No

b. If yes, at what depth was it observed? Upper boundary: 48 inches Lower boundary: 80-108" inches



Commonwealth of Massachusetts

City/Town of Pelham

Form 11 - Soil Suitability Assessment for On-Site Sewage Disposal

F. Certification

I certify that I am currently approved by the Department of Environmental Protection pursuant to 310 CMR 15.017 to conduct soil evaluations and that the above analysis has been performed by me consistent with the required training, expertise and experience described in 310 CMR 15.017. I further certify that the results of my soil evaluation, as indicated in the attached Soil Evaluation Form, are accurate and in accordance with 310 CMR 15.100 through 15.107.

Signature of Soil Evaluator

ALAN WEISS, RS #933, SE #2568, Cold Spring Env. Inc.

Typed or Printed Name of Soil Evaluator / License #

-

Name of Board of Health Witness

12/01/2020

Date

6/1995

Date of Soil Evaluator Exam

Board of Health

Note: In accordance with 310 CMR 15.018(2) this form must be submitted to the approving authority within 60 days of the date of field testing, and to the designer and the property owner with [Percolation Test Form 12](#).



Commonwealth of Massachusetts

City/Town of Pelham

Form 11 - Soil Suitability Assessment for On-Site Sewage Disposal

A. Facility Information

C/O Berkshire Design Group

Owner Name

220 Amherst Road

Street Address

Pelham

City

MA

State

3-30

Map/Lot #

01002

Zip Code

B. Site Information

- (Check one) New Construction Upgrade Repair
- Soil Survey Available? Yes No If yes: Cal web USDA 253B
Source Soil Map Unit
Hinckley Loamy Sand
Soil Name
- Surficial Geological Report Available? Yes No If yes: USGS current gis
Year Published/Source Publication Scale Map Unit
Stoney, Granular Stream Outwash
Geologic/Parent Material Stream Terrace
Landform
- Flood Rate Insurance Map
Above the 500-year flood boundary? Yes No Within the 100-year flood boundary? Yes No
Within the 500-year flood boundary? Yes No Within a velocity zone? Yes No
- Wetland Area: Wetlands Conservancy Program Map -
Map Unit Name
- Current Water Resource Conditions (USGS): Month/Year Range: Above Normal Normal Below Normal
- Other references reviewed: _____



Commonwealth of Massachusetts

City/Town of Pelham

Form 11 - Soil Suitability Assessment for On-Site Sewage Disposal

C. On-Site Review (minimum of two holes required at every proposed primary and reserved disposal area)

Deep Observation Hole Number: TP-4 Date: 12.3.2020 Time: 1300 Weather: -

1. Location

Ground Elevation at Surface of Hole: shown Location (identify on plan): -

2. Land Use: grassy (e.g., woodland, agricultural field, vacant lot, etc.) no Surface Stones 5 Slope (%) deciduous mix Vegetation terrace Landform shown Position on Landscape (attach sheet)

3. Distances from: Open Water Body 100'+ feet Drainage Way 100'+ feet Possible Wet Area 50'+ feet Property Line 20'+ feet Drinking Water Well 100'+ feet Other - feet

4. Parent Material: Outwash Unsuitable Materials Present: [] Yes [x] No

If Yes: [] Disturbed Soil [] Fill Material [] Impervious Layer(s) [] Weathered/Fractured Rock [] Bedrock

5. Groundwater Observed: [x] Yes [] No If yes: 76" Depth Weeping from Pit - Depth Standing Water in Hole

Estimated Depth to High Groundwater: 58"+ inches elevation



Commonwealth of Massachusetts

City/Town of Pelham

Form 11 - Soil Suitability Assessment for On-Site Sewage Disposal

C. On-Site Review (continued)

Deep Observation Hole Number: TP-4

Depth (in.)	Soil Horizon/ Layer	Soil Matrix: Color- Moist (Munsell)	Redoximorphic Features (mottles)			Soil Texture (USDA)	Coarse Fragments % by Volume		Soil Structure	Soil Consistence (Moist)	Other
			Depth	Color	Percent		Gravel	Cobbles & Stones			
0-36"	Fill	10 YR 3.2				FSL					Disturbed
36-110"	C1	2.5 Y5.6	58"	10YR2.2	10	CS	10	10	Granular	Bouldery	Outwash

Additional Notes:



Commonwealth of Massachusetts

City/Town of Pelham

Form 11 - Soil Suitability Assessment for On-Site Sewage Disposal

D. Determination of High Groundwater Elevation

1. Method Used:

- Depth observed standing water in observation hole A. not _____ inches B. not _____ inches
- Depth weeping from side of observation hole A. 76" _____ inches B. not _____ inches
- Depth to soil redoximorphic features (mottles) A. 58"+ _____ inches B. not _____ inches
- Groundwater adjustment (USGS methodology) A. _____ inches B. _____ inches

2.

Index Well Number _____ Reading Date _____ Index Well Level _____

Adjustment Factor _____ Adjusted Groundwater Level _____

E. Depth of Pervious Material

1. Depth of Naturally Occurring Pervious Material

a. Does at least four feet of naturally occurring pervious material exist in all areas observed throughout the area proposed for the soil absorption system?

- Yes No

b. If yes, at what depth was it observed? Upper boundary: 36" _____ inches Lower boundary: 110" _____ inches



Commonwealth of Massachusetts

City/Town of Pelham

Form 11 - Soil Suitability Assessment for On-Site Sewage Disposal

F. Certification

I certify that I am currently approved by the Department of Environmental Protection pursuant to 310 CMR 15.017 to conduct soil evaluations and that the above analysis has been performed by me consistent with the required training, expertise and experience described in 310 CMR 15.017. I further certify that the results of my soil evaluation, as indicated in the attached Soil Evaluation Form, are accurate and in accordance with 310 CMR 15.100 through 15.107.

Signature of Soil Evaluator

ALAN WEISS, RS #933, SE #2568, Cold Spring Env. Inc.

Typed or Printed Name of Soil Evaluator / License #

-

Name of Board of Health Witness

12/01/2020

Date

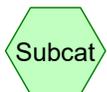
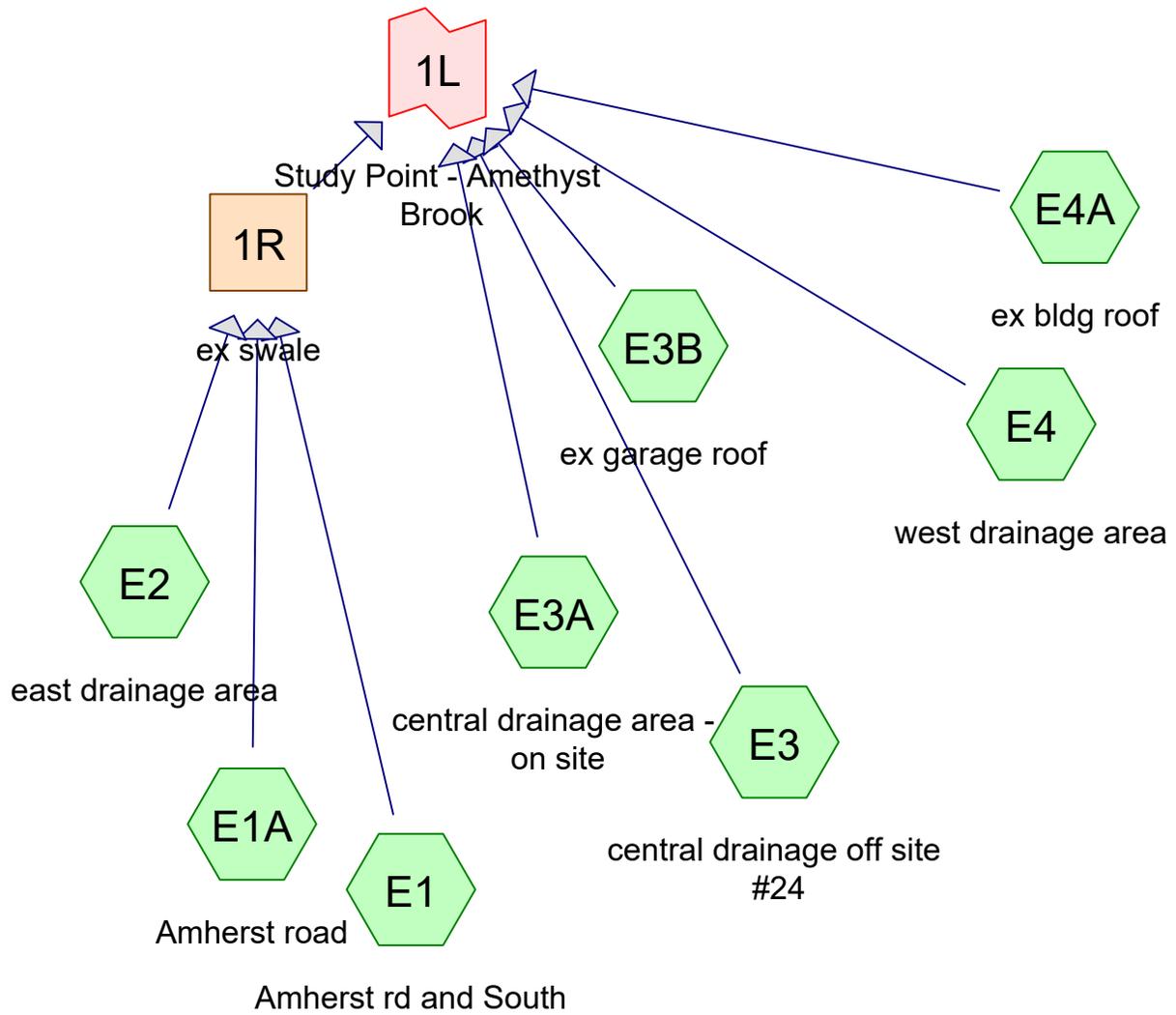
6/1995

Date of Soil Evaluator Exam

Board of Health

Note: In accordance with 310 CMR 15.018(2) this form must be submitted to the approving authority within 60 days of the date of field testing, and to the designer and the property owner with [Percolation Test Form 12](#).

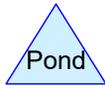
Appendix C – Stormwater Hydrology Calculations



Subcat



Reach



Pond



Link

Routing Diagram for 20.024 EXIST REV
 Prepared by Berkshire Design Group, Printed 12/14/2020
 HydroCAD® 10.00-24 s/n 10759 © 2018 HydroCAD Software Solutions LLC

20.024 EXIST REV

Prepared by Berkshire Design Group

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Page 2

Project Notes

Rainfall events imported from "NRCS-Rain.txt" for 4007 MA Amherst Hampshire County

20.024 EXIST REV

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Page 3

Area Listing (all nodes)

Area (acres)	CN	Description (subcatchment-numbers)
0.706	49	50-75% Grass cover, Fair, HSG A (E1, E1A, E2, E3, E3A, E4A)
0.038	49	Drip edge around buildings (E3A)
0.028	96	Gravel surface, HSG A (E2)
1.128	98	Paved parking, HSG A (E1, E1A, E2, E3, E3A, E4, E4A)
0.019	98	Paved parking, HSG B (E1)
0.056	98	Roofs, HSG A (E3B)
2.791	36	Woods, Fair, HSG A (E1, E2, E3, E3A, E4)
0.704	60	Woods, Fair, HSG B (E1)
5.469	55	TOTAL AREA

20.024 EXIST REV

Prepared by Berkshire Design Group

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Page 4

Soil Listing (all nodes)

Area (acres)	Soil Group	Subcatchment Numbers
4.709	HSG A	E1, E1A, E2, E3, E3A, E3B, E4, E4A
0.722	HSG B	E1
0.000	HSG C	
0.000	HSG D	
0.038	Other	E3A
5.469		TOTAL AREA

20.024 EXIST REV

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Page 5

Ground Covers (all nodes)

HSG-A (acres)	HSG-B (acres)	HSG-C (acres)	HSG-D (acres)	Other (acres)	Total (acres)	Ground Cover	Subcatchment Numbers
0.706	0.000	0.000	0.000	0.000	0.706	50-75% Grass cover, Fair	E1, E1A, E2, E3, E3A, E4A
0.000	0.000	0.000	0.000	0.038	0.038	Drip edge around buildings	E3A
0.028	0.000	0.000	0.000	0.000	0.028	Gravel surface	E2
1.128	0.019	0.000	0.000	0.000	1.146	Paved parking	E1, E1A, E2, E3, E3A, E4, E4A
0.056	0.000	0.000	0.000	0.000	0.056	Roofs	E3B
2.791	0.704	0.000	0.000	0.000	3.495	Woods, Fair	E1, E2, E3, E3A, E4
4.709	0.722	0.000	0.000	0.038	5.469	TOTAL AREA	

20.024 EXIST REV

Prepared by Berkshire Design Group

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NRCC 24-hr C 2-Year Rainfall=3.07"

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Summary for Subcatchment E1: Amherst rd and South

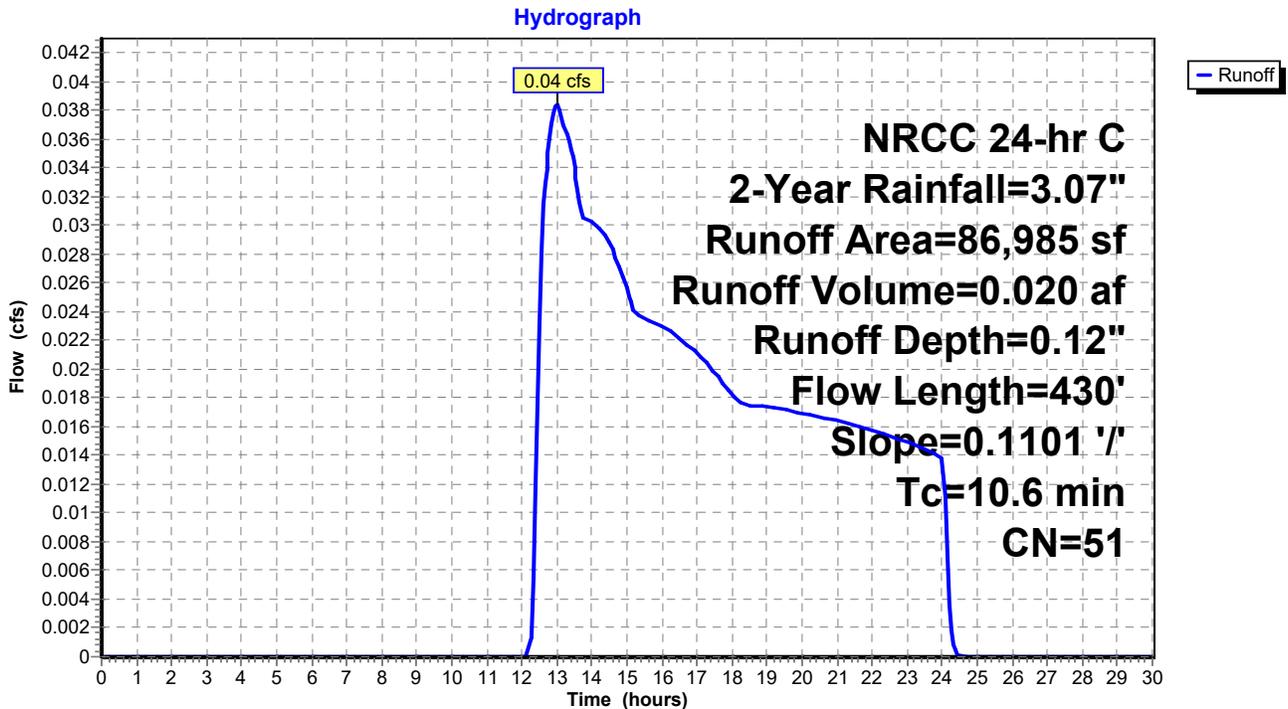
Runoff = 0.04 cfs @ 13.01 hrs, Volume= 0.020 af, Depth= 0.12"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-30.00 hrs, dt= 0.05 hrs
NRCC 24-hr C 2-Year Rainfall=3.07"

Area (sf)	CN	Description
7,024	98	Paved parking, HSG A
806	98	Paved parking, HSG B
39,100	36	Woods, Fair, HSG A
30,655	60	Woods, Fair, HSG B
9,400	49	50-75% Grass cover, Fair, HSG A
86,985	51	Weighted Average
79,155		91.00% Pervious Area
7,830		9.00% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
10.6	430	0.1101	0.68		Lag/CN Method, Contour Length= 9,580' Interval= 1'

Subcatchment E1: Amherst rd and South



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Summary for Subcatchment E1A: Amherst road

[49] Hint: $T_c < 2dt$ may require smaller dt

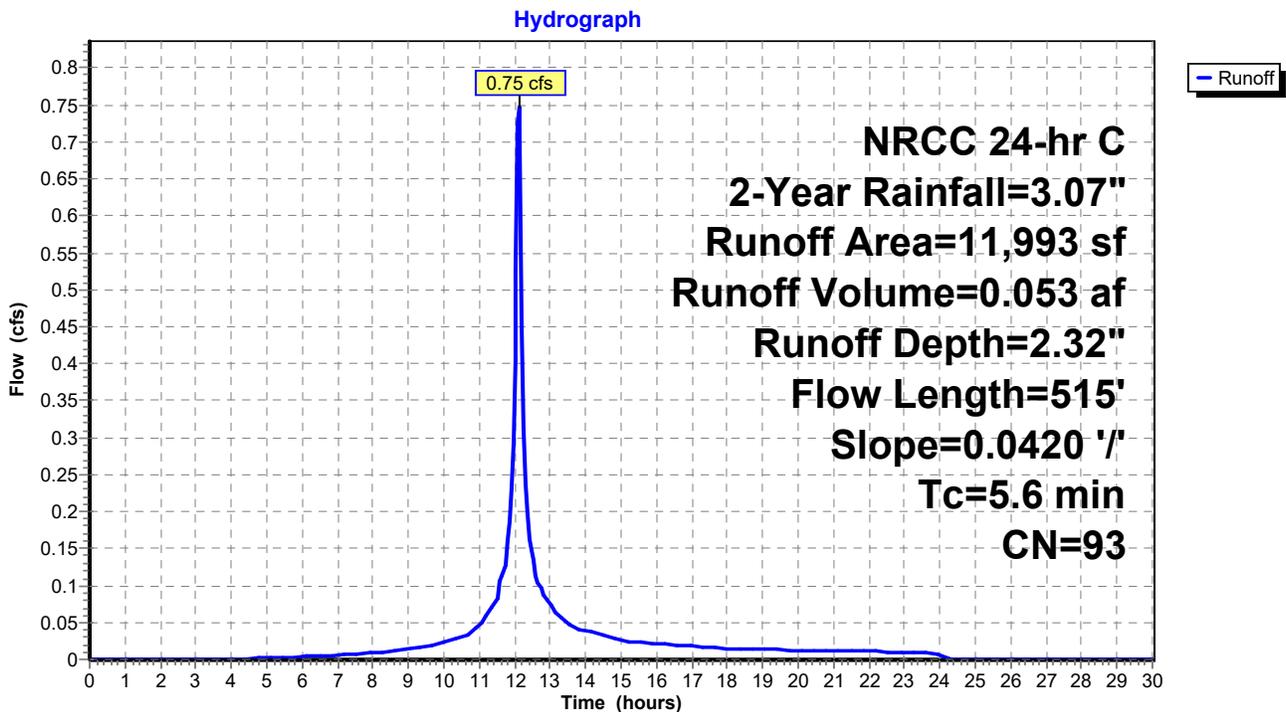
Runoff = 0.75 cfs @ 12.12 hrs, Volume= 0.053 af, Depth= 2.32"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-30.00 hrs, $dt= 0.05$ hrs
 NRCC 24-hr C 2-Year Rainfall=3.07"

Area (sf)	CN	Description
10,800	98	Paved parking, HSG A
1,193	49	50-75% Grass cover, Fair, HSG A
11,993	93	Weighted Average
1,193		9.95% Pervious Area
10,800		90.05% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
5.6	515	0.0420	1.53		Lag/CN Method, Contour Length= 504' Interval= 1'

Subcatchment E1A: Amherst road



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Summary for Subcatchment E2: east drainage area

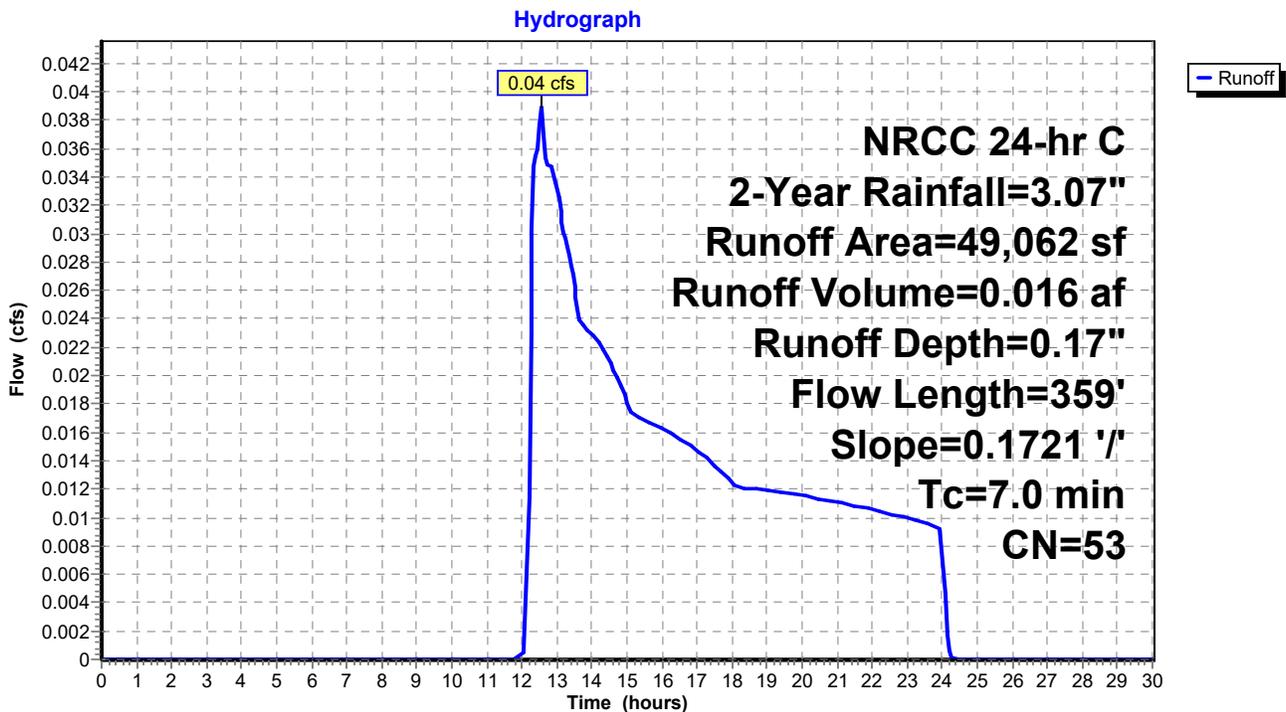
Runoff = 0.04 cfs @ 12.54 hrs, Volume= 0.016 af, Depth= 0.17"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-30.00 hrs, dt= 0.05 hrs
NRCC 24-hr C 2-Year Rainfall=3.07"

Area (sf)	CN	Description
10,891	98	Paved parking, HSG A
31,957	36	Woods, Fair, HSG A
5,000	49	50-75% Grass cover, Fair, HSG A
1,214	96	Gravel surface, HSG A
49,062	53	Weighted Average
38,171		77.80% Pervious Area
10,891		22.20% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
7.0	359	0.1721	0.86		Lag/CN Method, Contour Length= 8,443' Interval= 1'

Subcatchment E2: east drainage area



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Summary for Subcatchment E3: central drainage off site #24

Runoff = 0.00 cfs @ 21.16 hrs, Volume= 0.002 af, Depth= 0.03"

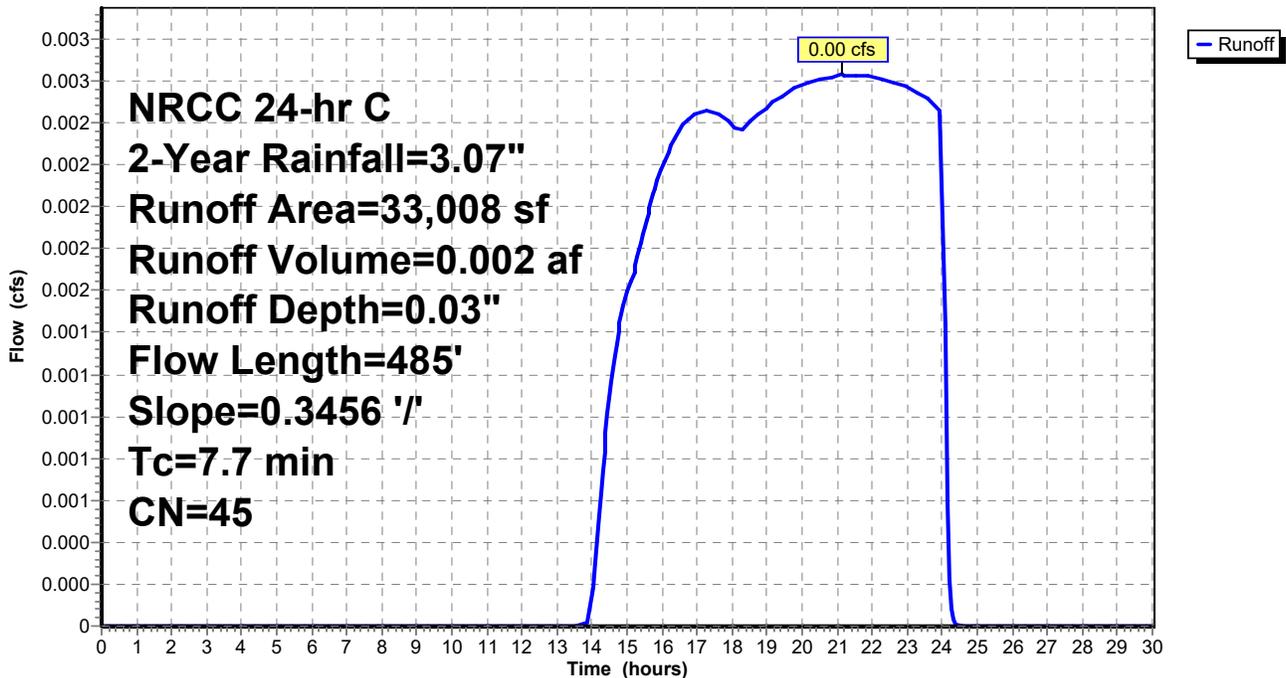
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-30.00 hrs, dt= 0.05 hrs
NRCC 24-hr C 2-Year Rainfall=3.07"

Area (sf)	CN	Description
3,810	98	Paved parking, HSG A
24,198	36	Woods, Fair, HSG A
5,000	49	50-75% Grass cover, Fair, HSG A
33,008	45	Weighted Average
29,198		88.46% Pervious Area
3,810		11.54% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
7.7	485	0.3456	1.05		Lag/CN Method, Contour Length= 11,408' Interval= 1'

Subcatchment E3: central drainage off site #24

Hydrograph



20.024 EXIST REV

Summary for Subcatchment E3A: central drainage area - on site

[49] Hint: $T_c < 2dt$ may require smaller dt

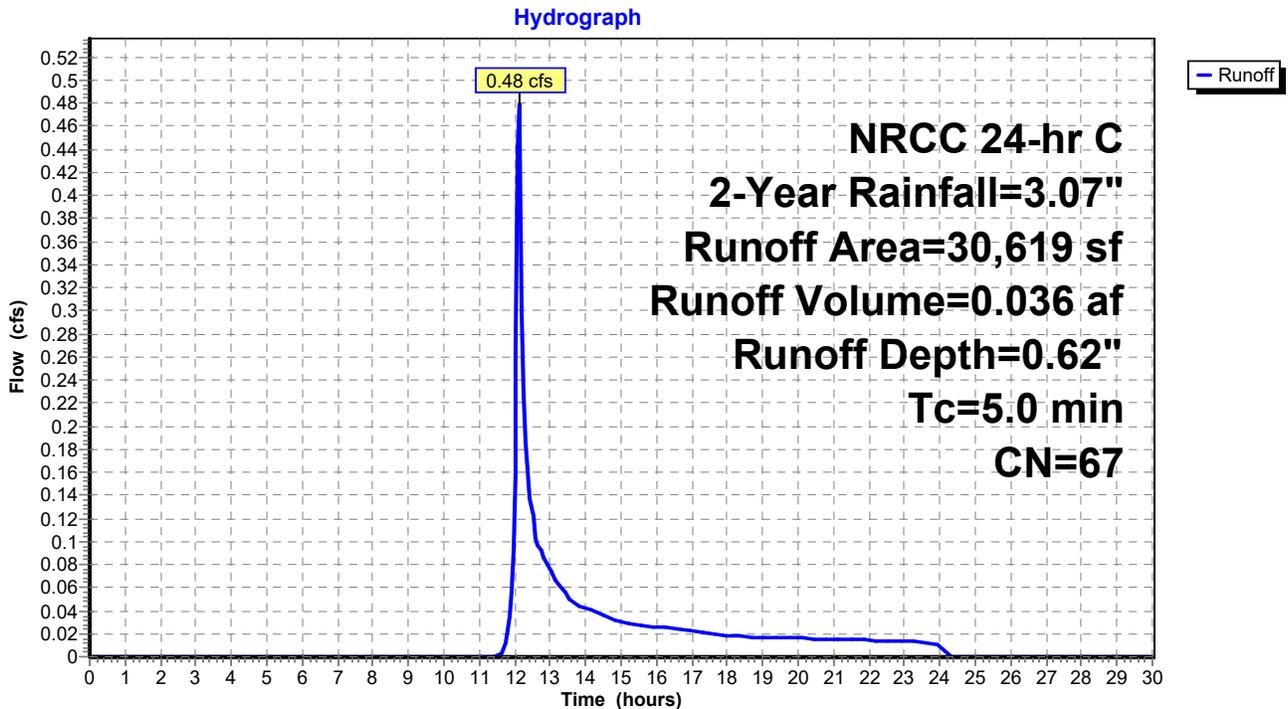
Runoff = 0.48 cfs @ 12.13 hrs, Volume= 0.036 af, Depth= 0.62"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-30.00 hrs, $dt= 0.05$ hrs
 NRCC 24-hr C 2-Year Rainfall=3.07"

Area (sf)	CN	Description
12,631	98	Paved parking, HSG A
10,000	49	50-75% Grass cover, Fair, HSG A
6,338	36	Woods, Fair, HSG A
* 1,650	49	Drip edge around buildings
30,619	67	Weighted Average
17,988		58.75% Pervious Area
12,631		41.25% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
5.0					Direct Entry,

Subcatchment E3A: central drainage area - on site



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NRCC 24-hr C 2-Year Rainfall=3.07"

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Summary for Subcatchment E3B: ex garage roof

[49] Hint: Tc<2dt may require smaller dt

Runoff = 0.18 cfs @ 12.11 hrs, Volume= 0.013 af, Depth= 2.84"

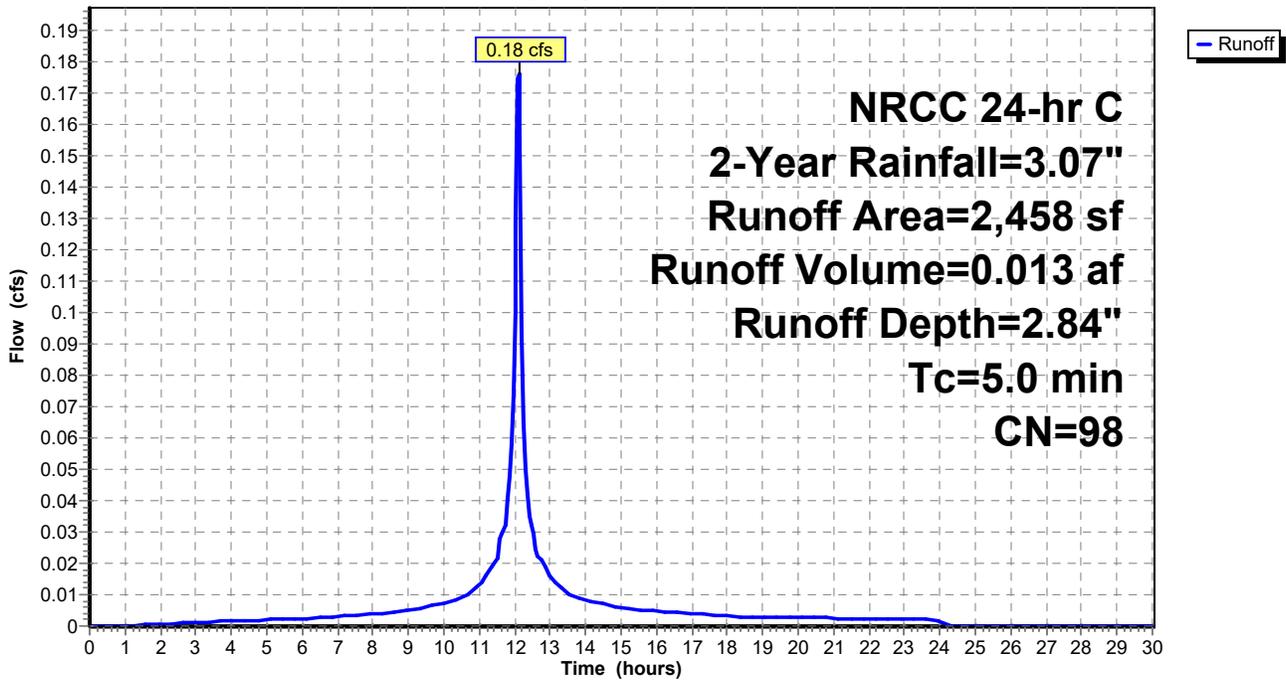
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-30.00 hrs, dt= 0.05 hrs
NRCC 24-hr C 2-Year Rainfall=3.07"

Area (sf)	CN	Description
2,458	98	Roofs, HSG A
2,458		100.00% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
5.0					Direct Entry,

Subcatchment E3B: ex garage roof

Hydrograph



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NRCC 24-hr C 2-Year Rainfall=3.07"

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Summary for Subcatchment E4: west drainage area

[45] Hint: Runoff=Zero

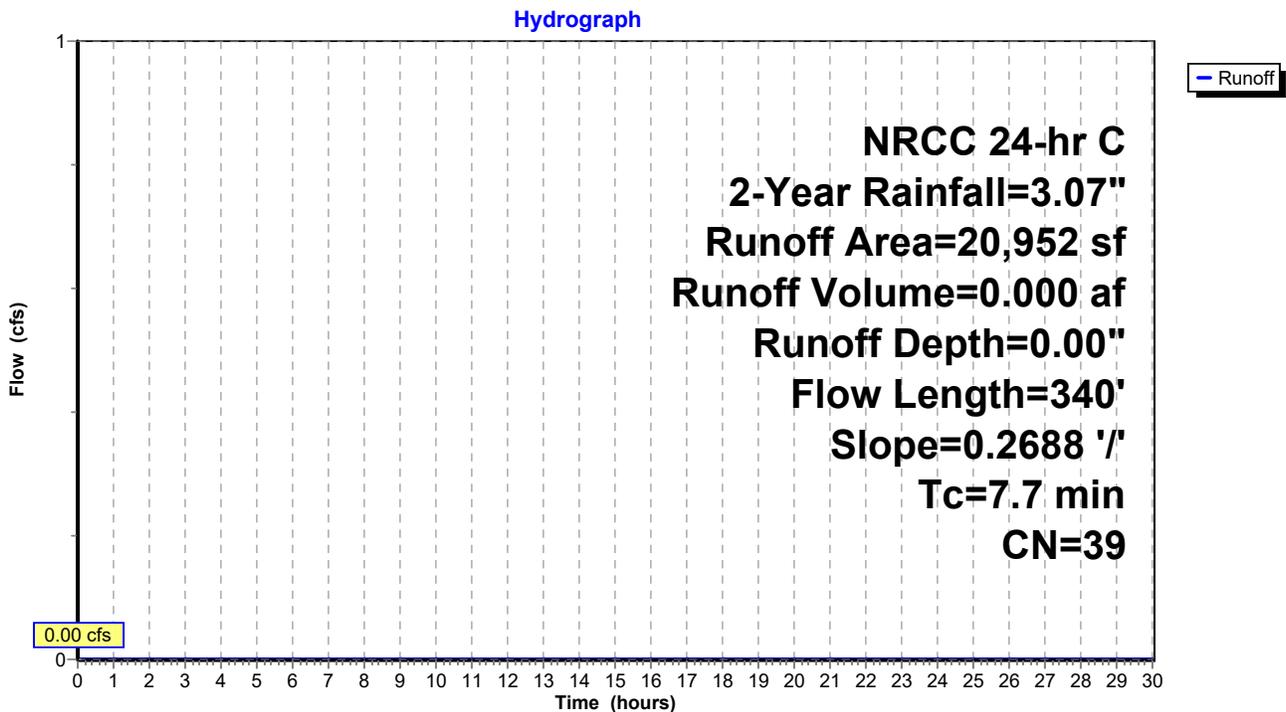
Runoff = 0.00 cfs @ 0.00 hrs, Volume= 0.000 af, Depth= 0.00"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-30.00 hrs, dt= 0.05 hrs
 NRCC 24-hr C 2-Year Rainfall=3.07"

Area (sf)	CN	Description
967	98	Paved parking, HSG A
19,985	36	Woods, Fair, HSG A
20,952	39	Weighted Average
19,985		95.38% Pervious Area
967		4.62% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
7.7	340	0.2688	0.74		Lag/CN Method, Contour Length= 5,632' Interval= 1'

Subcatchment E4: west drainage area



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Summary for Subcatchment E4A: ex bldg roof

[49] Hint: $T_c < 2dt$ may require smaller dt

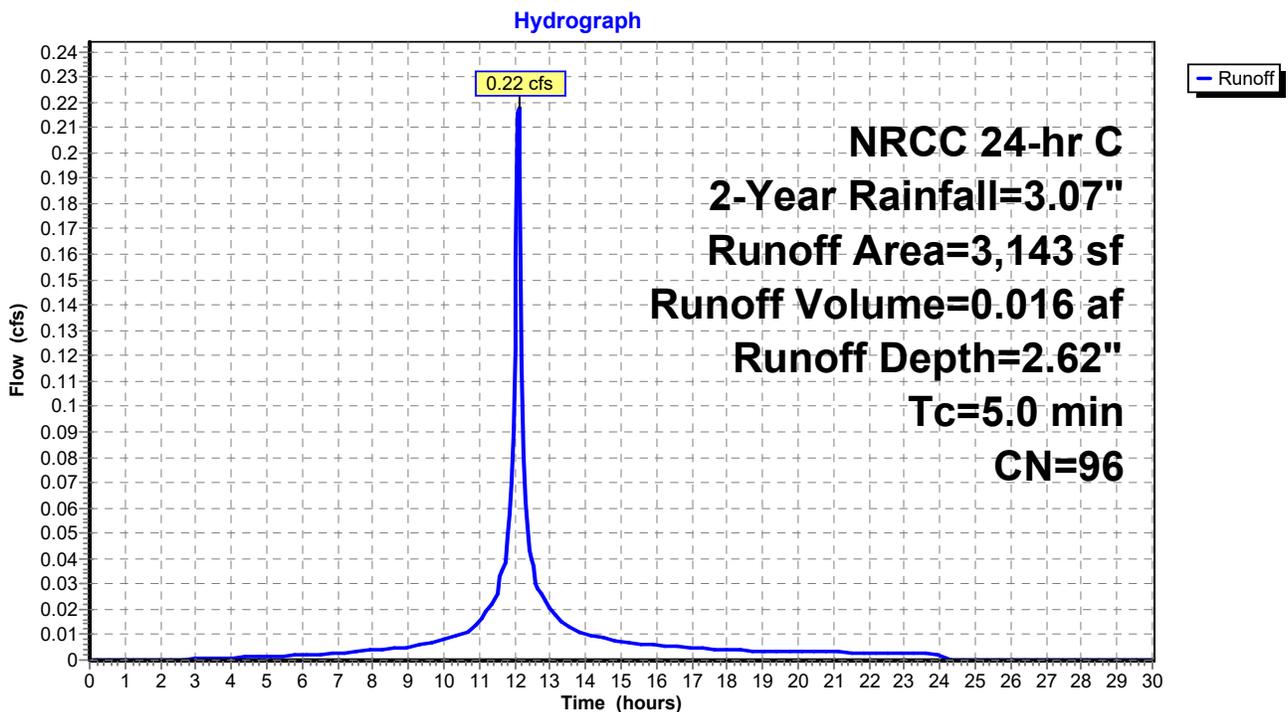
Runoff = 0.22 cfs @ 12.11 hrs, Volume= 0.016 af, Depth= 2.62"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-30.00 hrs, $dt= 0.05$ hrs
 NRCC 24-hr C 2-Year Rainfall=3.07"

Area (sf)	CN	Description
3,000	98	Paved parking, HSG A
143	49	50-75% Grass cover, Fair, HSG A
3,143	96	Weighted Average
143		4.55% Pervious Area
3,000		95.45% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
5.0					Direct Entry,

Subcatchment E4A: ex bldg roof



Summary for Reach 1R: ex swale

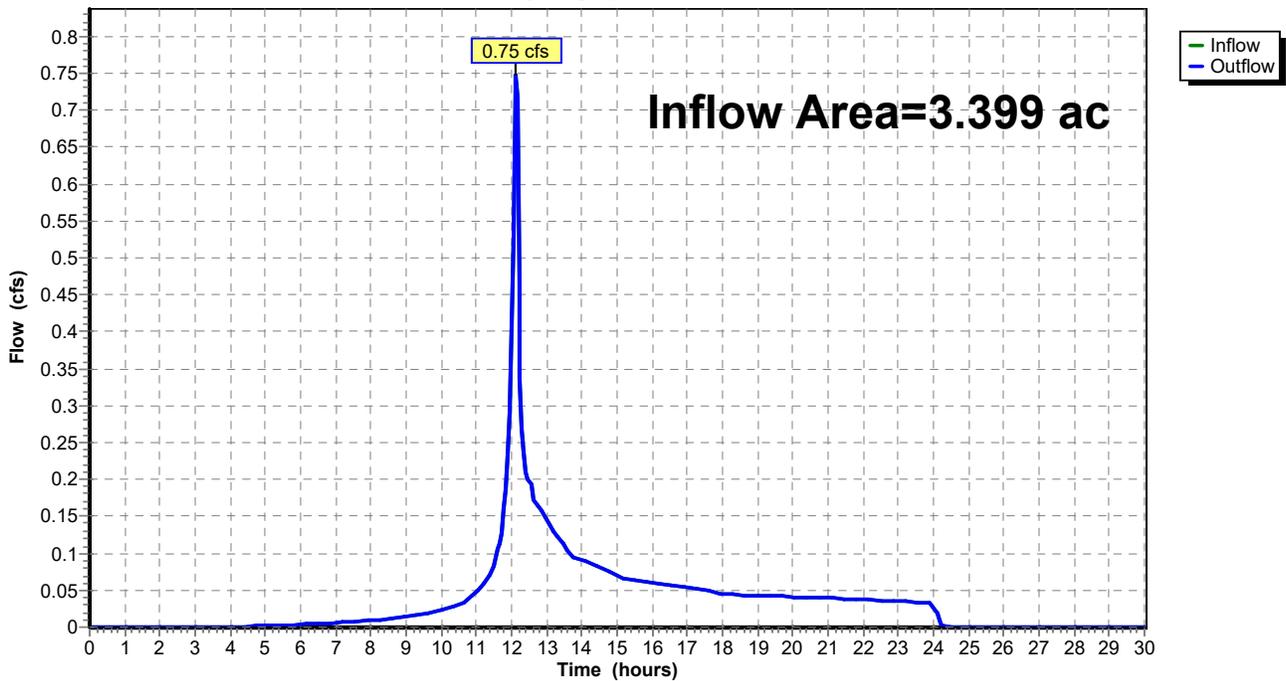
[40] Hint: Not Described (Outflow=Inflow)

Inflow Area = 3.399 ac, 19.94% Impervious, Inflow Depth = 0.31" for 2-Year event
Inflow = 0.75 cfs @ 12.12 hrs, Volume= 0.089 af
Outflow = 0.75 cfs @ 12.12 hrs, Volume= 0.089 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind method, Time Span= 0.00-30.00 hrs, dt= 0.05 hrs

Reach 1R: ex swale

Hydrograph

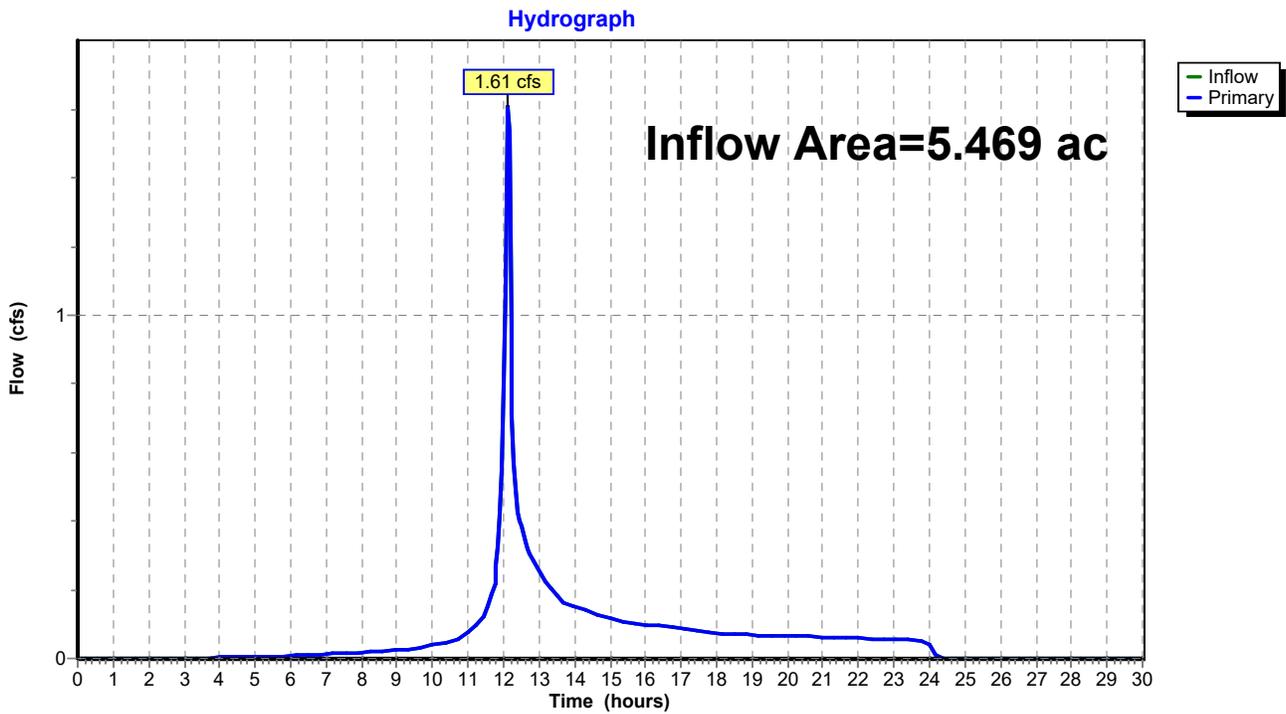


Summary for Link 1L: Study Point - Amethyst Brook

Inflow Area = 5.469 ac, 21.99% Impervious, Inflow Depth = 0.34" for 2-Year event
Inflow = 1.61 cfs @ 12.12 hrs, Volume= 0.157 af
Primary = 1.61 cfs @ 12.12 hrs, Volume= 0.157 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-30.00 hrs, dt= 0.05 hrs

Link 1L: Study Point - Amethyst Brook



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Summary for Subcatchment E1: Amherst rd and South

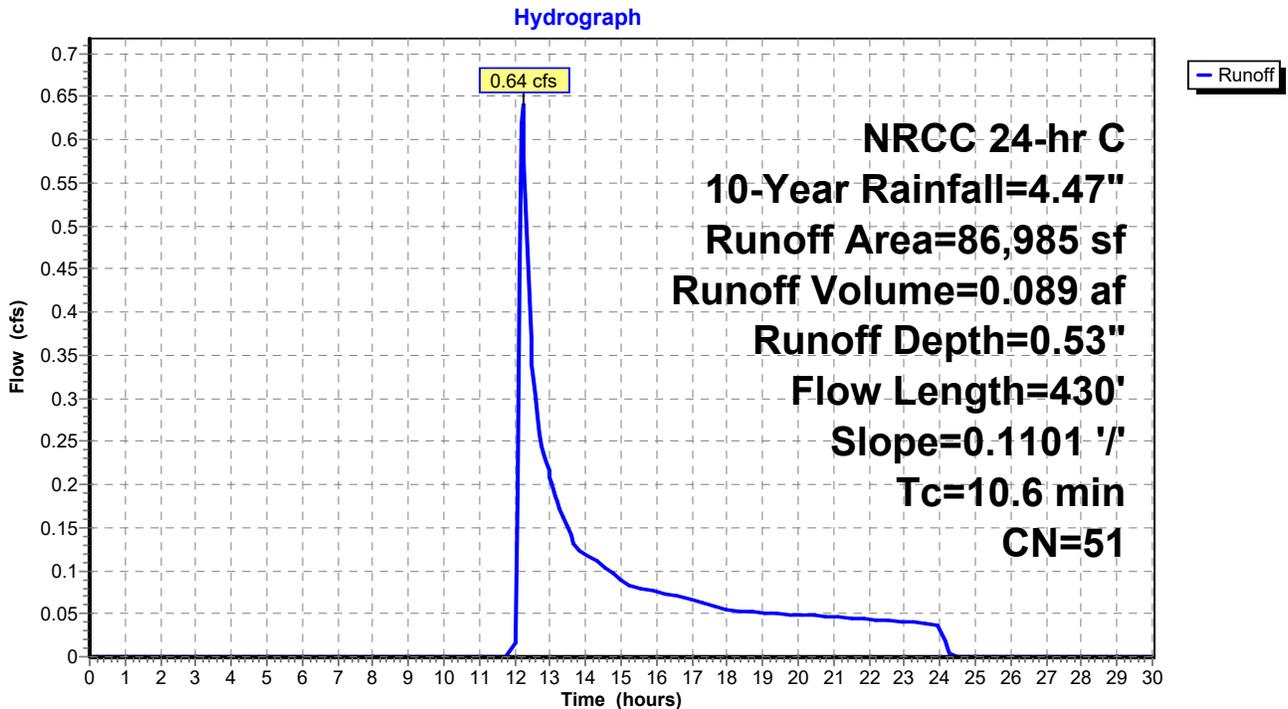
Runoff = 0.64 cfs @ 12.22 hrs, Volume= 0.089 af, Depth= 0.53"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-30.00 hrs, dt= 0.05 hrs
NRCC 24-hr C 10-Year Rainfall=4.47"

Area (sf)	CN	Description
7,024	98	Paved parking, HSG A
806	98	Paved parking, HSG B
39,100	36	Woods, Fair, HSG A
30,655	60	Woods, Fair, HSG B
9,400	49	50-75% Grass cover, Fair, HSG A
86,985	51	Weighted Average
79,155		91.00% Pervious Area
7,830		9.00% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
10.6	430	0.1101	0.68		Lag/CN Method, Contour Length= 9,580' Interval= 1'

Subcatchment E1: Amherst rd and South



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Summary for Subcatchment E1A: Amherst road

[49] Hint: Tc<2dt may require smaller dt

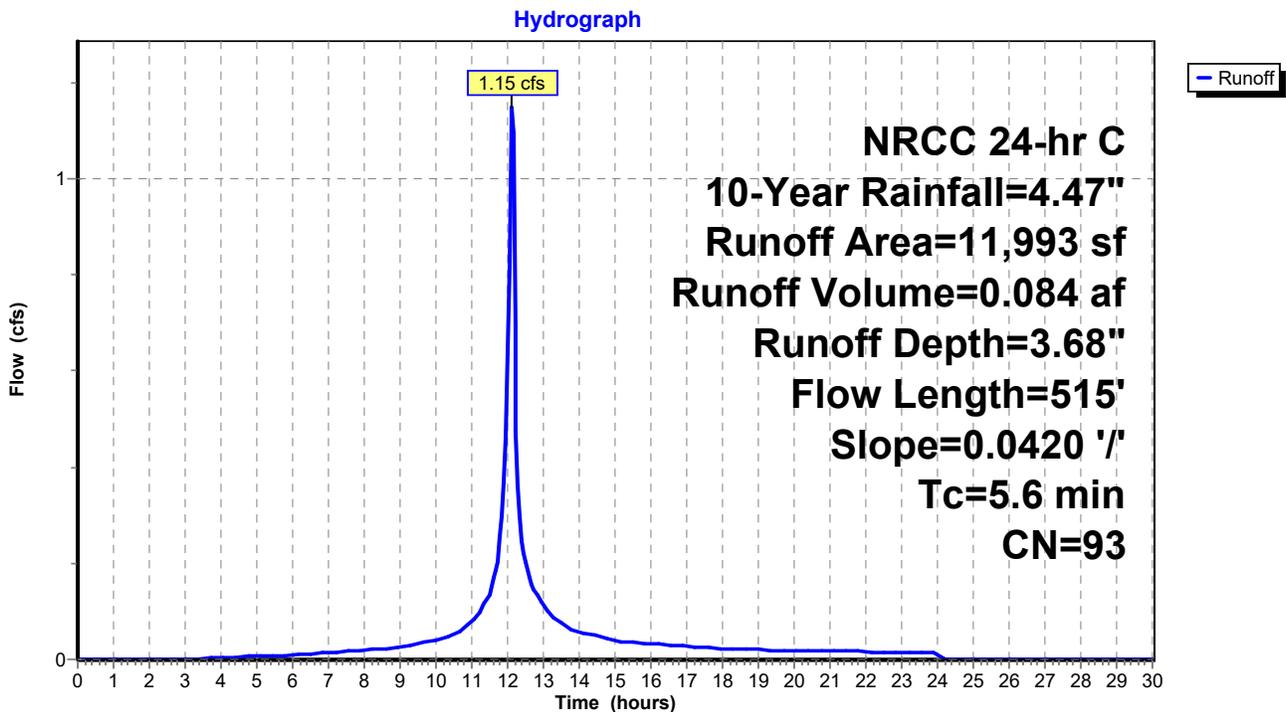
Runoff = 1.15 cfs @ 12.12 hrs, Volume= 0.084 af, Depth= 3.68"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-30.00 hrs, dt= 0.05 hrs
NRCC 24-hr C 10-Year Rainfall=4.47"

Area (sf)	CN	Description
10,800	98	Paved parking, HSG A
1,193	49	50-75% Grass cover, Fair, HSG A
11,993	93	Weighted Average
1,193		9.95% Pervious Area
10,800		90.05% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
5.6	515	0.0420	1.53		Lag/CN Method, Contour Length= 504' Interval= 1'

Subcatchment E1A: Amherst road



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Summary for Subcatchment E2: east drainage area

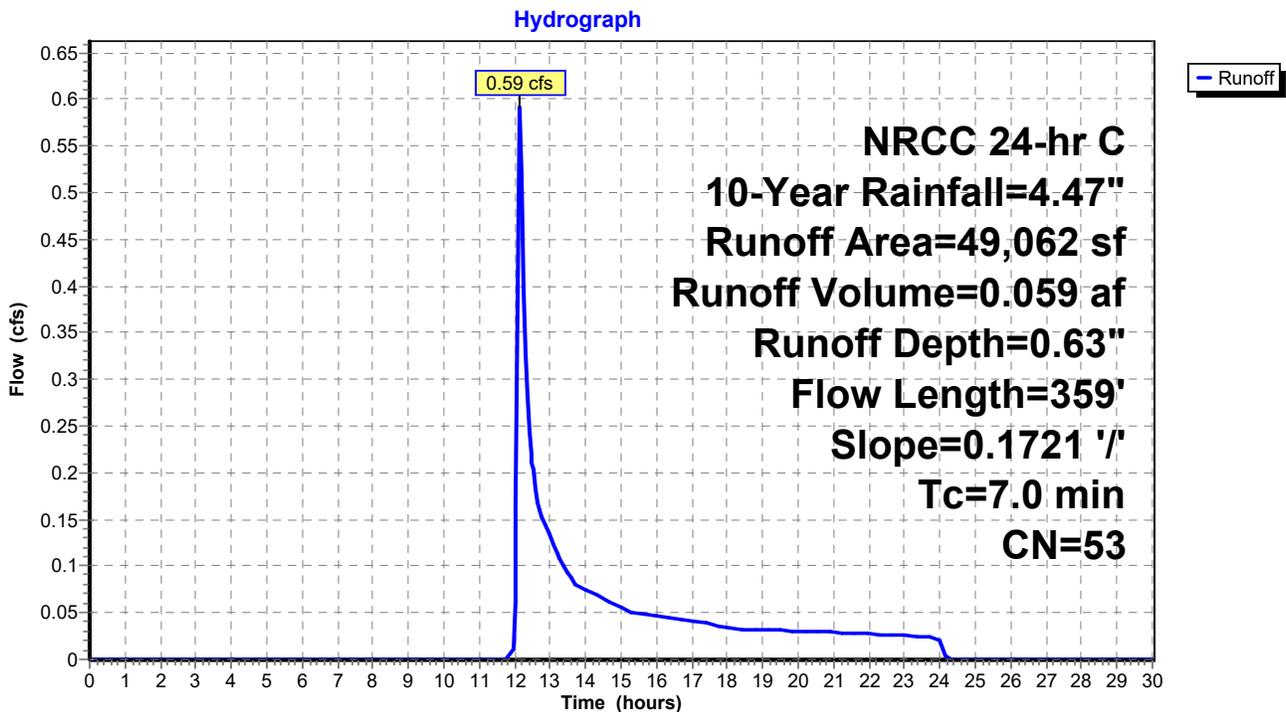
Runoff = 0.59 cfs @ 12.16 hrs, Volume= 0.059 af, Depth= 0.63"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-30.00 hrs, dt= 0.05 hrs
NRCC 24-hr C 10-Year Rainfall=4.47"

Area (sf)	CN	Description
10,891	98	Paved parking, HSG A
31,957	36	Woods, Fair, HSG A
5,000	49	50-75% Grass cover, Fair, HSG A
1,214	96	Gravel surface, HSG A
49,062	53	Weighted Average
38,171		77.80% Pervious Area
10,891		22.20% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
7.0	359	0.1721	0.86		Lag/CN Method, Contour Length= 8,443' Interval= 1'

Subcatchment E2: east drainage area



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Summary for Subcatchment E3: central drainage off site #24

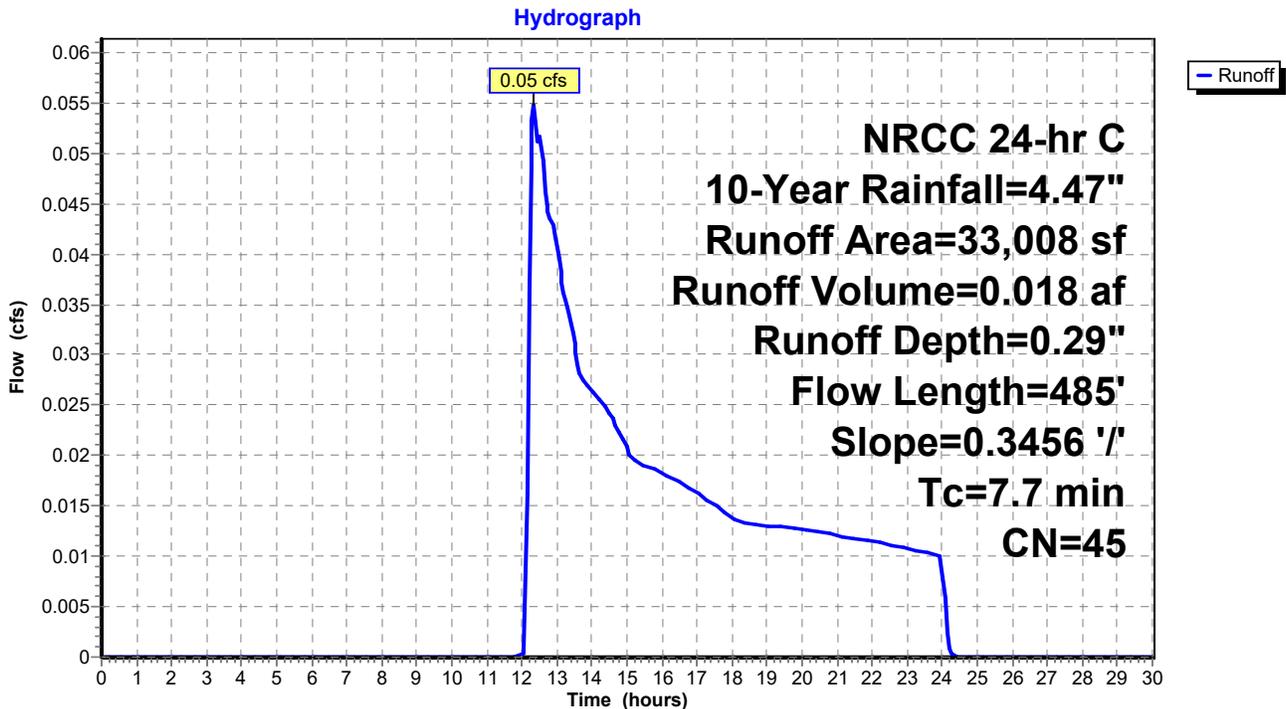
Runoff = 0.05 cfs @ 12.35 hrs, Volume= 0.018 af, Depth= 0.29"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-30.00 hrs, dt= 0.05 hrs
NRCC 24-hr C 10-Year Rainfall=4.47"

Area (sf)	CN	Description
3,810	98	Paved parking, HSG A
24,198	36	Woods, Fair, HSG A
5,000	49	50-75% Grass cover, Fair, HSG A
33,008	45	Weighted Average
29,198		88.46% Pervious Area
3,810		11.54% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
7.7	485	0.3456	1.05		Lag/CN Method, Contour Length= 11,408' Interval= 1'

Subcatchment E3: central drainage off site #24



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Summary for Subcatchment E3A: central drainage area - on site

[49] Hint: Tc<2dt may require smaller dt

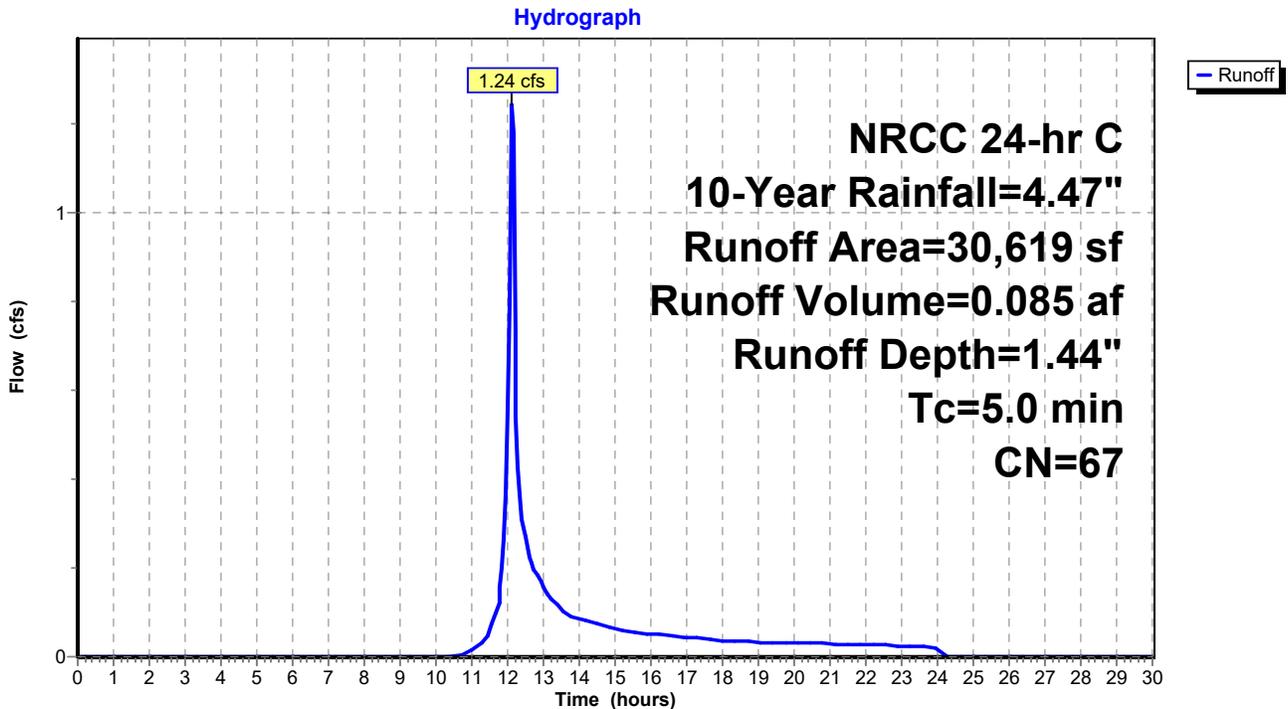
Runoff = 1.24 cfs @ 12.12 hrs, Volume= 0.085 af, Depth= 1.44"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-30.00 hrs, dt= 0.05 hrs
NRCC 24-hr C 10-Year Rainfall=4.47"

Area (sf)	CN	Description
12,631	98	Paved parking, HSG A
10,000	49	50-75% Grass cover, Fair, HSG A
6,338	36	Woods, Fair, HSG A
* 1,650	49	Drip edge around buildings
30,619	67	Weighted Average
17,988		58.75% Pervious Area
12,631		41.25% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
5.0					Direct Entry,

Subcatchment E3A: central drainage area - on site



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Summary for Subcatchment E3B: ex garage roof

[49] Hint: Tc<2dt may require smaller dt

Runoff = 0.26 cfs @ 12.11 hrs, Volume= 0.020 af, Depth= 4.23"

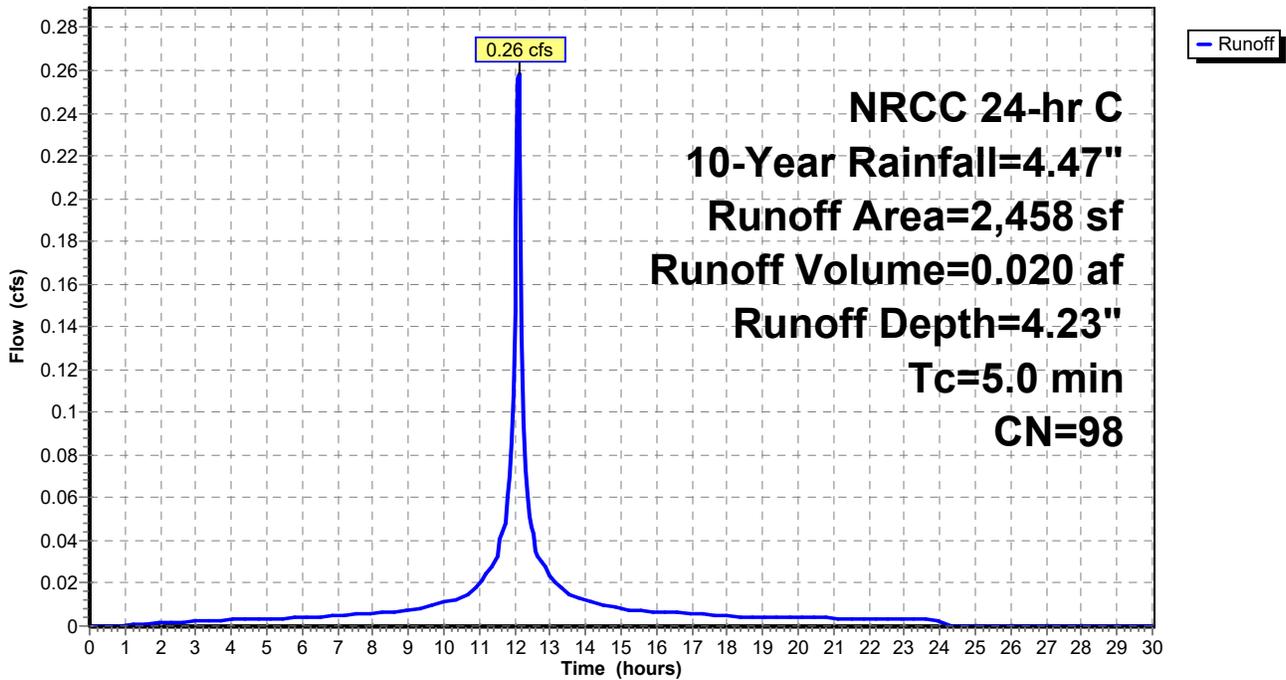
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-30.00 hrs, dt= 0.05 hrs
NRCC 24-hr C 10-Year Rainfall=4.47"

Area (sf)	CN	Description
2,458	98	Roofs, HSG A
2,458		100.00% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
5.0					Direct Entry,

Subcatchment E3B: ex garage roof

Hydrograph



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NRCC 24-hr C 10-Year Rainfall=4.47"

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Summary for Subcatchment E4: west drainage area

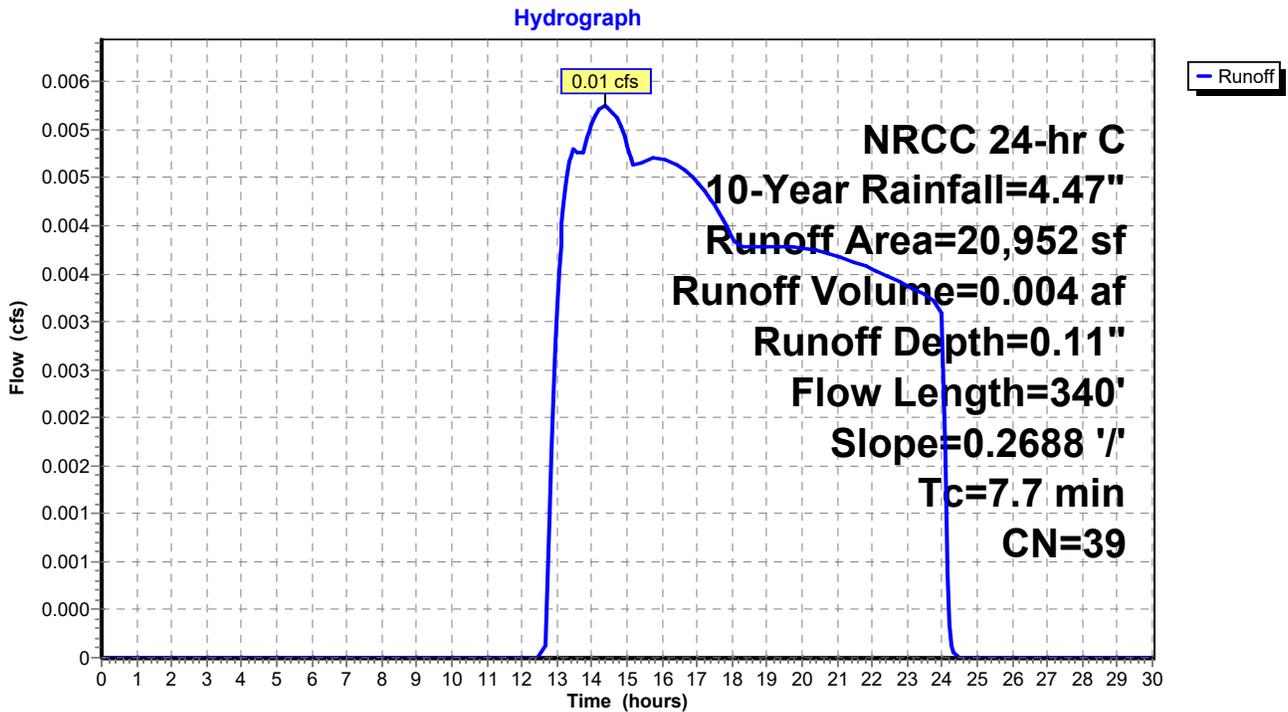
Runoff = 0.01 cfs @ 14.37 hrs, Volume= 0.004 af, Depth= 0.11"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-30.00 hrs, dt= 0.05 hrs
NRCC 24-hr C 10-Year Rainfall=4.47"

Area (sf)	CN	Description
967	98	Paved parking, HSG A
19,985	36	Woods, Fair, HSG A
20,952	39	Weighted Average
19,985		95.38% Pervious Area
967		4.62% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
7.7	340	0.2688	0.74		Lag/CN Method, Contour Length= 5,632' Interval= 1'

Subcatchment E4: west drainage area



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NRCC 24-hr C 10-Year Rainfall=4.47"

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Summary for Subcatchment E4A: ex bldg roof

[49] Hint: Tc<2dt may require smaller dt

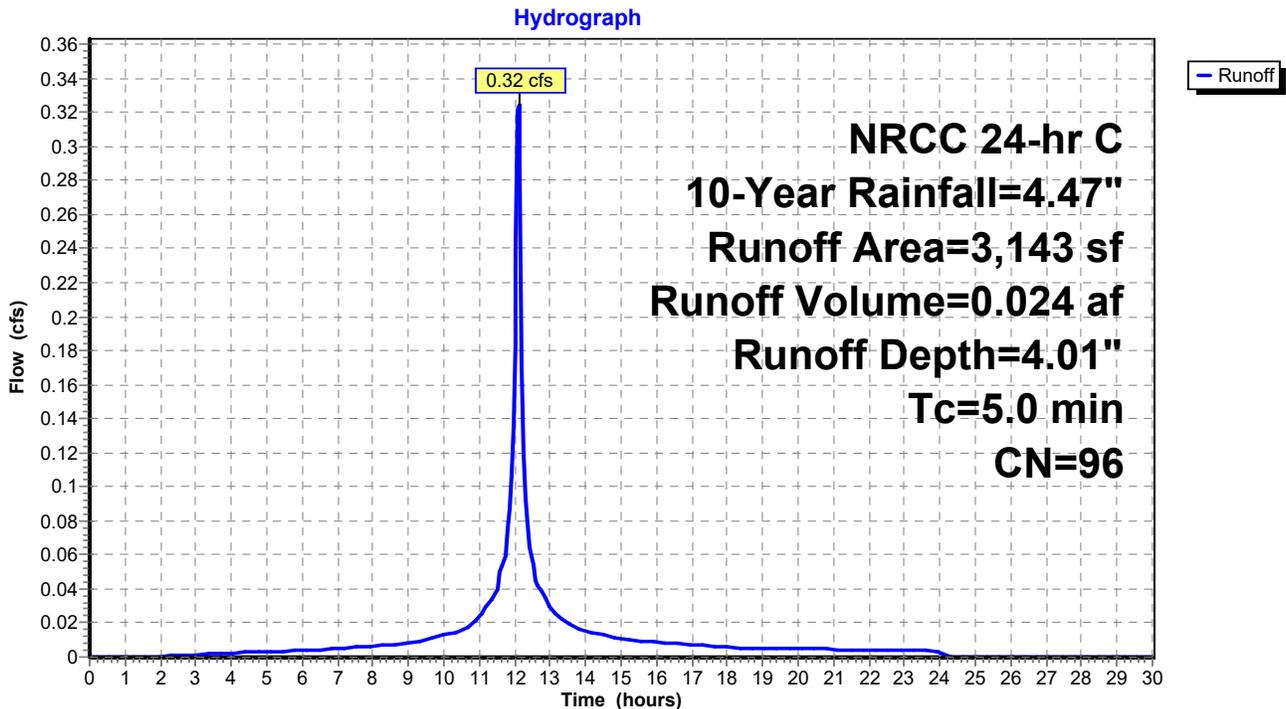
Runoff = 0.32 cfs @ 12.11 hrs, Volume= 0.024 af, Depth= 4.01"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-30.00 hrs, dt= 0.05 hrs
NRCC 24-hr C 10-Year Rainfall=4.47"

Area (sf)	CN	Description
3,000	98	Paved parking, HSG A
143	49	50-75% Grass cover, Fair, HSG A
3,143	96	Weighted Average
143		4.55% Pervious Area
3,000		95.45% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
5.0					Direct Entry,

Subcatchment E4A: ex bldg roof

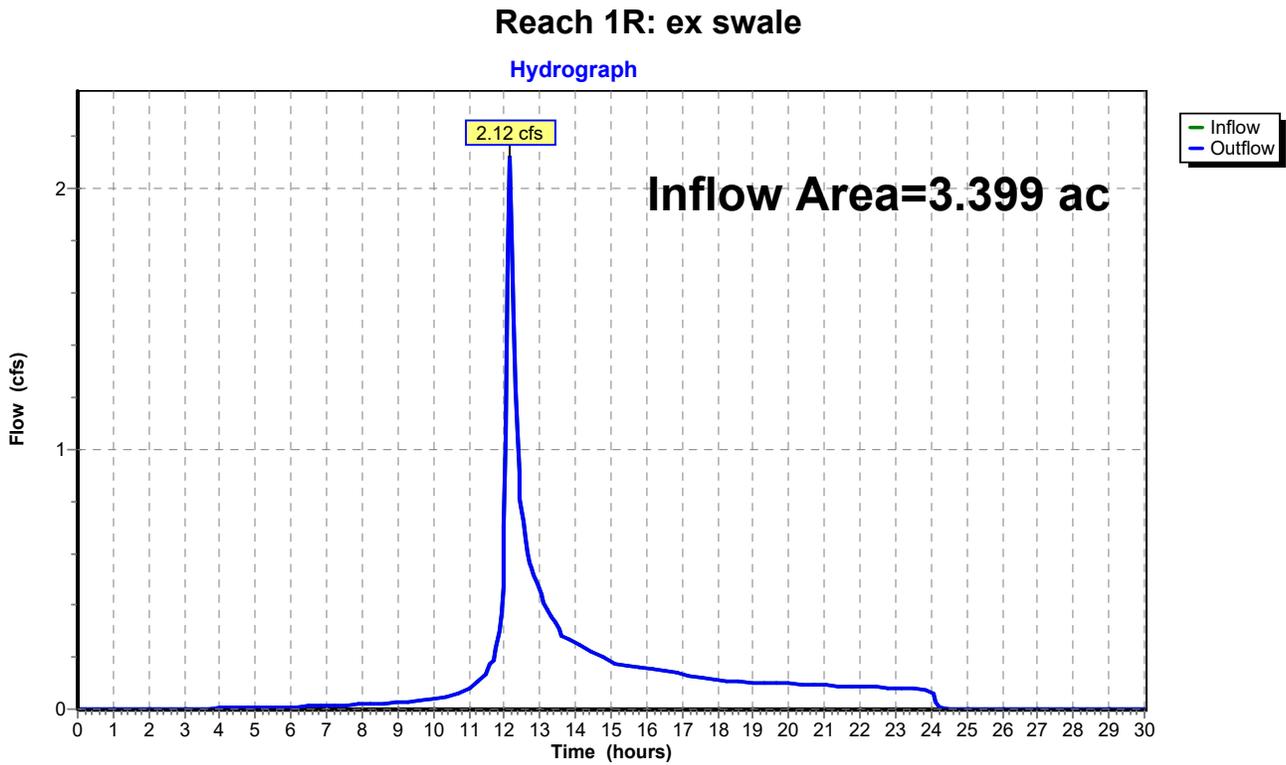


Summary for Reach 1R: ex swale

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area = 3.399 ac, 19.94% Impervious, Inflow Depth = 0.82" for 10-Year event
Inflow = 2.12 cfs @ 12.15 hrs, Volume= 0.232 af
Outflow = 2.12 cfs @ 12.15 hrs, Volume= 0.232 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind method, Time Span= 0.00-30.00 hrs, dt= 0.05 hrs

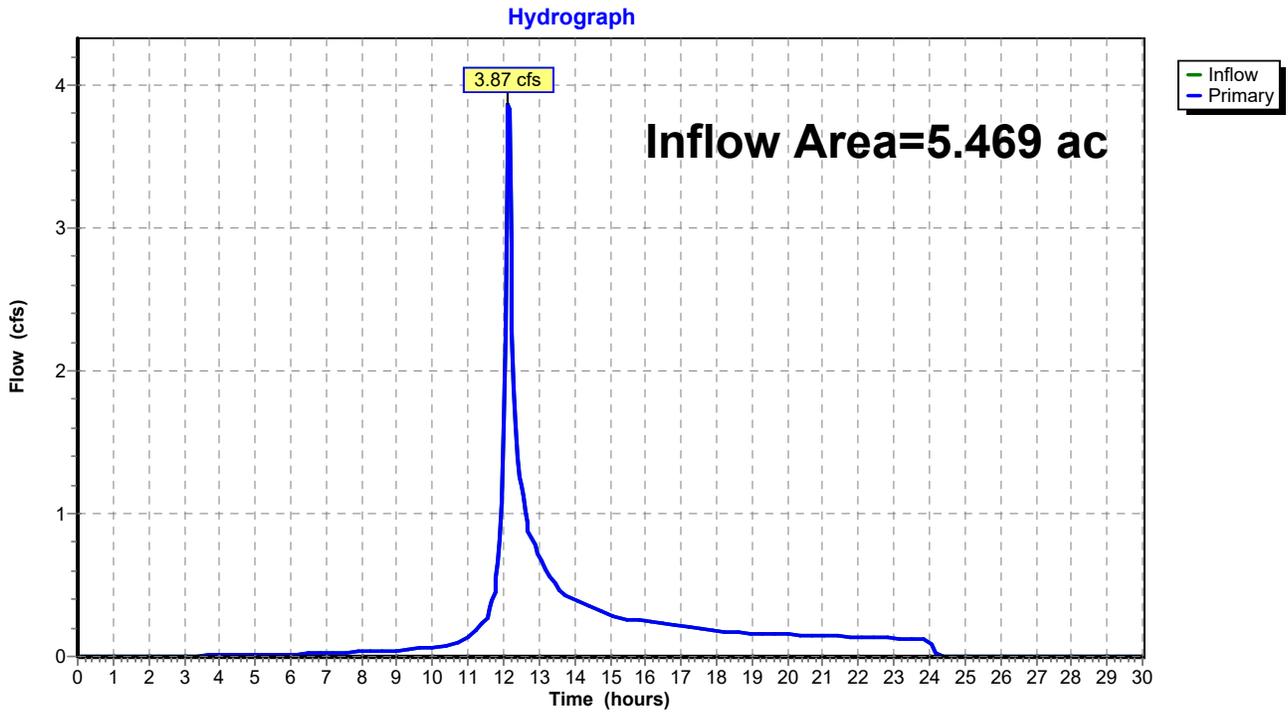


Summary for Link 1L: Study Point - Amethyst Brook

Inflow Area = 5.469 ac, 21.99% Impervious, Inflow Depth = 0.84" for 10-Year event
Inflow = 3.87 cfs @ 12.14 hrs, Volume= 0.383 af
Primary = 3.87 cfs @ 12.14 hrs, Volume= 0.383 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-30.00 hrs, dt= 0.05 hrs

Link 1L: Study Point - Amethyst Brook



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NRCC 24-hr C 100-Year Rainfall=7.68"

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Summary for Subcatchment E1: Amherst rd and South

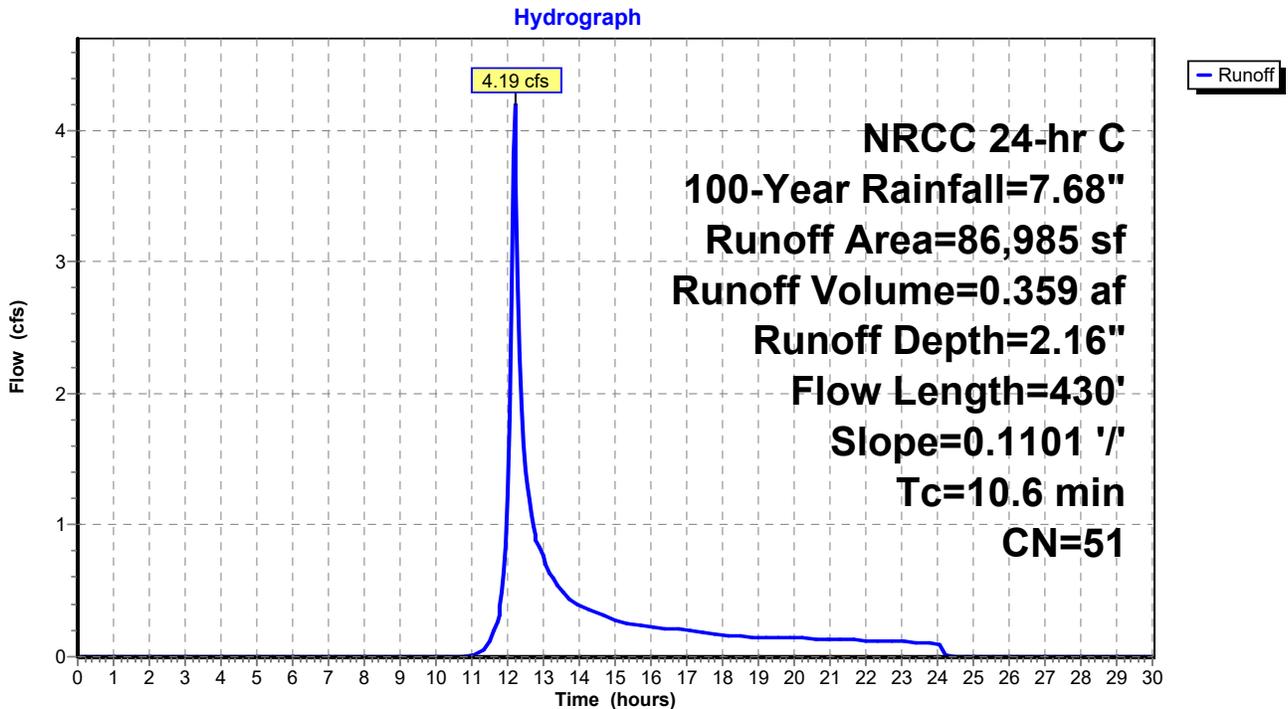
Runoff = 4.19 cfs @ 12.19 hrs, Volume= 0.359 af, Depth= 2.16"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-30.00 hrs, dt= 0.05 hrs
NRCC 24-hr C 100-Year Rainfall=7.68"

Area (sf)	CN	Description
7,024	98	Paved parking, HSG A
806	98	Paved parking, HSG B
39,100	36	Woods, Fair, HSG A
30,655	60	Woods, Fair, HSG B
9,400	49	50-75% Grass cover, Fair, HSG A
86,985	51	Weighted Average
79,155		91.00% Pervious Area
7,830		9.00% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
10.6	430	0.1101	0.68		Lag/CN Method, Contour Length= 9,580' Interval= 1'

Subcatchment E1: Amherst rd and South



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NRCC 24-hr C 100-Year Rainfall=7.68"

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Summary for Subcatchment E1A: Amherst road

[49] Hint: Tc<2dt may require smaller dt

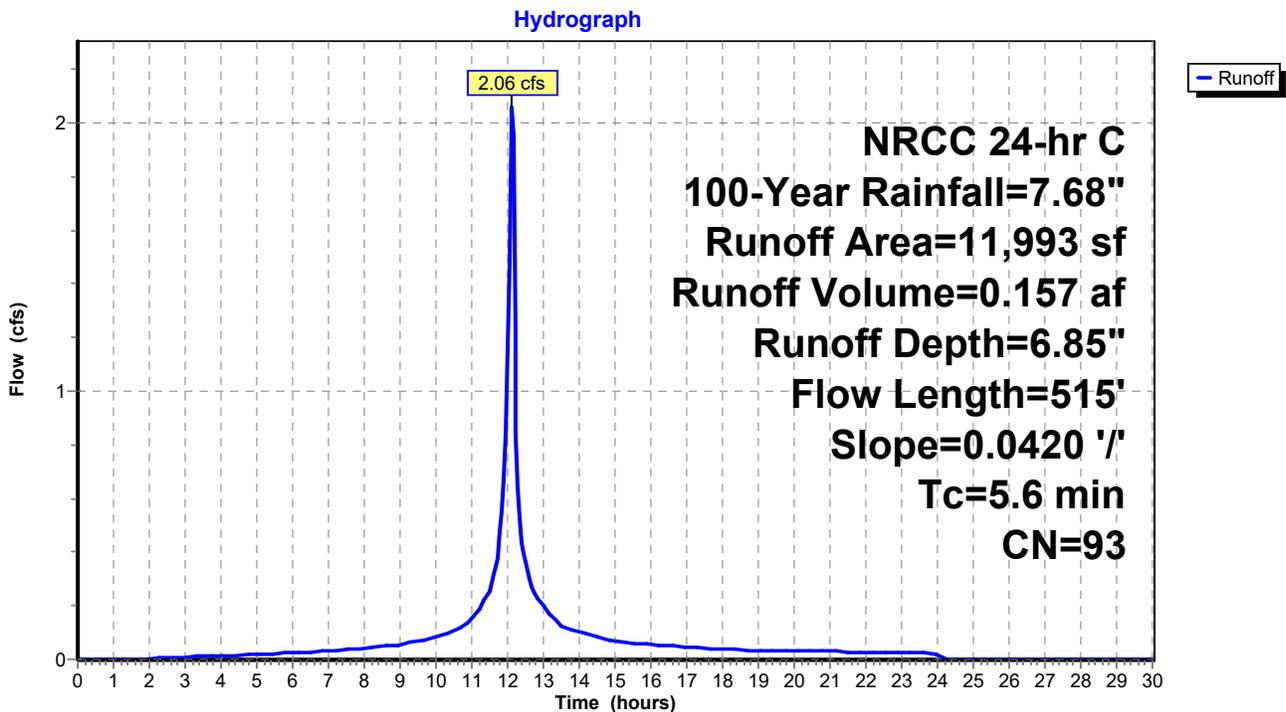
Runoff = 2.06 cfs @ 12.12 hrs, Volume= 0.157 af, Depth= 6.85"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-30.00 hrs, dt= 0.05 hrs
NRCC 24-hr C 100-Year Rainfall=7.68"

Area (sf)	CN	Description
10,800	98	Paved parking, HSG A
1,193	49	50-75% Grass cover, Fair, HSG A
11,993	93	Weighted Average
1,193		9.95% Pervious Area
10,800		90.05% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
5.6	515	0.0420	1.53		Lag/CN Method, Contour Length= 504' Interval= 1'

Subcatchment E1A: Amherst road



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Summary for Subcatchment E2: east drainage area

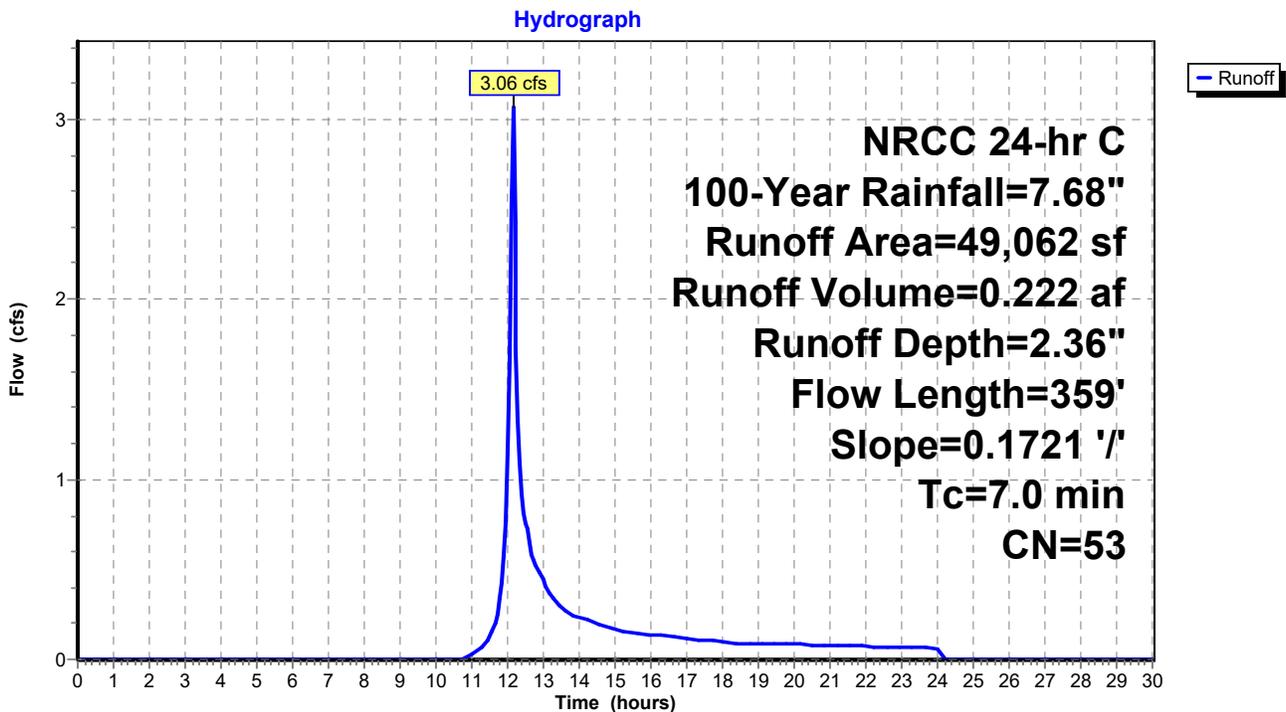
Runoff = 3.06 cfs @ 12.15 hrs, Volume= 0.222 af, Depth= 2.36"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-30.00 hrs, dt= 0.05 hrs
NRCC 24-hr C 100-Year Rainfall=7.68"

Area (sf)	CN	Description
10,891	98	Paved parking, HSG A
31,957	36	Woods, Fair, HSG A
5,000	49	50-75% Grass cover, Fair, HSG A
1,214	96	Gravel surface, HSG A
49,062	53	Weighted Average
38,171		77.80% Pervious Area
10,891		22.20% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
7.0	359	0.1721	0.86		Lag/CN Method, Contour Length= 8,443' Interval= 1'

Subcatchment E2: east drainage area



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Summary for Subcatchment E3: central drainage off site #24

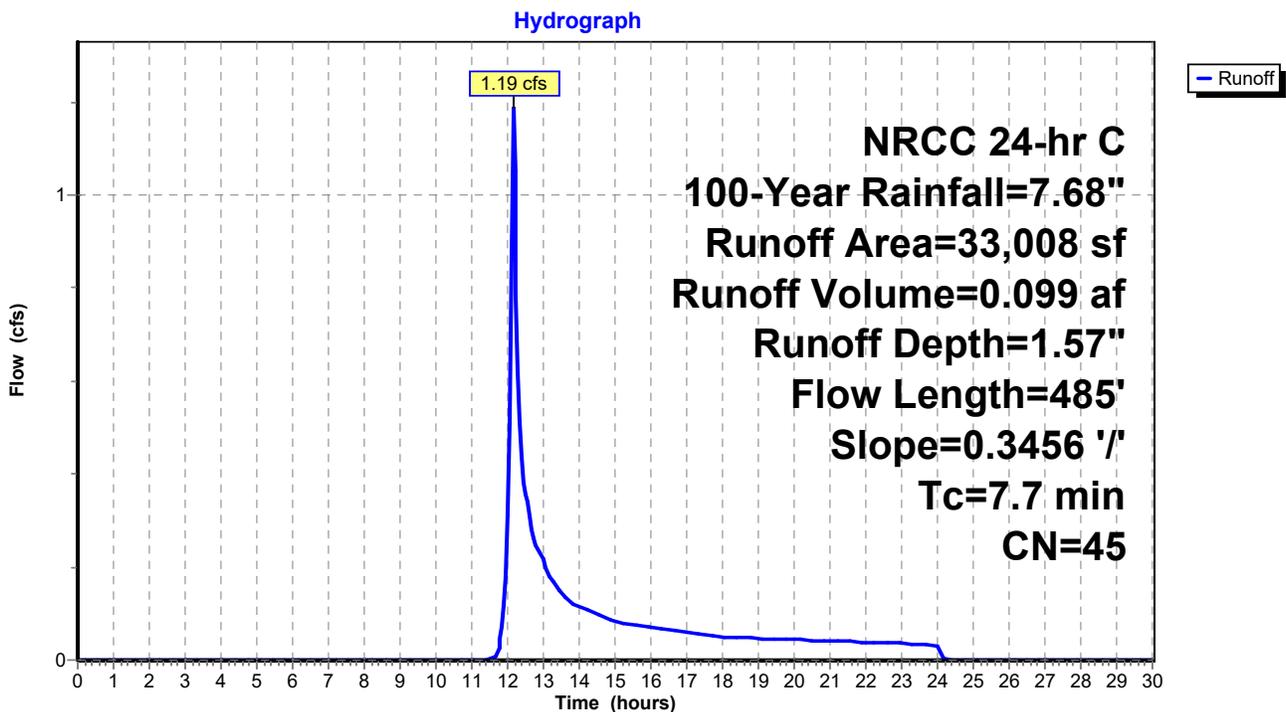
Runoff = 1.19 cfs @ 12.16 hrs, Volume= 0.099 af, Depth= 1.57"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-30.00 hrs, dt= 0.05 hrs
NRCC 24-hr C 100-Year Rainfall=7.68"

Area (sf)	CN	Description
3,810	98	Paved parking, HSG A
24,198	36	Woods, Fair, HSG A
5,000	49	50-75% Grass cover, Fair, HSG A
33,008	45	Weighted Average
29,198		88.46% Pervious Area
3,810		11.54% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
7.7	485	0.3456	1.05		Lag/CN Method, Contour Length= 11,408' Interval= 1'

Subcatchment E3: central drainage off site #24



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Summary for Subcatchment E3A: central drainage area - on site

[49] Hint: Tc<2dt may require smaller dt

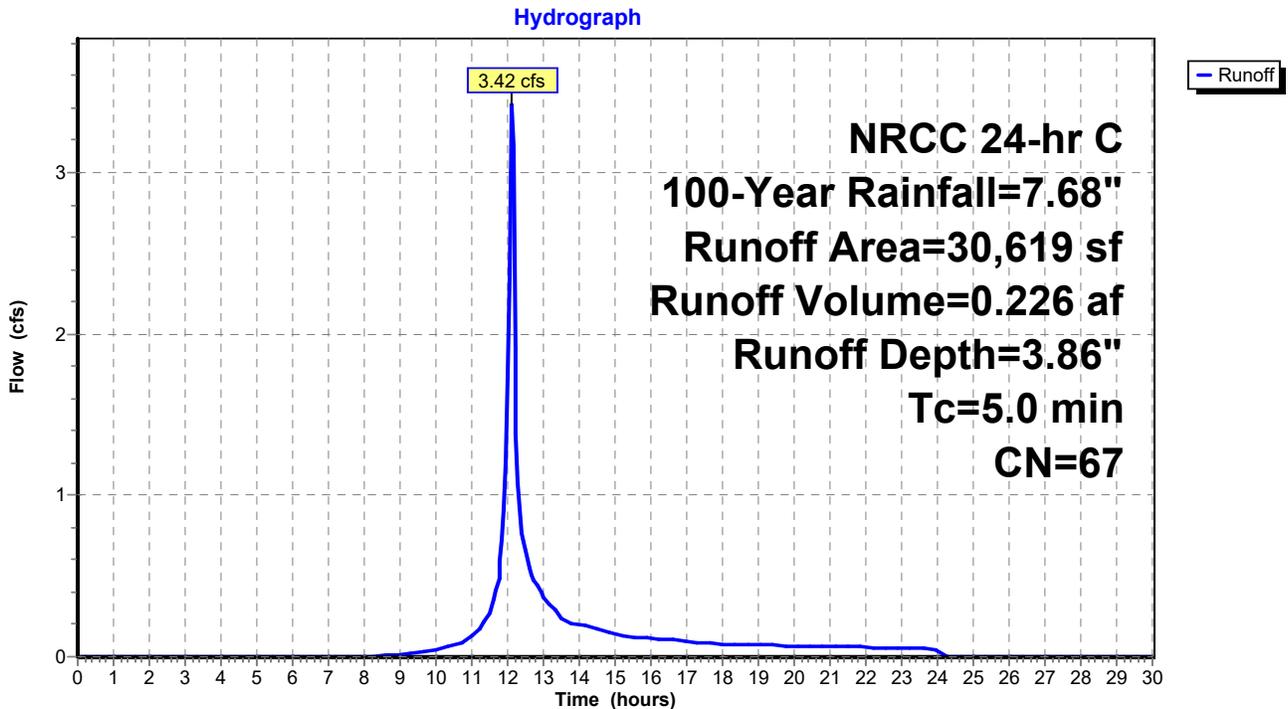
Runoff = 3.42 cfs @ 12.12 hrs, Volume= 0.226 af, Depth= 3.86"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-30.00 hrs, dt= 0.05 hrs
NRCC 24-hr C 100-Year Rainfall=7.68"

Area (sf)	CN	Description
12,631	98	Paved parking, HSG A
10,000	49	50-75% Grass cover, Fair, HSG A
6,338	36	Woods, Fair, HSG A
* 1,650	49	Drip edge around buildings
30,619	67	Weighted Average
17,988		58.75% Pervious Area
12,631		41.25% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
5.0					Direct Entry,

Subcatchment E3A: central drainage area - on site



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Summary for Subcatchment E3B: ex garage roof

[49] Hint: $T_c < 2dt$ may require smaller dt

Runoff = 0.45 cfs @ 12.11 hrs, Volume= 0.035 af, Depth= 7.44"

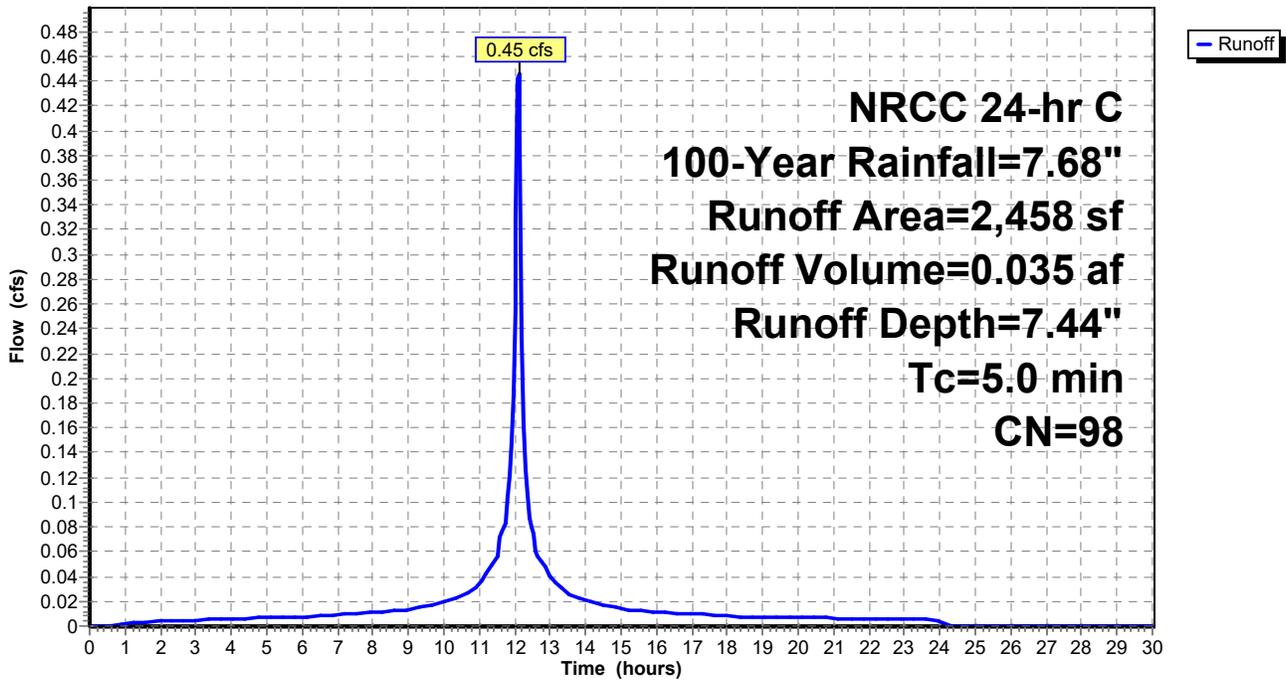
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-30.00 hrs, dt= 0.05 hrs
NRCC 24-hr C 100-Year Rainfall=7.68"

Area (sf)	CN	Description
2,458	98	Roofs, HSG A
2,458		100.00% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
5.0					Direct Entry,

Subcatchment E3B: ex garage roof

Hydrograph



20.024 EXIST REV

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NRCC 24-hr C 100-Year Rainfall=7.68"

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Summary for Subcatchment E4: west drainage area

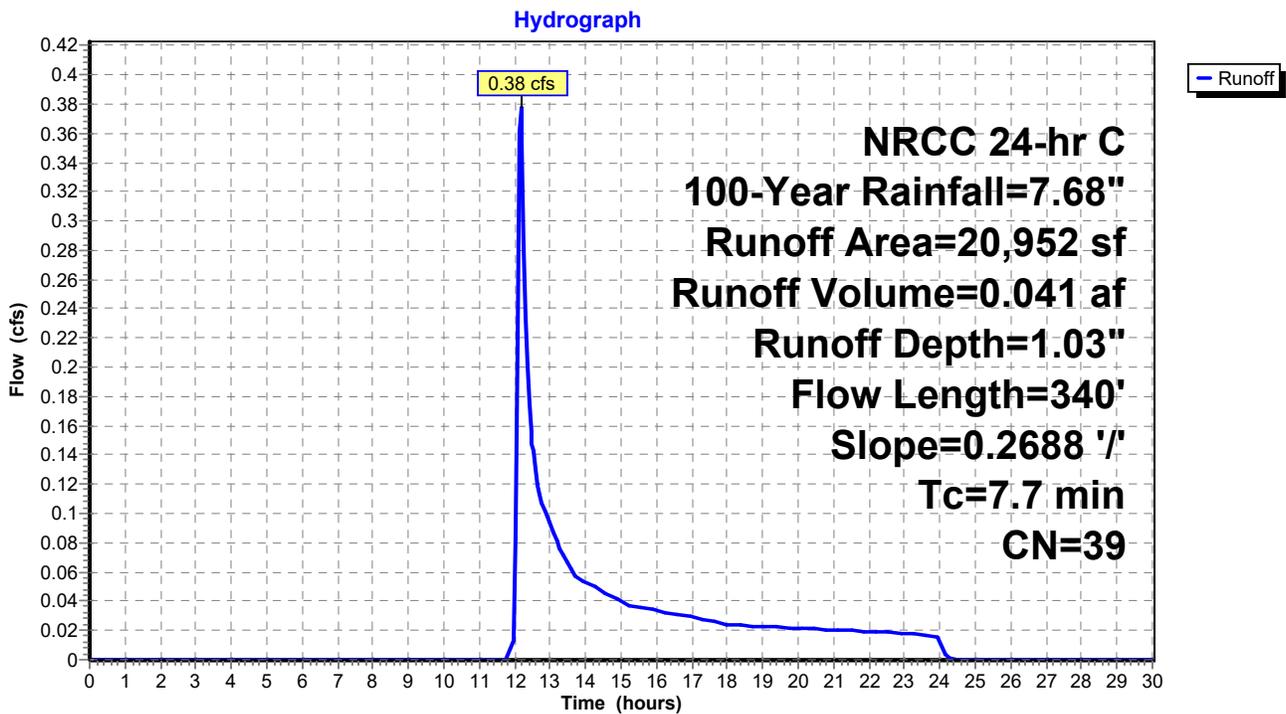
Runoff = 0.38 cfs @ 12.17 hrs, Volume= 0.041 af, Depth= 1.03"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-30.00 hrs, dt= 0.05 hrs
NRCC 24-hr C 100-Year Rainfall=7.68"

Area (sf)	CN	Description
967	98	Paved parking, HSG A
19,985	36	Woods, Fair, HSG A
20,952	39	Weighted Average
19,985		95.38% Pervious Area
967		4.62% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
7.7	340	0.2688	0.74		Lag/CN Method, Contour Length= 5,632' Interval= 1'

Subcatchment E4: west drainage area



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Summary for Subcatchment E4A: ex bldg roof

[49] Hint: Tc<2dt may require smaller dt

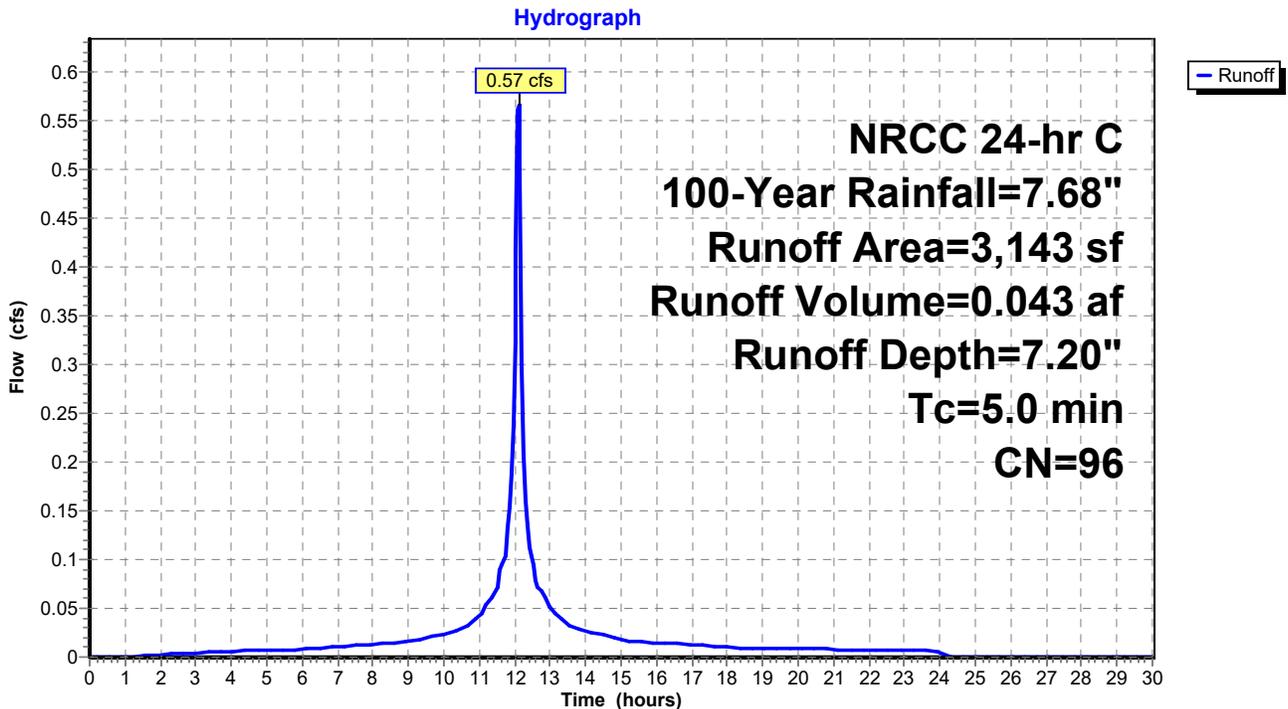
Runoff = 0.57 cfs @ 12.11 hrs, Volume= 0.043 af, Depth= 7.20"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-30.00 hrs, dt= 0.05 hrs
NRCC 24-hr C 100-Year Rainfall=7.68"

Area (sf)	CN	Description
3,000	98	Paved parking, HSG A
143	49	50-75% Grass cover, Fair, HSG A
3,143	96	Weighted Average
143		4.55% Pervious Area
3,000		95.45% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
5.0					Direct Entry,

Subcatchment E4A: ex bldg roof



Summary for Reach 1R: ex swale

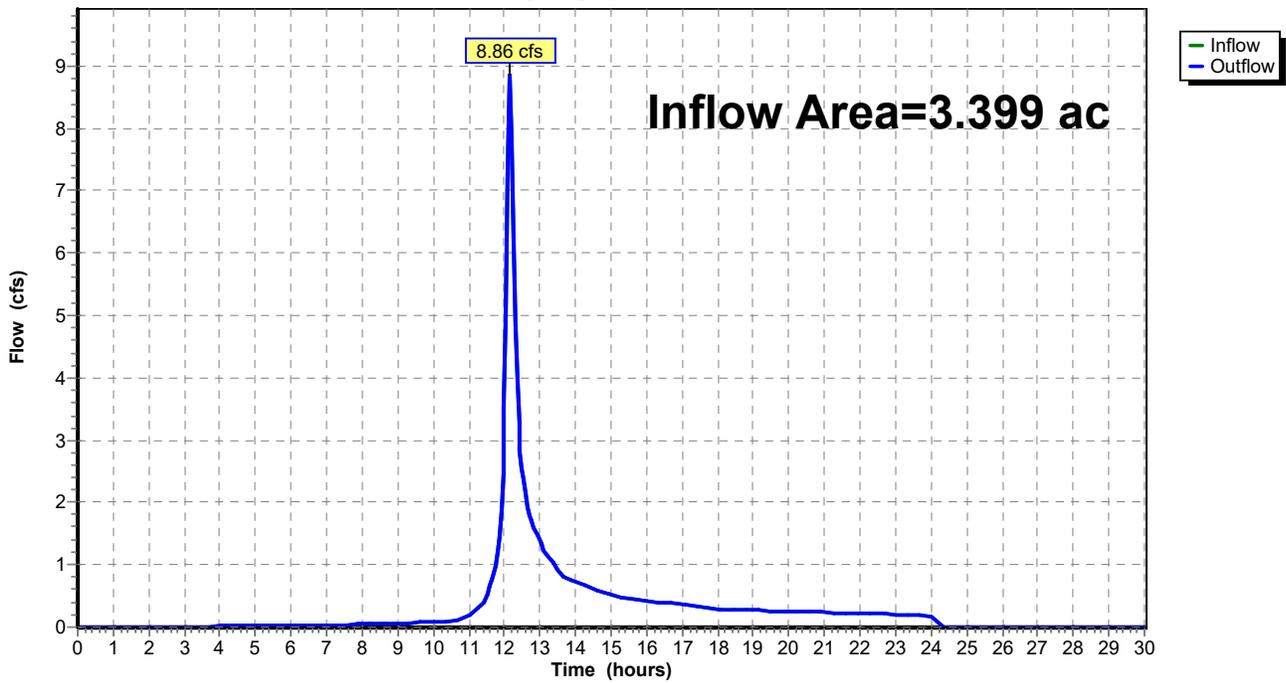
[40] Hint: Not Described (Outflow=Inflow)

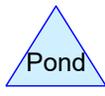
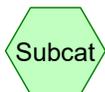
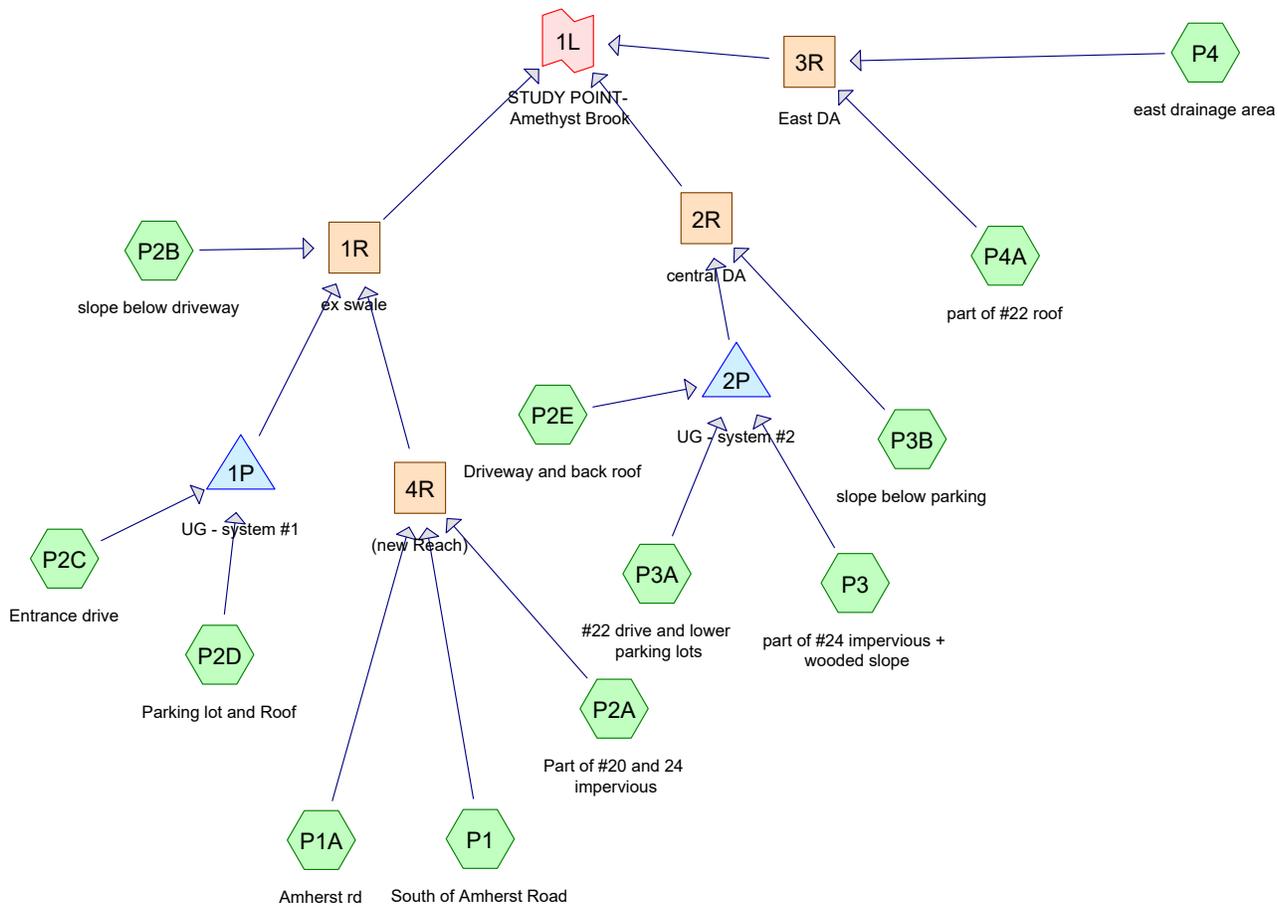
Inflow Area = 3.399 ac, 19.94% Impervious, Inflow Depth = 2.61" for 100-Year event
Inflow = 8.86 cfs @ 12.16 hrs, Volume= 0.738 af
Outflow = 8.86 cfs @ 12.16 hrs, Volume= 0.738 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind method, Time Span= 0.00-30.00 hrs, dt= 0.05 hrs

Reach 1R: ex swale

Hydrograph





Routing Diagram for 20.024 PROP REV
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Project Notes

Rainfall events imported from "NRCS-Rain.txt" for 4007 MA Amherst Hampshire County

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Area Listing (all nodes)

Area (acres)	CN	Description (subcatchment-numbers)
0.728	49	50-75% Grass cover, Fair, HSG A (P1, P1A, P2A, P2C, P2D, P2E, P3, P3A, P3B)
0.045	96	Gravel surface, HSG A (P2E, P3A)
0.939	98	Impervious (P2C, P2D, P2E, P3, P3A, P3B, P4)
0.061	98	Impervious HSG A (P2A)
0.018	98	Impervious - roof (P2E)
0.161	98	Impervious HSG A (P1)
0.019	98	Impervious HSG B (P1)
0.248	98	Paved road, HSG A (P1A)
0.079	98	Unconnected roofs, HSG A (P4A)
0.008	98	Wall (P2B)
2.459	36	Woods, Fair, HSG A (P1, P2A, P2B, P3, P3B, P4, P4A)
0.704	60	Woods, Fair, HSG B (P1)
5.469	59	TOTAL AREA

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Soil Listing (all nodes)

Area (acres)	Soil Group	Subcatchment Numbers
3.781	HSG A	P1, P1A, P2A, P2B, P2C, P2D, P2E, P3, P3A, P3B, P4, P4A
0.722	HSG B	P1
0.000	HSG C	
0.000	HSG D	
0.965	Other	P2B, P2C, P2D, P2E, P3, P3A, P3B, P4
5.469		TOTAL AREA

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Ground Covers (all nodes)

HSG-A (acres)	HSG-B (acres)	HSG-C (acres)	HSG-D (acres)	Other (acres)	Total (acres)	Ground Cover	Subcatchment Numbers
0.728	0.000	0.000	0.000	0.000	0.728	50-75% Grass cover, Fair	P1, P1A, P2A, P2C, P2D, P2E, P3, P3A, P3B
0.045	0.000	0.000	0.000	0.000	0.045	Gravel surface	P2E, P3A
0.222	0.019	0.000	0.000	0.939	1.180	Impervious	P1, P2A, P2C, P2D, P2E, P3, P3A, P3B, P4
0.000	0.000	0.000	0.000	0.018	0.018	Impervious - roof	P2E
0.248	0.000	0.000	0.000	0.000	0.248	Paved road	P1A
0.079	0.000	0.000	0.000	0.000	0.079	Unconnected roofs	P4A
0.000	0.000	0.000	0.000	0.008	0.008	Wall	P2B
2.459	0.704	0.000	0.000	0.000	3.163	Woods, Fair	P1, P2A, P2B, P3, P3B, P4, P4A
3.781	0.722	0.000	0.000	0.965	5.469	TOTAL AREA	

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NRCC 24-hr C 2-Year Rainfall=3.07"

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Summary for Subcatchment P1: South of Amherst Road

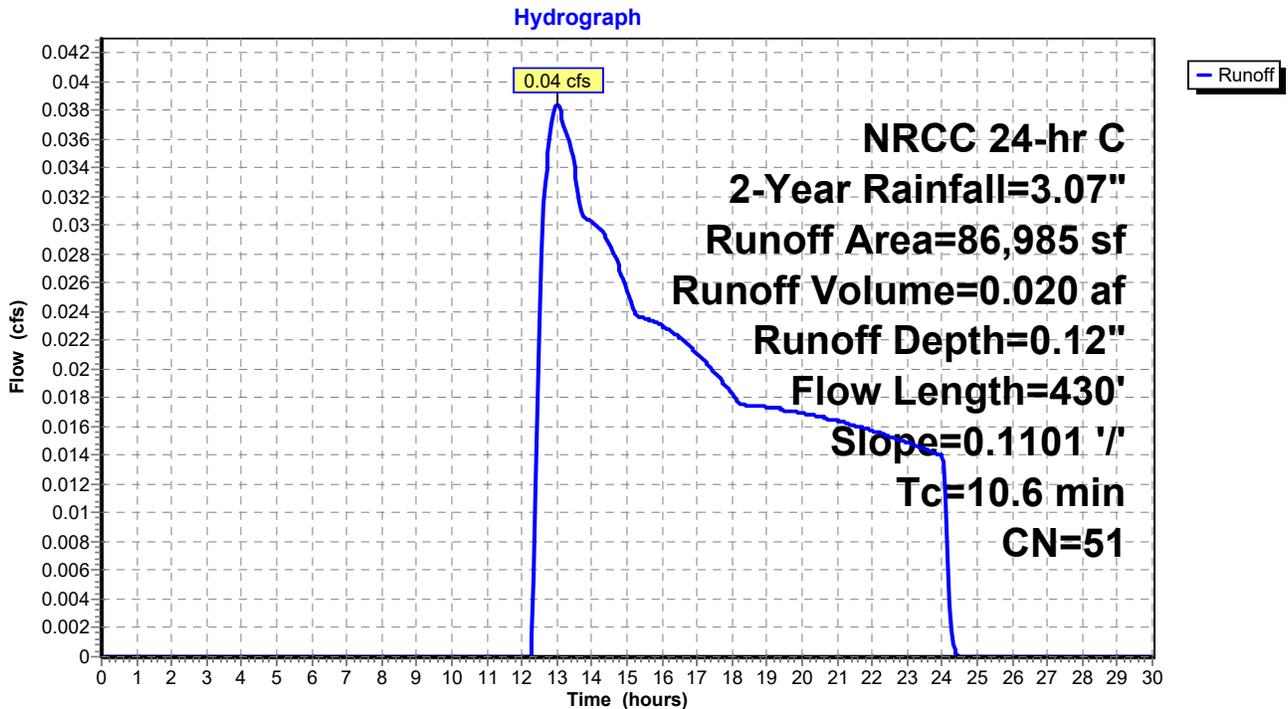
Runoff = 0.04 cfs @ 13.01 hrs, Volume= 0.020 af, Depth= 0.12"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-30.00 hrs, dt= 0.05 hrs
NRCC 24-hr C 2-Year Rainfall=3.07"

	Area (sf)	CN	Description
*	7,024	98	Impervious HSG A
*	806	98	Impervious HSG B
	39,100	36	Woods, Fair, HSG A
	30,655	60	Woods, Fair, HSG B
	9,400	49	50-75% Grass cover, Fair, HSG A
	86,985	51	Weighted Average
	79,155		91.00% Pervious Area
	7,830		9.00% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
10.6	430	0.1101	0.68		Lag/CN Method, Contour Length= 9,580' Interval= 1'

Subcatchment P1: South of Amherst Road



Summary for Subcatchment P1A: Amherst rd

[49] Hint: Tc<2dt may require smaller dt

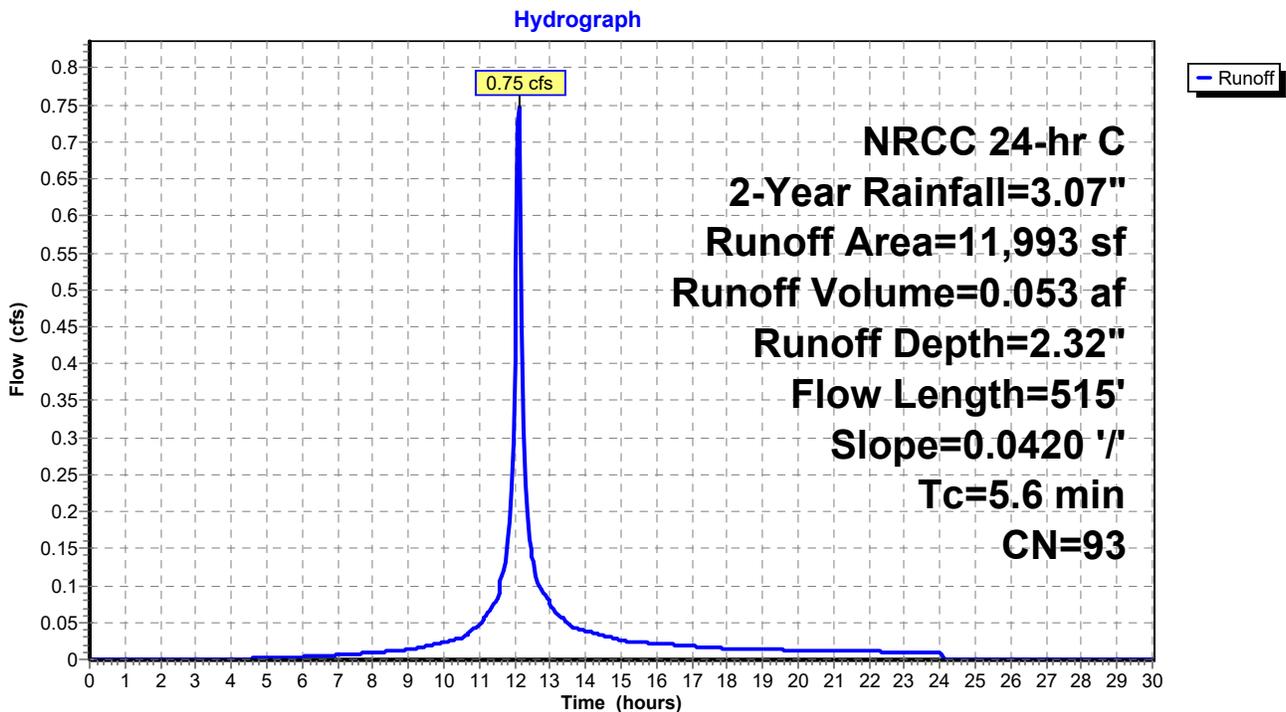
Runoff = 0.75 cfs @ 12.12 hrs, Volume= 0.053 af, Depth= 2.32"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-30.00 hrs, dt= 0.05 hrs
NRCC 24-hr C 2-Year Rainfall=3.07"

	Area (sf)	CN	Description
*	10,800	98	Paved road, HSG A
	1,193	49	50-75% Grass cover, Fair, HSG A
	11,993	93	Weighted Average
	1,193		9.95% Pervious Area
	10,800		90.05% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
5.6	515	0.0420	1.53		Lag/CN Method, Contour Length= 504' Interval= 1'

Subcatchment P1A: Amherst rd



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Summary for Subcatchment P2A: Part of #20 and 24 impervious

[49] Hint: $T_c < 2dt$ may require smaller dt

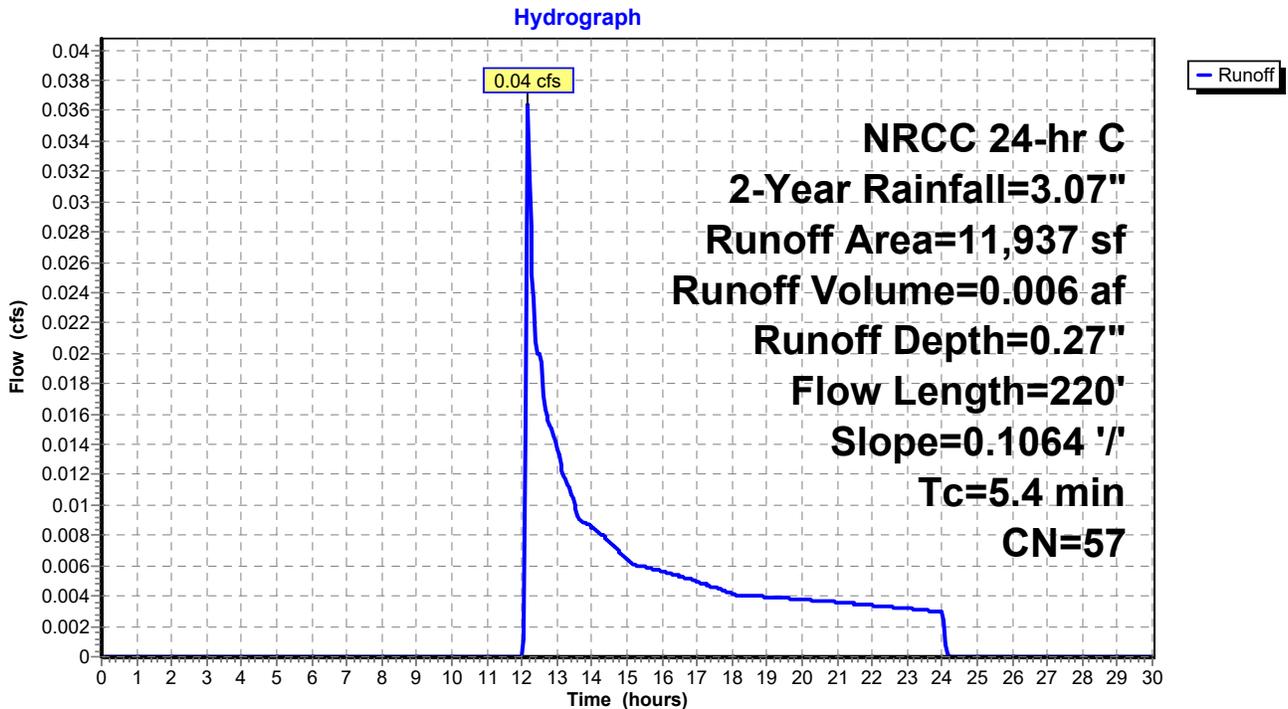
Runoff = 0.04 cfs @ 12.17 hrs, Volume= 0.006 af, Depth= 0.27"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-30.00 hrs, dt= 0.05 hrs
NRCC 24-hr C 2-Year Rainfall=3.07"

	Area (sf)	CN	Description
*	2,647	98	Impervious HSG A
	7,000	49	50-75% Grass cover, Fair, HSG A
	2,290	36	Woods, Fair, HSG A
	11,937	57	Weighted Average
	9,290		77.83% Pervious Area
	2,647		22.17% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
5.4	220	0.1064	0.68		Lag/CN Method, Contour Length= 1,270' Interval= 1'

Subcatchment P2A: Part of #20 and 24 impervious



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Summary for Subcatchment P2B: slope below driveway

[49] Hint: Tc<2dt may require smaller dt

[45] Hint: Runoff=Zero

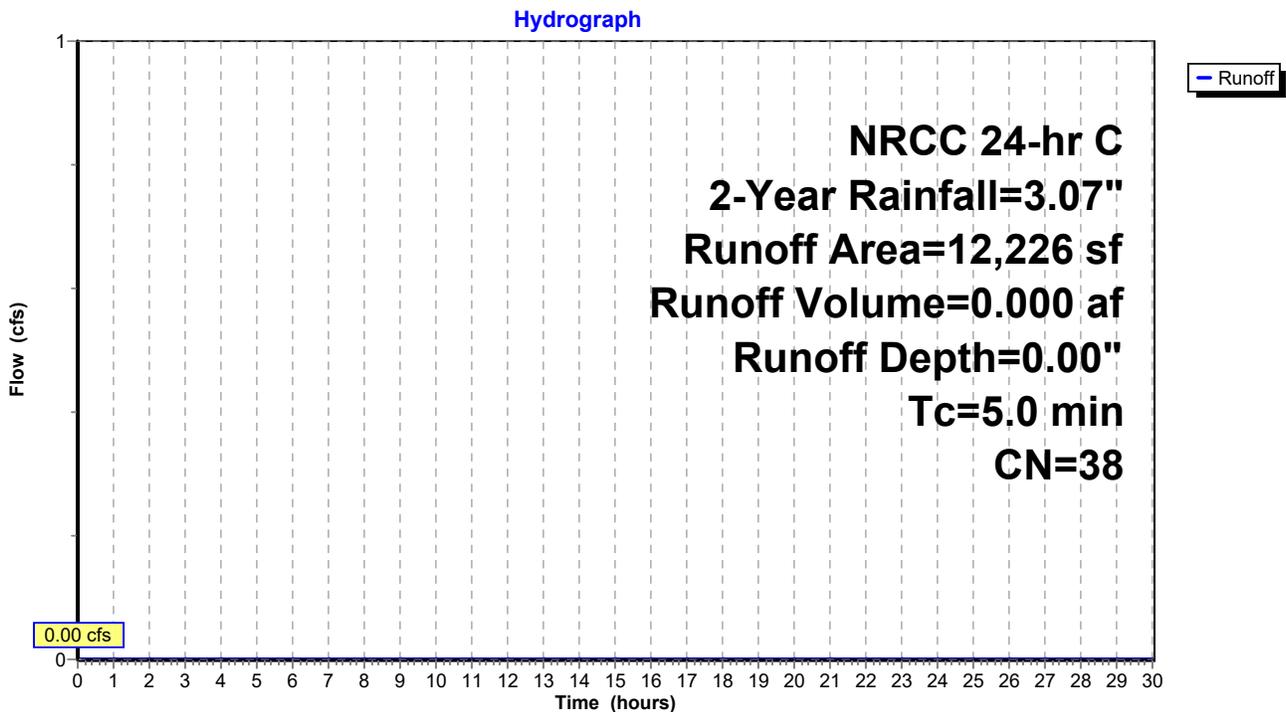
Runoff = 0.00 cfs @ 0.00 hrs, Volume= 0.000 af, Depth= 0.00"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-30.00 hrs, dt= 0.05 hrs
NRCC 24-hr C 2-Year Rainfall=3.07"

Area (sf)	CN	Description
11,888	36	Woods, Fair, HSG A
* 338	98	Wall
12,226	38	Weighted Average
11,888		97.24% Pervious Area
338		2.76% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
5.0					Direct Entry,

Subcatchment P2B: slope below driveway



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Summary for Subcatchment P2C: Entrance drive

[49] Hint: Tc<2dt may require smaller dt

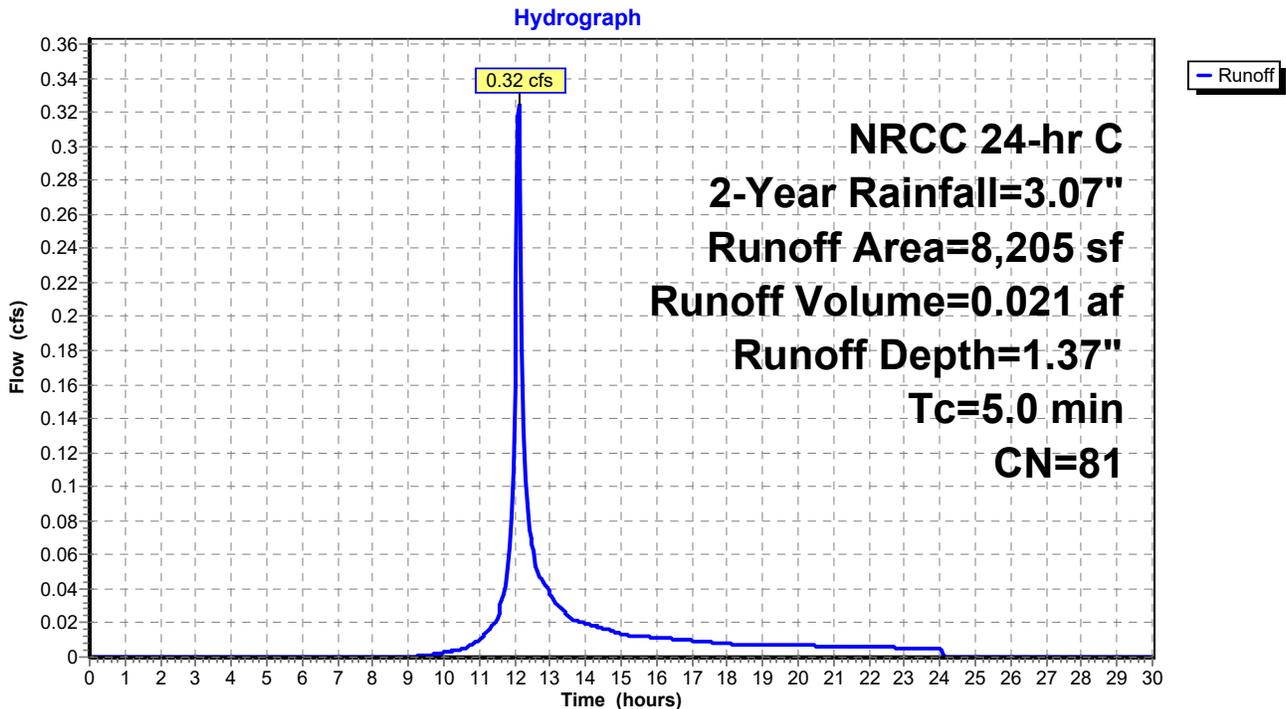
Runoff = 0.32 cfs @ 12.12 hrs, Volume= 0.021 af, Depth= 1.37"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-30.00 hrs, dt= 0.05 hrs
NRCC 24-hr C 2-Year Rainfall=3.07"

	Area (sf)	CN	Description
*	5,389	98	Impervious
	2,816	49	50-75% Grass cover, Fair, HSG A
	8,205	81	Weighted Average
	2,816		34.32% Pervious Area
	5,389		65.68% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
5.0					Direct Entry,

Subcatchment P2C: Entrance drive



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Summary for Subcatchment P2D: Parking lot and Roof

[49] Hint: Tc<2dt may require smaller dt

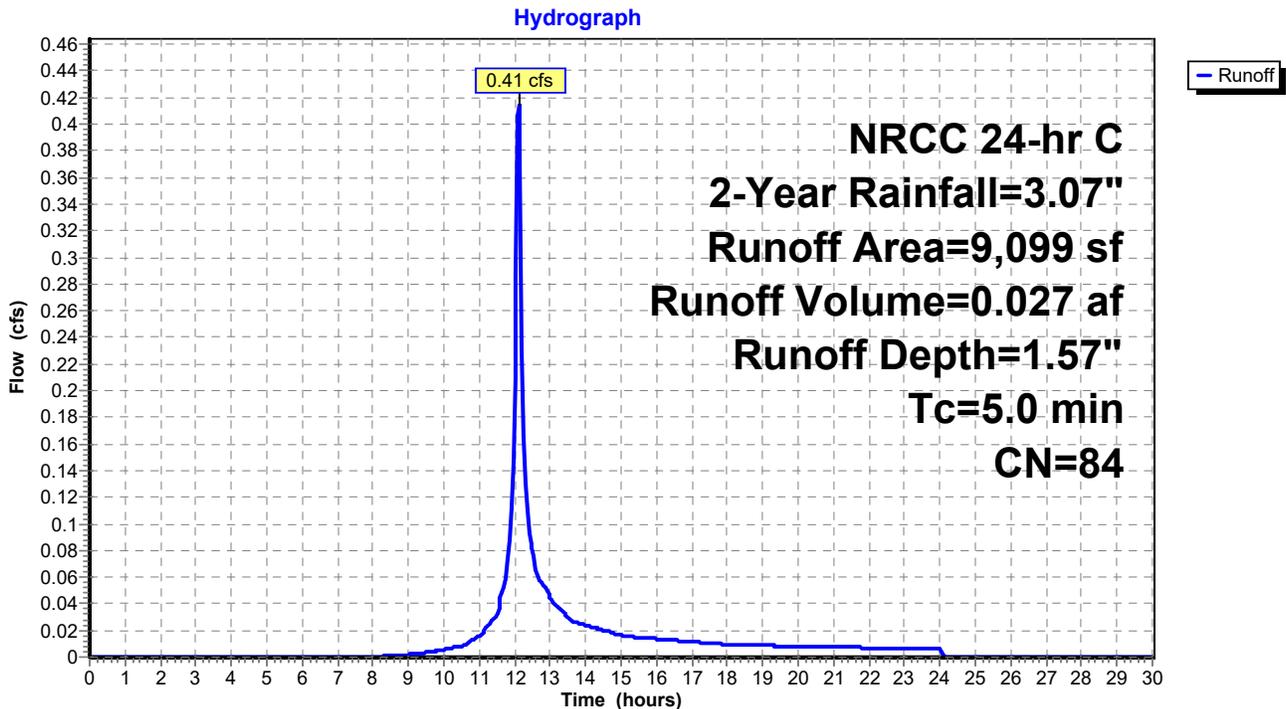
Runoff = 0.41 cfs @ 12.12 hrs, Volume= 0.027 af, Depth= 1.57"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-30.00 hrs, dt= 0.05 hrs
NRCC 24-hr C 2-Year Rainfall=3.07"

	Area (sf)	CN	Description
*	6,504	98	Impervious
	2,595	49	50-75% Grass cover, Fair, HSG A
	9,099	84	Weighted Average
	2,595		28.52% Pervious Area
	6,504		71.48% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
5.0					Direct Entry,

Subcatchment P2D: Parking lot and Roof



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Summary for Subcatchment P2E: Driveway and back roof

[49] Hint: Tc<2dt may require smaller dt

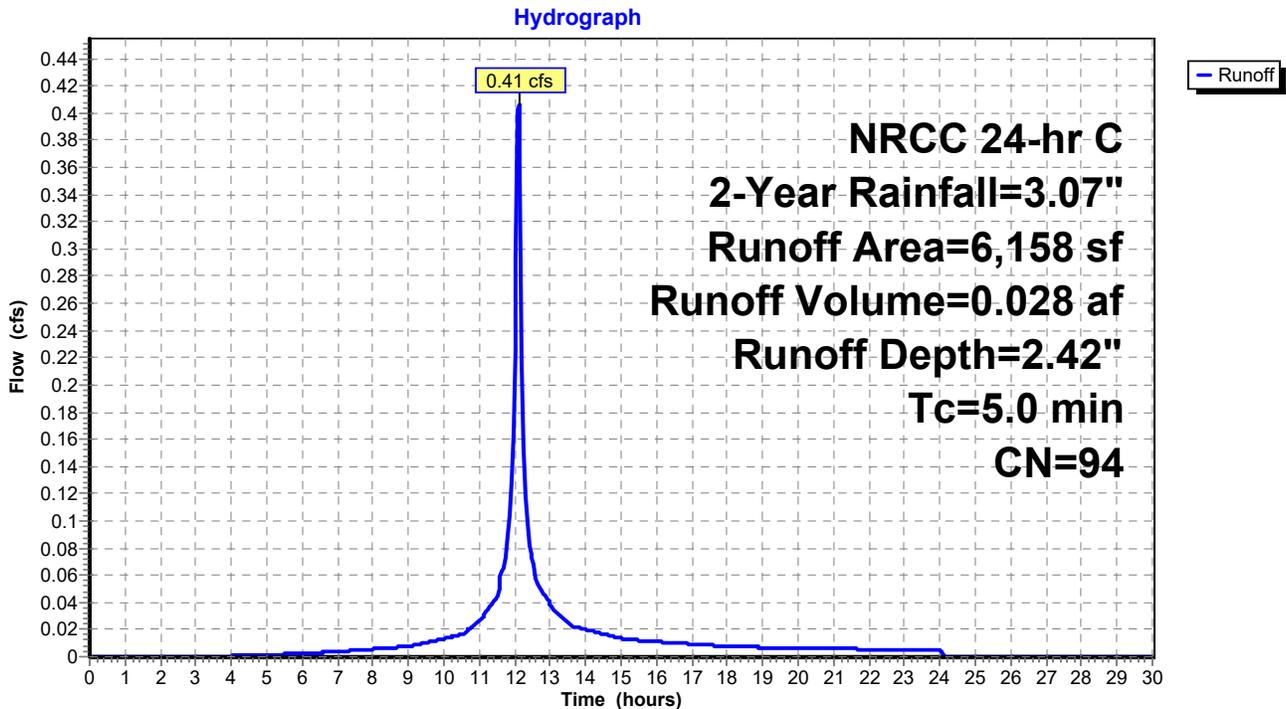
Runoff = 0.41 cfs @ 12.11 hrs, Volume= 0.028 af, Depth= 2.42"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-30.00 hrs, dt= 0.05 hrs
NRCC 24-hr C 2-Year Rainfall=3.07"

	Area (sf)	CN	Description
*	4,254	98	Impervious
	653	96	Gravel surface, HSG A
	451	49	50-75% Grass cover, Fair, HSG A
*	800	98	Impervious - roof
	6,158	94	Weighted Average
	1,104		17.93% Pervious Area
	5,054		82.07% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
5.0					Direct Entry,

Subcatchment P2E: Driveway and back roof



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Summary for Subcatchment P3A: #22 drive and lower parking lots

[49] Hint: Tc<2dt may require smaller dt

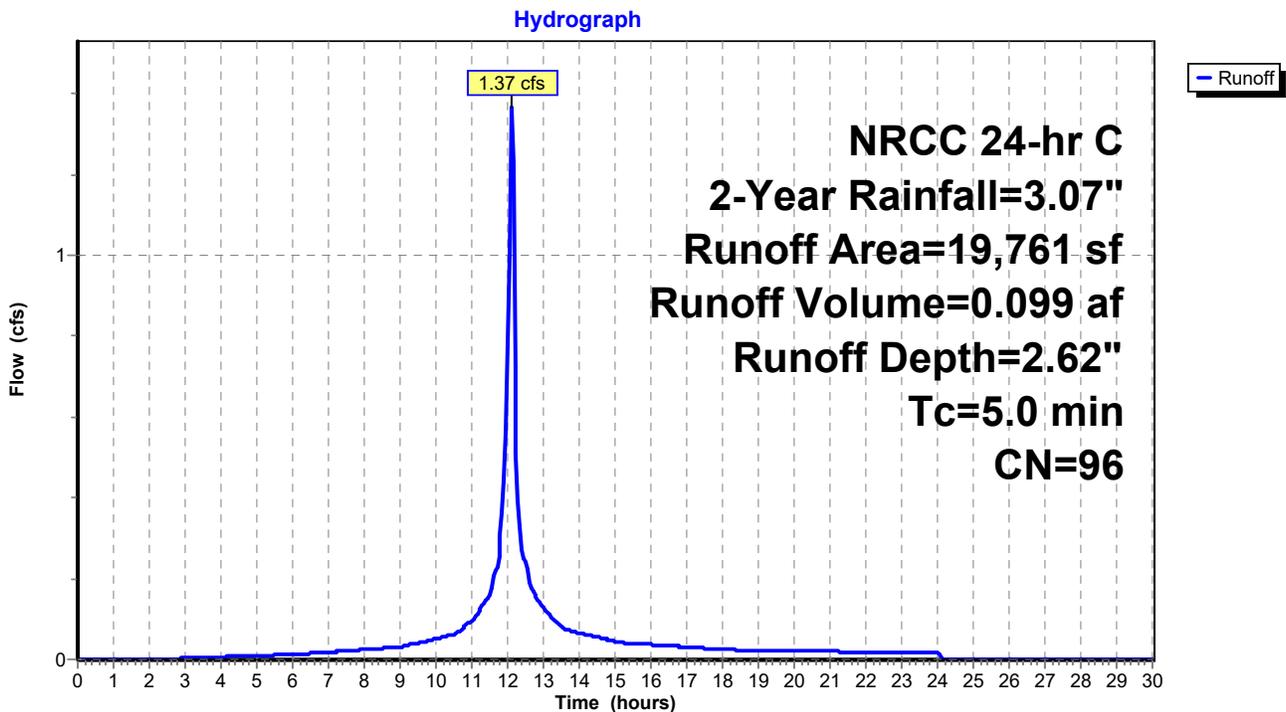
Runoff = 1.37 cfs @ 12.11 hrs, Volume= 0.099 af, Depth= 2.62"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-30.00 hrs, dt= 0.05 hrs
NRCC 24-hr C 2-Year Rainfall=3.07"

	Area (sf)	CN	Description
*	17,647	98	Impervious
	1,300	96	Gravel surface, HSG A
	814	49	50-75% Grass cover, Fair, HSG A
	19,761	96	Weighted Average
	2,114		10.70% Pervious Area
	17,647		89.30% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
5.0					Direct Entry,

Subcatchment P3A: #22 drive and lower parking lots



Summary for Subcatchment P3B: slope below parking

[49] Hint: Tc<2dt may require smaller dt

Runoff = 0.00 cfs @ 16.24 hrs, Volume= 0.001 af, Depth= 0.05"

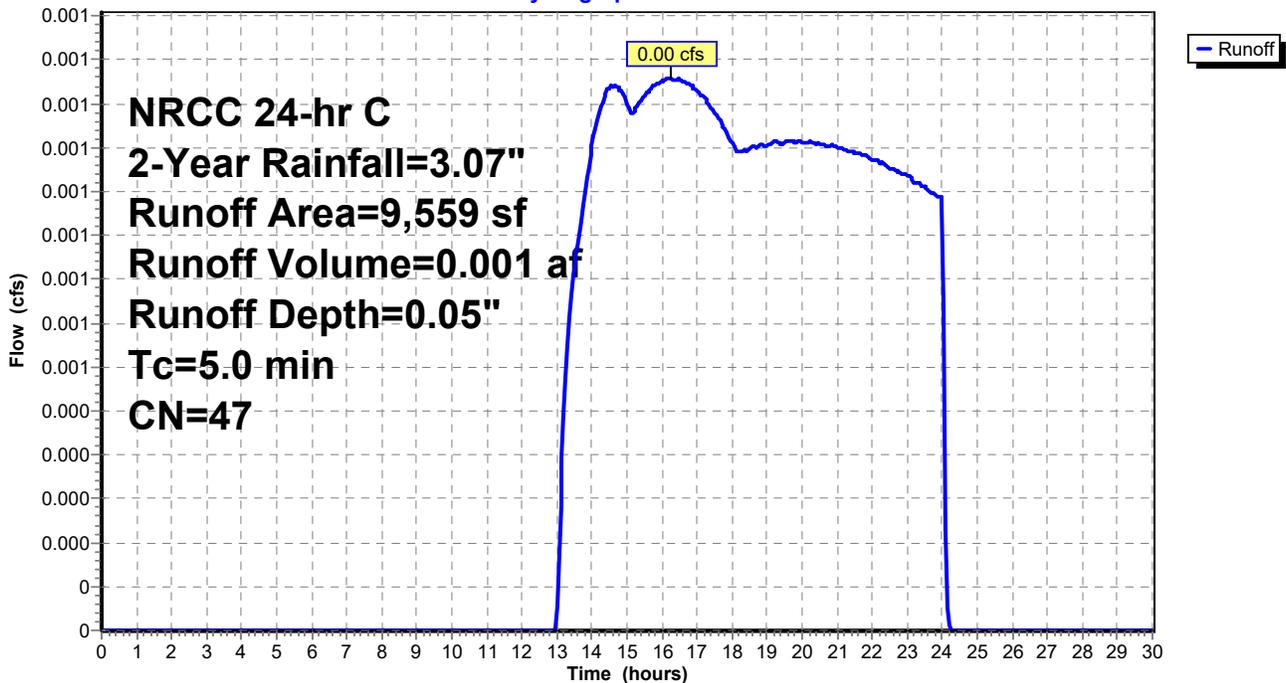
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-30.00 hrs, dt= 0.05 hrs
NRCC 24-hr C 2-Year Rainfall=3.07"

	Area (sf)	CN	Description
*	1,285	98	Impervious
	6,274	36	Woods, Fair, HSG A
	2,000	49	50-75% Grass cover, Fair, HSG A
	9,559	47	Weighted Average
	8,274		86.56% Pervious Area
	1,285		13.44% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
5.0					Direct Entry,

Subcatchment P3B: slope below parking

Hydrograph



Summary for Subcatchment P4: east drainage area

[45] Hint: Runoff=Zero

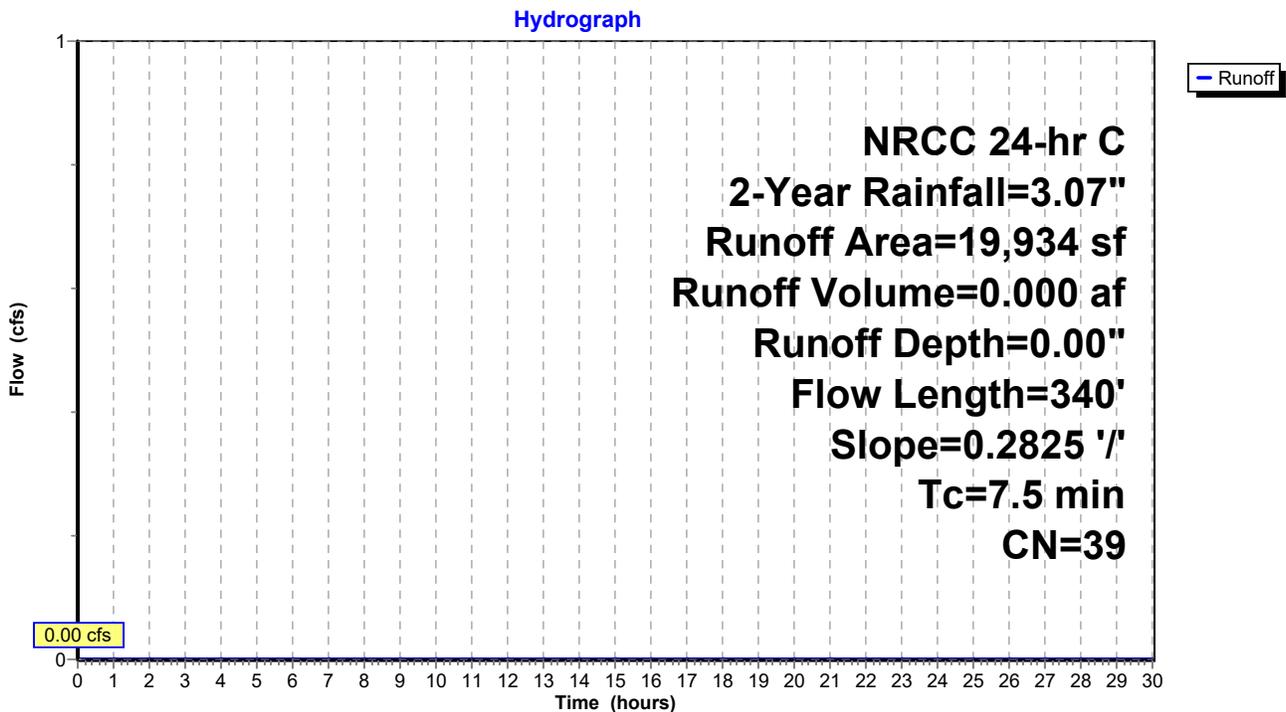
Runoff = 0.00 cfs @ 0.00 hrs, Volume= 0.000 af, Depth= 0.00"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-30.00 hrs, dt= 0.05 hrs
 NRCC 24-hr C 2-Year Rainfall=3.07"

Area (sf)	CN	Description
18,814	36	Woods, Fair, HSG A
* 1,120	98	Impervious
19,934	39	Weighted Average
18,814		94.38% Pervious Area
1,120		5.62% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
7.5	340	0.2825	0.75		Lag/CN Method, Contour Length= 5,632' Interval= 1'

Subcatchment P4: east drainage area



Summary for Subcatchment P4A: part of #22 roof

[49] Hint: Tc<2dt may require smaller dt

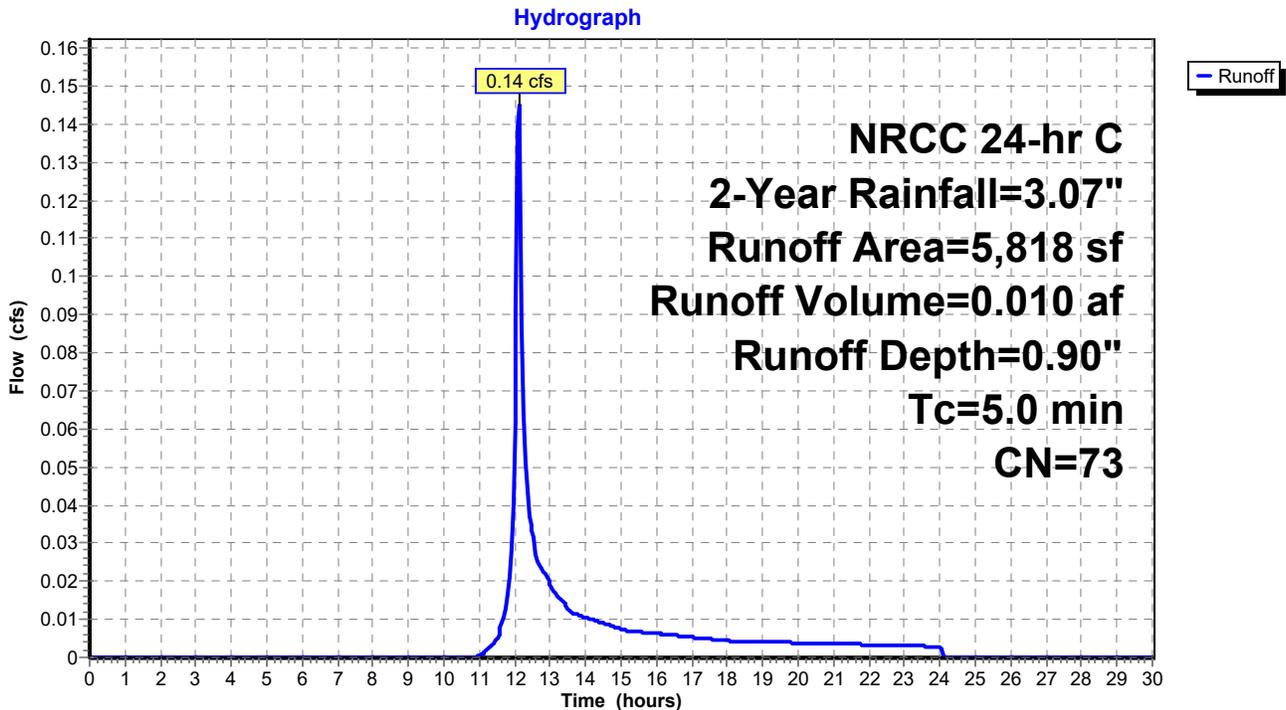
Runoff = 0.14 cfs @ 12.12 hrs, Volume= 0.010 af, Depth= 0.90"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-30.00 hrs, dt= 0.05 hrs
NRCC 24-hr C 2-Year Rainfall=3.07"

Area (sf)	CN	Description
3,455	98	Unconnected roofs, HSG A
2,363	36	Woods, Fair, HSG A
5,818	73	Weighted Average
2,363		40.62% Pervious Area
3,455		59.38% Impervious Area
3,455		100.00% Unconnected

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
5.0					Direct Entry,

Subcatchment P4A: part of #22 roof



Summary for Reach 1R: ex swale

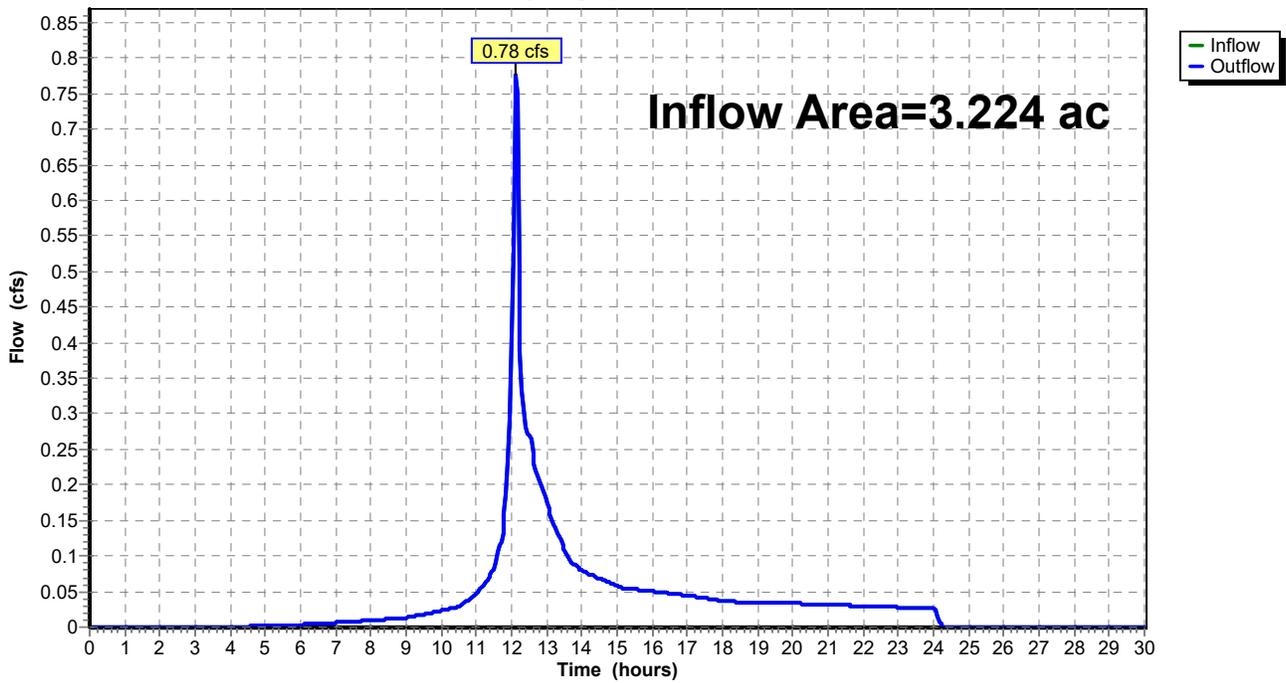
[40] Hint: Not Described (Outflow=Inflow)

Inflow Area = 3.224 ac, 23.86% Impervious, Inflow Depth = 0.32" for 2-Year event
Inflow = 0.78 cfs @ 12.13 hrs, Volume= 0.086 af
Outflow = 0.78 cfs @ 12.13 hrs, Volume= 0.086 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind method, Time Span= 0.00-30.00 hrs, dt= 0.05 hrs

Reach 1R: ex swale

Hydrograph



Summary for Reach 2R: central DA

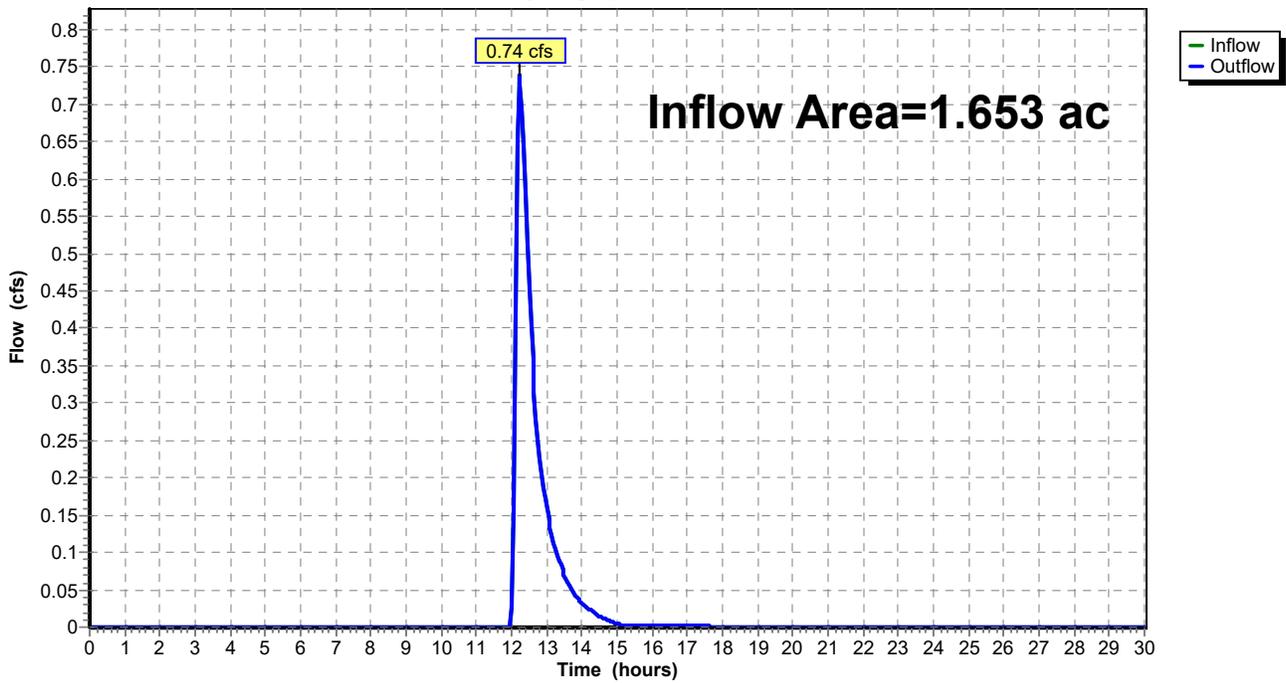
[40] Hint: Not Described (Outflow=Inflow)

Inflow Area = 1.653 ac, 39.84% Impervious, Inflow Depth = 0.30" for 2-Year event
Inflow = 0.74 cfs @ 12.22 hrs, Volume= 0.042 af
Outflow = 0.74 cfs @ 12.22 hrs, Volume= 0.042 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind method, Time Span= 0.00-30.00 hrs, dt= 0.05 hrs

Reach 2R: central DA

Hydrograph



Summary for Reach 3R: East DA

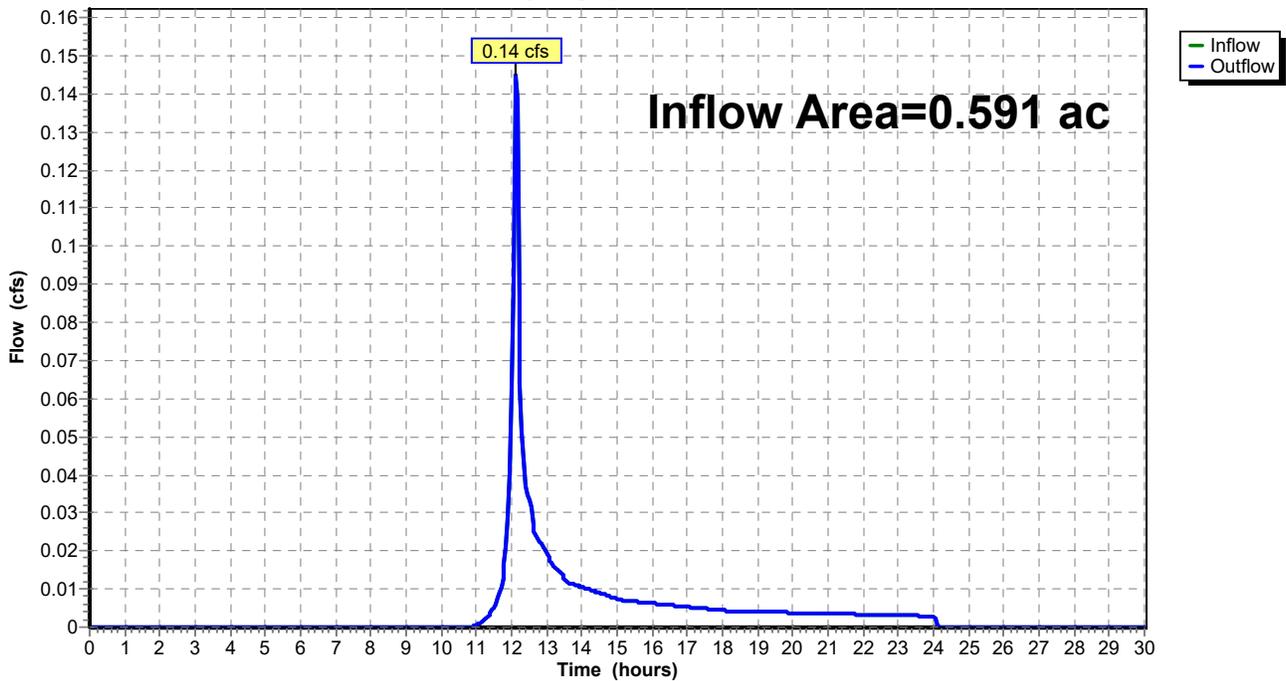
[40] Hint: Not Described (Outflow=Inflow)

Inflow Area = 0.591 ac, 17.77% Impervious, Inflow Depth = 0.20" for 2-Year event
Inflow = 0.14 cfs @ 12.12 hrs, Volume= 0.010 af
Outflow = 0.14 cfs @ 12.12 hrs, Volume= 0.010 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind method, Time Span= 0.00-30.00 hrs, dt= 0.05 hrs

Reach 3R: East DA

Hydrograph



Summary for Reach 4R: (new Reach)

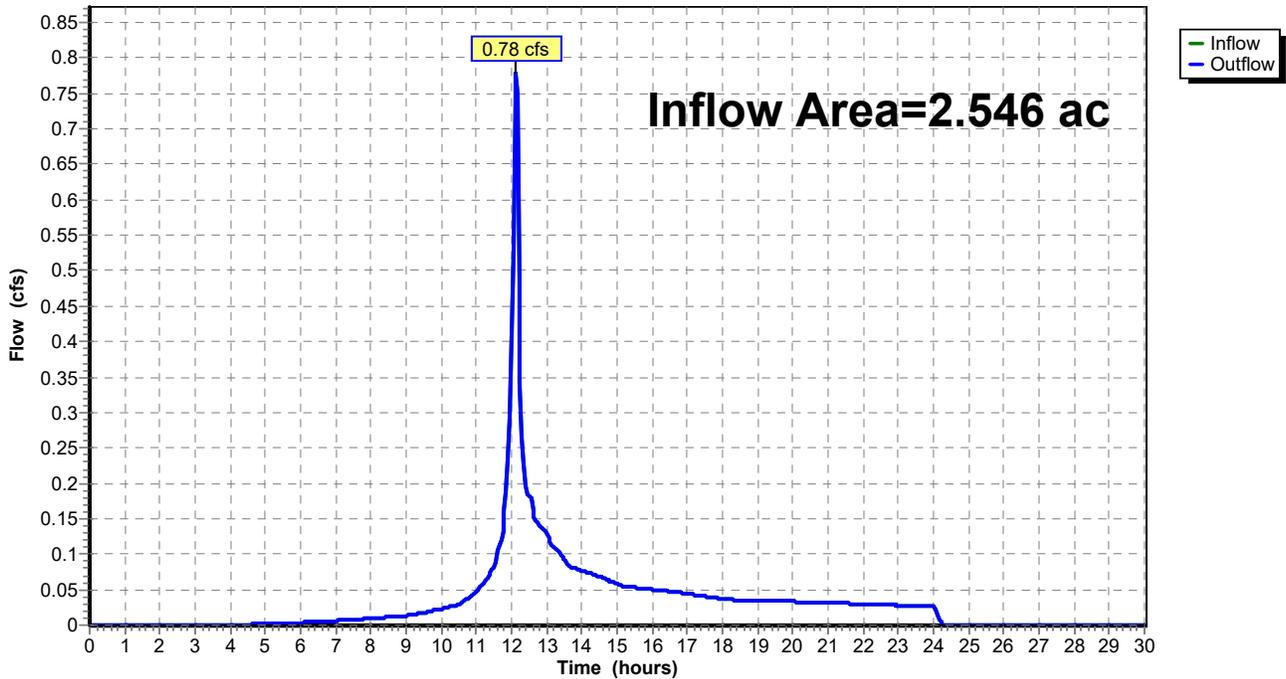
[40] Hint: Not Described (Outflow=Inflow)

Inflow Area = 2.546 ac, 19.18% Impervious, Inflow Depth = 0.38" for 2-Year event
Inflow = 0.78 cfs @ 12.13 hrs, Volume= 0.080 af
Outflow = 0.78 cfs @ 12.13 hrs, Volume= 0.080 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind method, Time Span= 0.00-30.00 hrs, dt= 0.05 hrs

Reach 4R: (new Reach)

Hydrograph



Summary for Pond 1P: UG - system #1

Inflow Area = 0.397 ac, 68.73% Impervious, Inflow Depth = 1.48" for 2-Year event
 Inflow = 0.74 cfs @ 12.12 hrs, Volume= 0.049 af
 Outflow = 0.15 cfs @ 12.47 hrs, Volume= 0.049 af, Atten= 79%, Lag= 21.4 min
 Discarded = 0.06 cfs @ 11.60 hrs, Volume= 0.043 af
 Primary = 0.09 cfs @ 12.47 hrs, Volume= 0.006 af

Routing by Stor-Ind method, Time Span= 0.00-30.00 hrs, dt= 0.05 hrs / 2
 Peak Elev= 305.39' @ 12.47 hrs Surf.Area= 0.027 ac Storage= 0.014 af

Plug-Flow detention time= 53.9 min calculated for 0.049 af (100% of inflow)
 Center-of-Mass det. time= 53.9 min (899.4 - 845.5)

Volume	Invert	Avail.Storage	Storage Description
#1A	304.50'	0.014 af	42.06'W x 27.46'L x 2.44'H Field A 0.065 af Overall - 0.030 af Embedded = 0.035 af x 40.0% Voids
#2A	305.00'	0.028 af	ACF R-Tank HD 1 x 290 Inside #1 Inside= 15.7"W x 17.3"H => 1.80 sf x 2.35'L = 4.2 cf Outside= 15.7"W x 17.3"H => 1.89 sf x 2.35'L = 4.4 cf 290 Chambers in 29 Rows
		0.042 af	Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices
#1	Primary	305.20'	5.0" Vert. Orifice/Grate C= 0.600
#2	Primary	306.40'	8.0" Horiz. Orifice/Grate C= 0.600 Limited to weir flow at low heads
#3	Discarded	304.50'	2.410 in/hr Exfiltration over Surface area Phase-In= 0.01'

Discarded OutFlow Max=0.06 cfs @ 11.60 hrs HW=304.52' (Free Discharge)
 ↳ **3=Exfiltration** (Exfiltration Controls 0.06 cfs)

Primary OutFlow Max=0.09 cfs @ 12.47 hrs HW=305.39' (Free Discharge)
 ↳ **1=Orifice/Grate** (Orifice Controls 0.09 cfs @ 1.47 fps)
 ↳ **2=Orifice/Grate** (Controls 0.00 cfs)

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Pond 1P: UG - system #1 - Chamber Wizard Field A

Chamber Model = ACF R-Tank HD 1 (ACF Environmental R-Tank HD)

Inside= 15.7"W x 17.3"H => 1.80 sf x 2.35'L = 4.2 cf

Outside= 15.7"W x 17.3"H => 1.89 sf x 2.35'L = 4.4 cf

10 Chambers/Row x 2.35' Long = 23.46' Row Length +24.0" End Stone x 2 = 27.46' Base Length

29 Rows x 15.7" Wide + 24.0" Side Stone x 2 = 42.06' Base Width

6.0" Base + 17.3" Chamber Height + 6.0" Cover = 2.44' Field Height

290 Chambers x 4.2 cf = 1,224.3 cf Chamber Storage

290 Chambers x 4.4 cf = 1,288.8 cf Displacement

2,821.9 cf Field - 1,288.8 cf Chambers = 1,533.1 cf Stone x 40.0% Voids = 613.3 cf Stone Storage

Chamber Storage + Stone Storage = 1,837.6 cf = 0.042 af

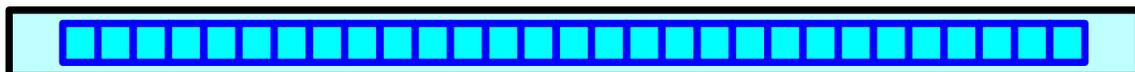
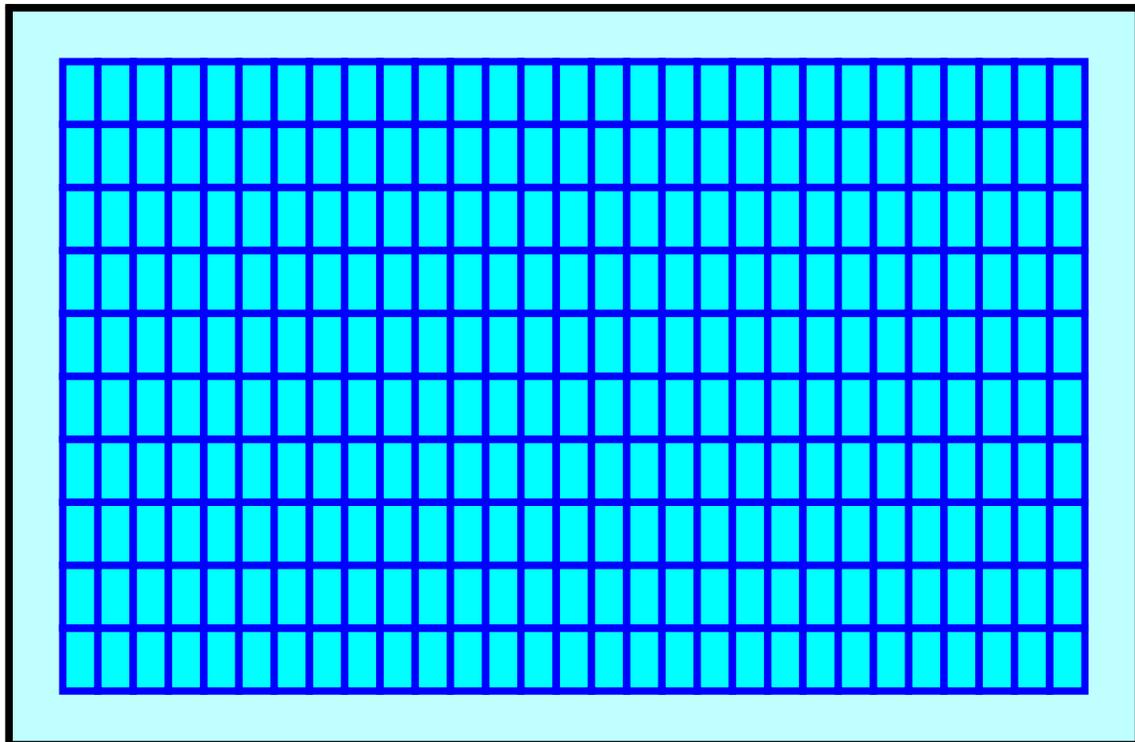
Overall Storage Efficiency = 65.1%

Overall System Size = 27.46' x 42.06' x 2.44'

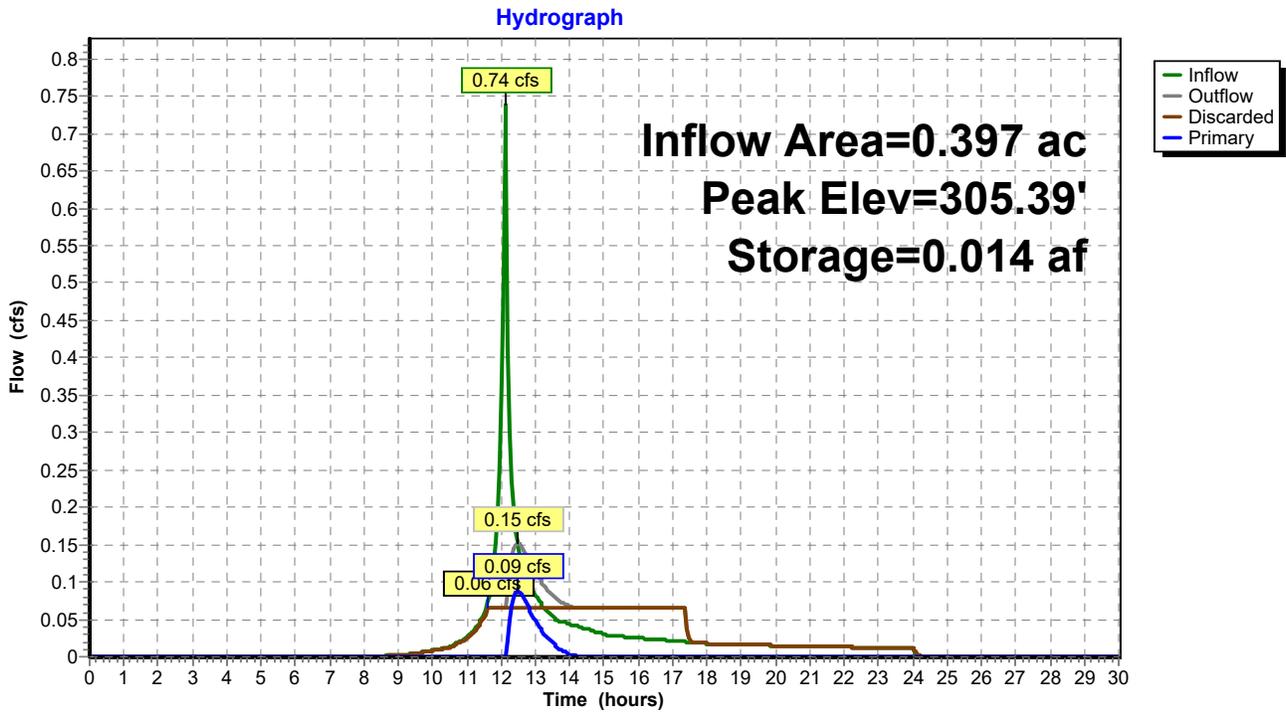
290 Chambers

104.5 cy Field

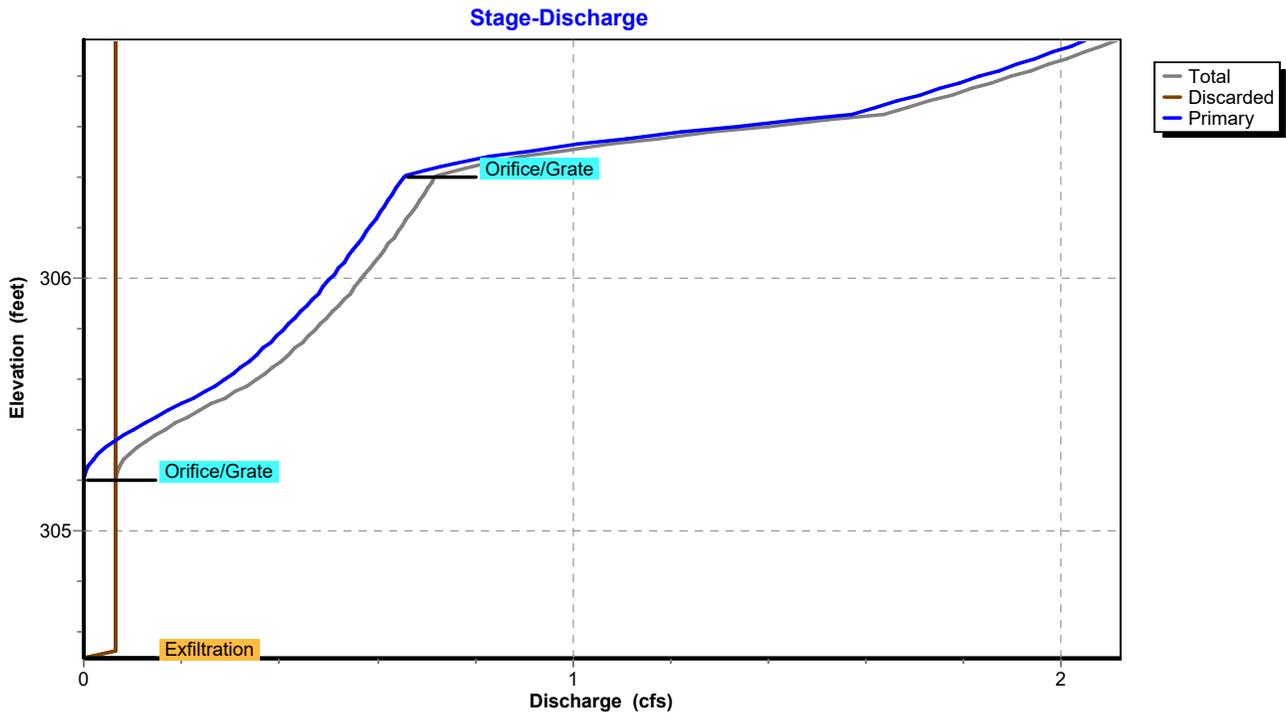
56.8 cy Stone



Pond 1P: UG - system #1



Pond 1P: UG - system #1



Summary for Pond 2P: UG - system #2

Inflow Area = 1.434 ac, 43.88% Impervious, Inflow Depth = 1.09" for 2-Year event
 Inflow = 1.77 cfs @ 12.11 hrs, Volume= 0.130 af
 Outflow = 0.82 cfs @ 12.22 hrs, Volume= 0.130 af, Atten= 54%, Lag= 6.7 min
 Discarded = 0.08 cfs @ 10.65 hrs, Volume= 0.089 af
 Primary = 0.74 cfs @ 12.22 hrs, Volume= 0.041 af

Routing by Stor-Ind method, Time Span= 0.00-30.00 hrs, dt= 0.05 hrs / 3
 Peak Elev= 294.22' @ 12.22 hrs Surf.Area= 0.034 ac Storage= 0.033 af

Plug-Flow detention time= 53.3 min calculated for 0.130 af (100% of inflow)
 Center-of-Mass det. time= 53.2 min (842.8 - 789.6)

Volume	Invert	Avail.Storage	Storage Description
#1A	292.80'	0.020 af	43.37'W x 34.50'L x 3.17'H Field A 0.109 af Overall - 0.060 af Embedded = 0.049 af x 40.0% Voids
#2A	293.30'	0.057 af	ACF R-Tank HD 1.5 x 390 Inside #1 Inside= 15.7"W x 26.0"H => 2.70 sf x 2.35'L = 6.3 cf Outside= 15.7"W x 26.0"H => 2.84 sf x 2.35'L = 6.7 cf 390 Chambers in 30 Rows
		0.076 af	Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices
#1	Primary	293.60'	7.0" Vert. Orifice/Grate C= 0.600
#2	Primary	294.50'	8.0" Vert. Orifice/Grate C= 0.600
#3	Primary	295.80'	12.0" Horiz. Orifice/Grate C= 0.600 Limited to weir flow at low heads
#4	Discarded	292.80'	2.410 in/hr Exfiltration over Surface area Phase-In= 0.01'

Discarded OutFlow Max=0.08 cfs @ 10.65 hrs HW=292.83' (Free Discharge)
 ↳4=Exfiltration (Exfiltration Controls 0.08 cfs)

Primary OutFlow Max=0.73 cfs @ 12.22 hrs HW=294.21' (Free Discharge)
 ↳1=Orifice/Grate (Orifice Controls 0.73 cfs @ 2.73 fps)
 ↳2=Orifice/Grate (Controls 0.00 cfs)
 ↳3=Orifice/Grate (Controls 0.00 cfs)

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Pond 2P: UG - system #2 - Chamber Wizard Field A

Chamber Model = ACF R-Tank HD 1.5 (ACF Environmental R-Tank HD)

Inside= 15.7"W x 26.0"H => 2.70 sf x 2.35'L = 6.3 cf

Outside= 15.7"W x 26.0"H => 2.84 sf x 2.35'L = 6.7 cf

13 Chambers/Row x 2.35' Long = 30.50' Row Length +24.0" End Stone x 2 = 34.50' Base Length

30 Rows x 15.7" Wide + 24.0" Side Stone x 2 = 43.37' Base Width

6.0" Base + 26.0" Chamber Height + 6.0" Cover = 3.17' Field Height

390 Chambers x 6.3 cf = 2,469.8 cf Chamber Storage

390 Chambers x 6.7 cf = 2,599.7 cf Displacement

4,735.6 cf Field - 2,599.7 cf Chambers = 2,135.8 cf Stone x 40.0% Voids = 854.3 cf Stone Storage

Chamber Storage + Stone Storage = 3,324.1 cf = 0.076 af

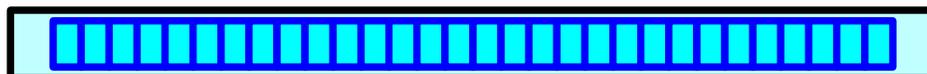
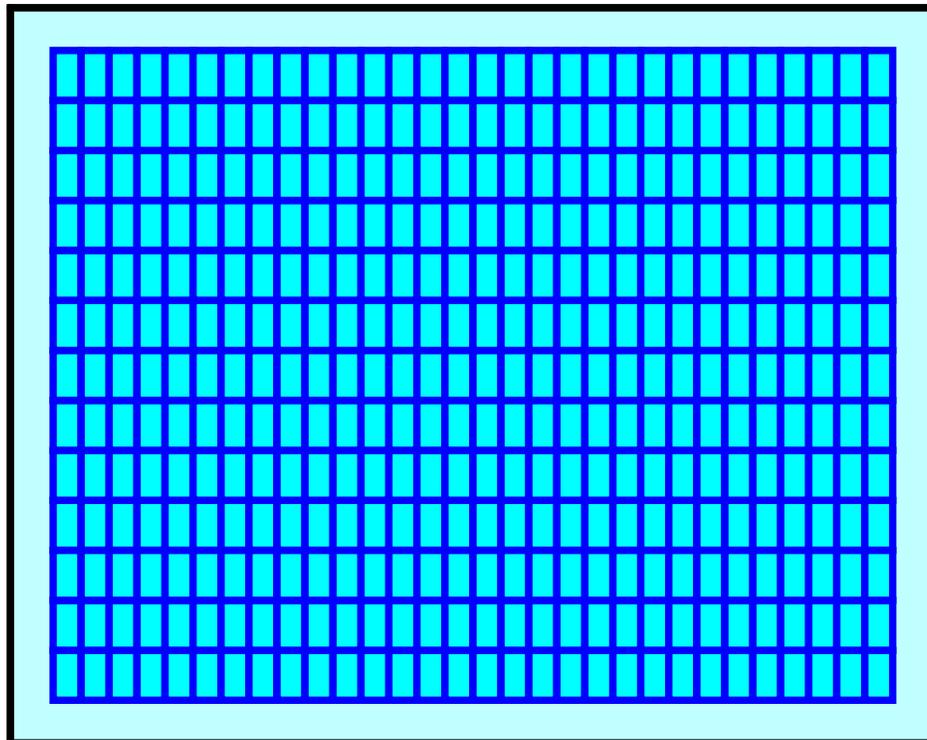
Overall Storage Efficiency = 70.2%

Overall System Size = 34.50' x 43.37' x 3.17'

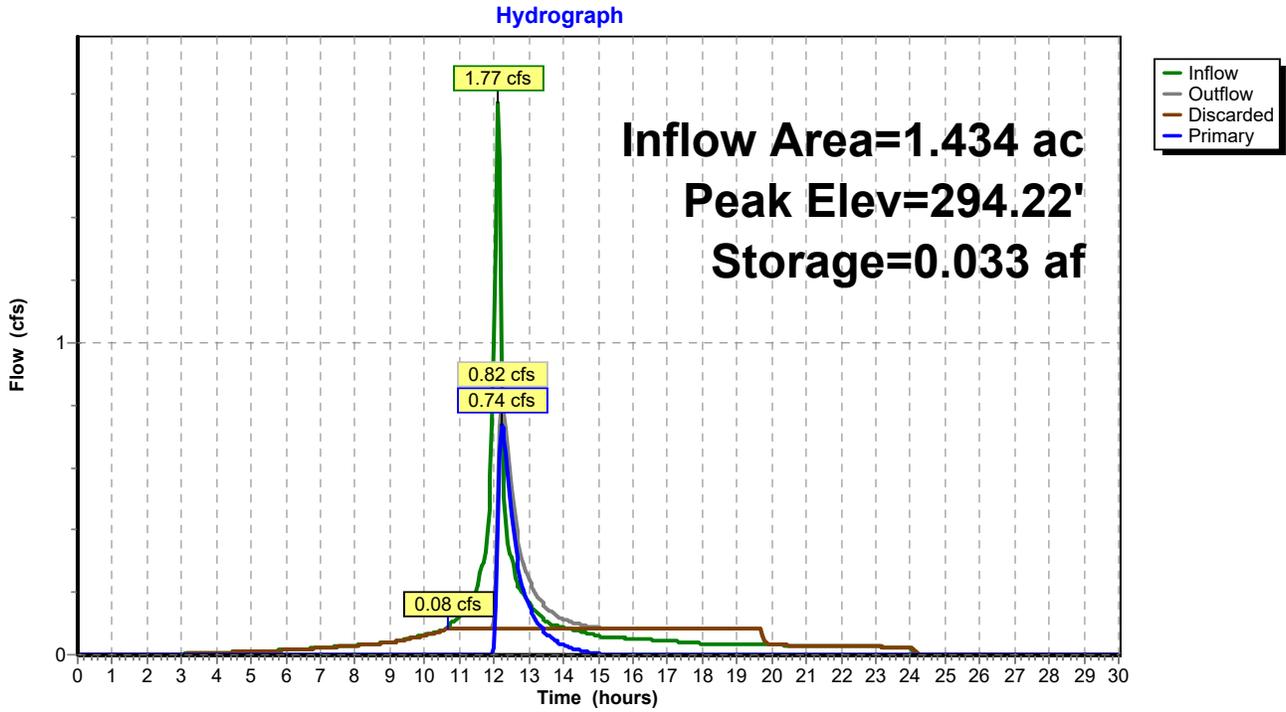
390 Chambers

175.4 cy Field

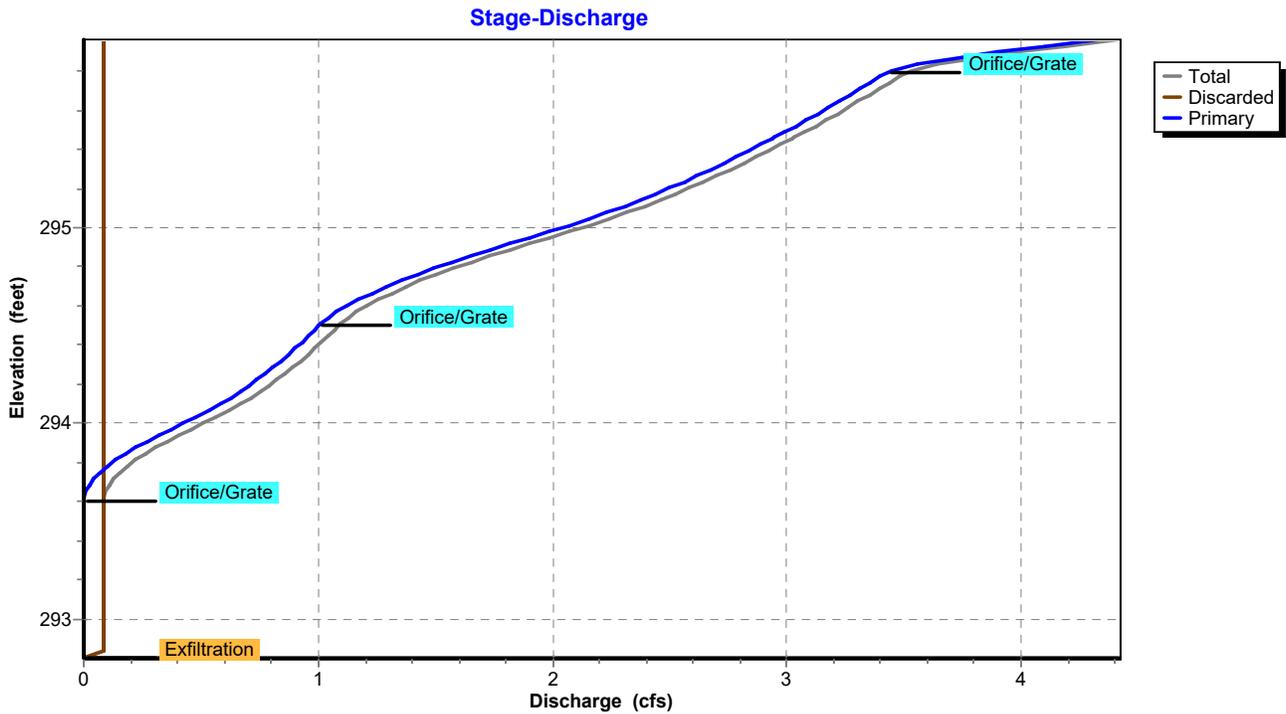
79.1 cy Stone



Pond 2P: UG - system #2



Pond 2P: UG - system #2

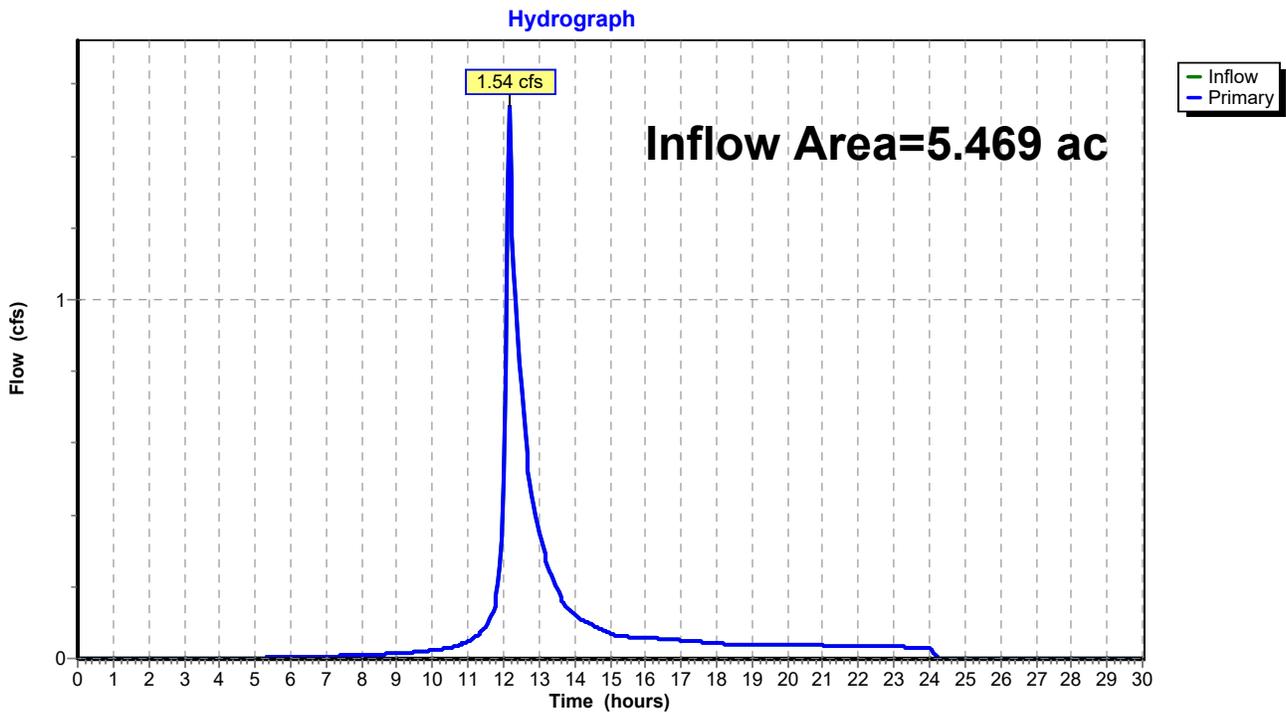


Summary for Link 1L: STUDY POINT- Amethyst Brook

Inflow Area = 5.469 ac, 28.03% Impervious, Inflow Depth = 0.30" for 2-Year event
Inflow = 1.54 cfs @ 12.15 hrs, Volume= 0.138 af
Primary = 1.54 cfs @ 12.15 hrs, Volume= 0.138 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-30.00 hrs, dt= 0.05 hrs

Link 1L: STUDY POINT- Amethyst Brook



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Summary for Subcatchment P1: South of Amherst Road

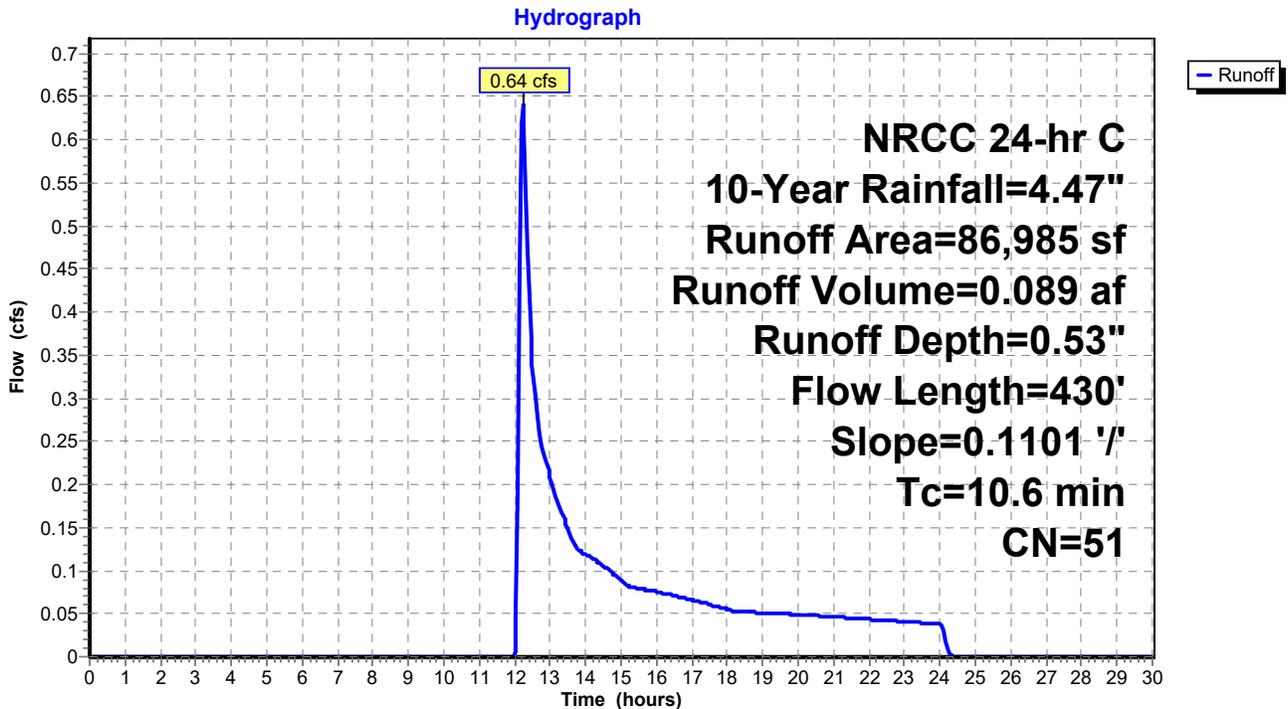
Runoff = 0.64 cfs @ 12.22 hrs, Volume= 0.089 af, Depth= 0.53"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-30.00 hrs, dt= 0.05 hrs
NRCC 24-hr C 10-Year Rainfall=4.47"

	Area (sf)	CN	Description
*	7,024	98	Impervious HSG A
*	806	98	Impervious HSG B
	39,100	36	Woods, Fair, HSG A
	30,655	60	Woods, Fair, HSG B
	9,400	49	50-75% Grass cover, Fair, HSG A
	86,985	51	Weighted Average
	79,155		91.00% Pervious Area
	7,830		9.00% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
10.6	430	0.1101	0.68		Lag/CN Method, Contour Length= 9,580' Interval= 1'

Subcatchment P1: South of Amherst Road



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Summary for Subcatchment P1A: Amherst rd

[49] Hint: Tc<2dt may require smaller dt

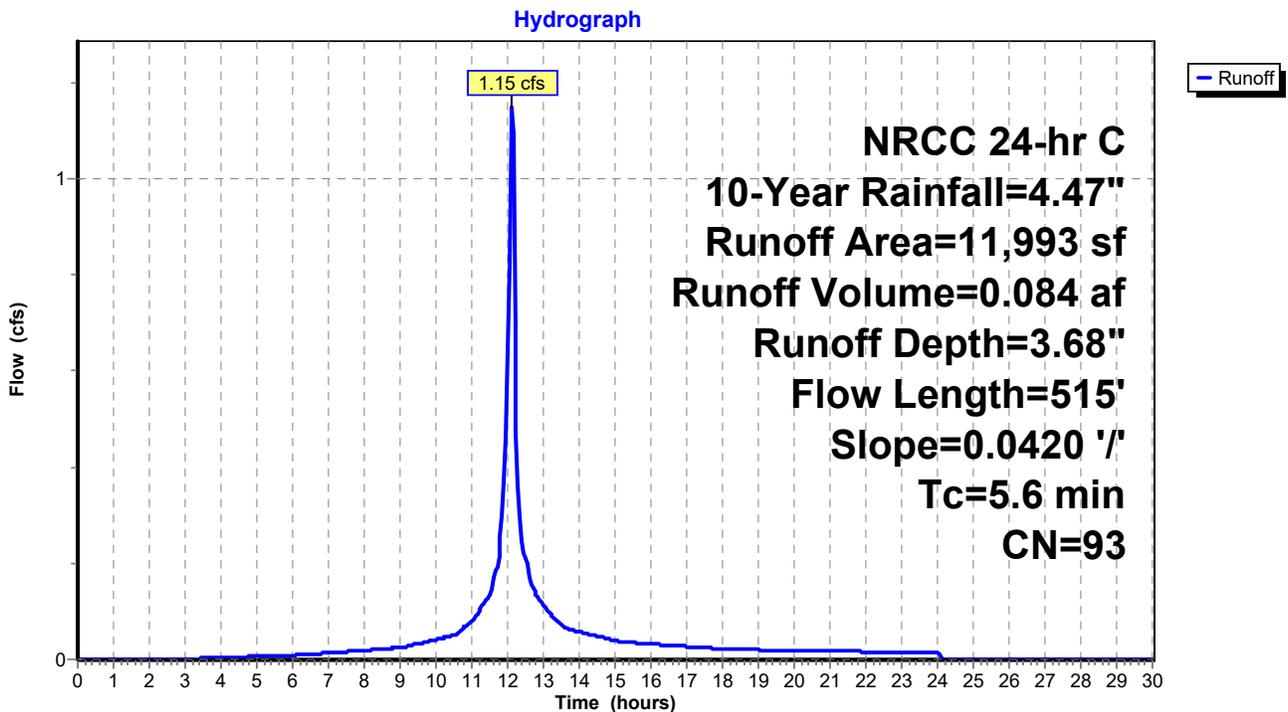
Runoff = 1.15 cfs @ 12.12 hrs, Volume= 0.084 af, Depth= 3.68"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-30.00 hrs, dt= 0.05 hrs
NRCC 24-hr C 10-Year Rainfall=4.47"

	Area (sf)	CN	Description
*	10,800	98	Paved road, HSG A
	1,193	49	50-75% Grass cover, Fair, HSG A
	11,993	93	Weighted Average
	1,193		9.95% Pervious Area
	10,800		90.05% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
5.6	515	0.0420	1.53		Lag/CN Method, Contour Length= 504' Interval= 1'

Subcatchment P1A: Amherst rd



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Summary for Subcatchment P2A: Part of #20 and 24 impervious

[49] Hint: $T_c < 2dt$ may require smaller dt

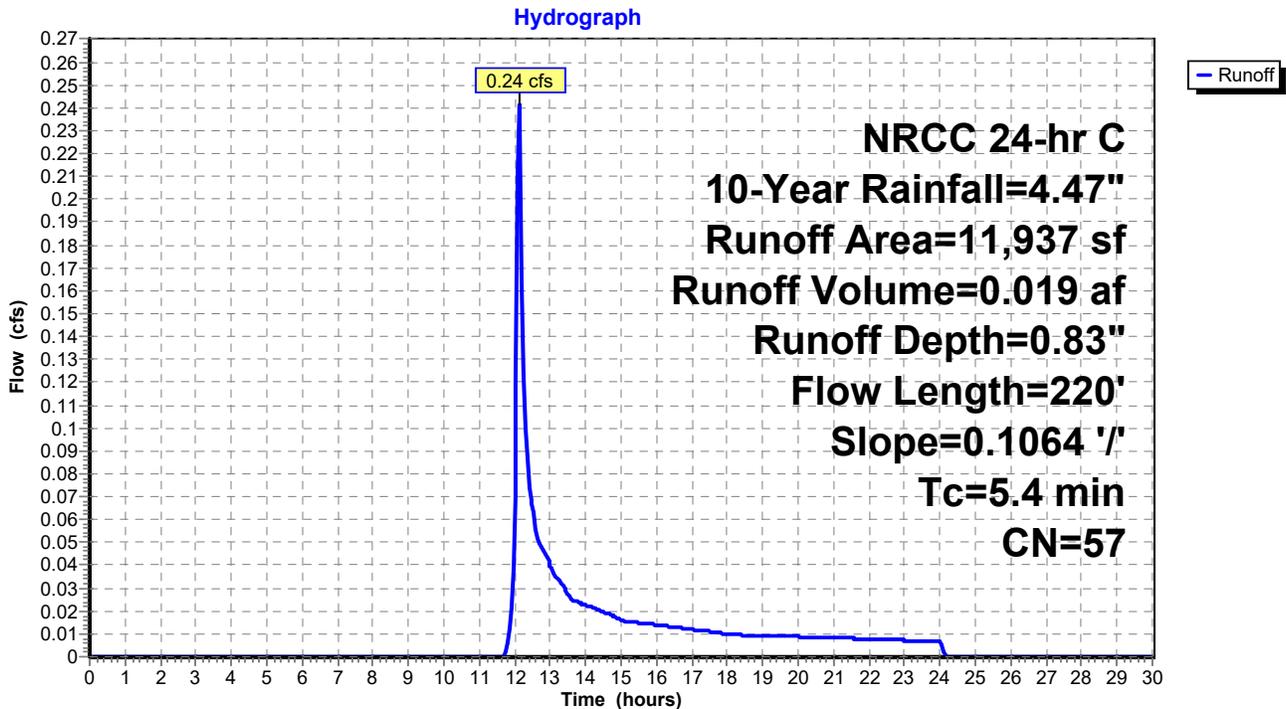
Runoff = 0.24 cfs @ 12.14 hrs, Volume= 0.019 af, Depth= 0.83"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-30.00 hrs, dt= 0.05 hrs
NRCC 24-hr C 10-Year Rainfall=4.47"

	Area (sf)	CN	Description
*	2,647	98	Impervious HSG A
	7,000	49	50-75% Grass cover, Fair, HSG A
	2,290	36	Woods, Fair, HSG A
	11,937	57	Weighted Average
	9,290		77.83% Pervious Area
	2,647		22.17% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
5.4	220	0.1064	0.68		Lag/CN Method, Contour Length= 1,270' Interval= 1'

Subcatchment P2A: Part of #20 and 24 impervious



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NRCC 24-hr C 10-Year Rainfall=4.47"

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Summary for Subcatchment P2B: slope below driveway

[49] Hint: $T_c < 2dt$ may require smaller dt

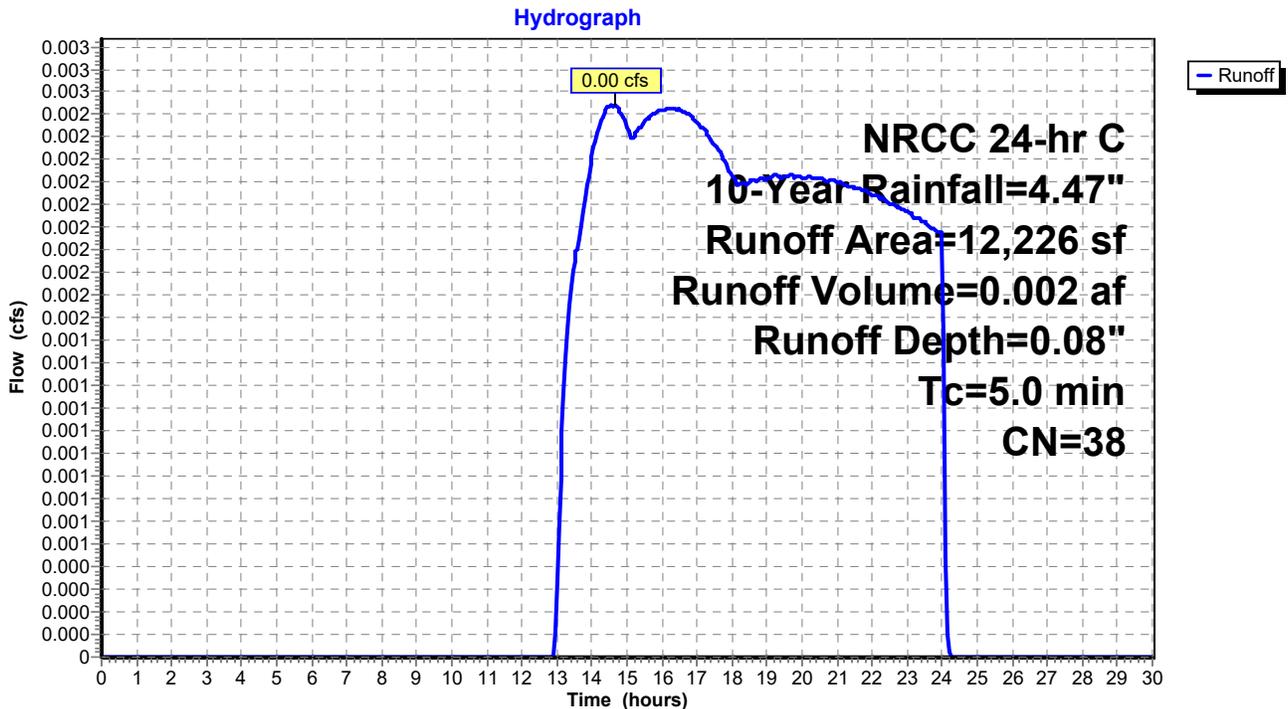
Runoff = 0.00 cfs @ 14.64 hrs, Volume= 0.002 af, Depth= 0.08"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-30.00 hrs, $dt= 0.05$ hrs
 NRCC 24-hr C 10-Year Rainfall=4.47"

Area (sf)	CN	Description
11,888	36	Woods, Fair, HSG A
* 338	98	Wall
12,226	38	Weighted Average
11,888		97.24% Pervious Area
338		2.76% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
5.0					Direct Entry,

Subcatchment P2B: slope below driveway



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NRCC 24-hr C 10-Year Rainfall=4.47"

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Summary for Subcatchment P2C: Entrance drive

[49] Hint: $T_c < 2dt$ may require smaller dt

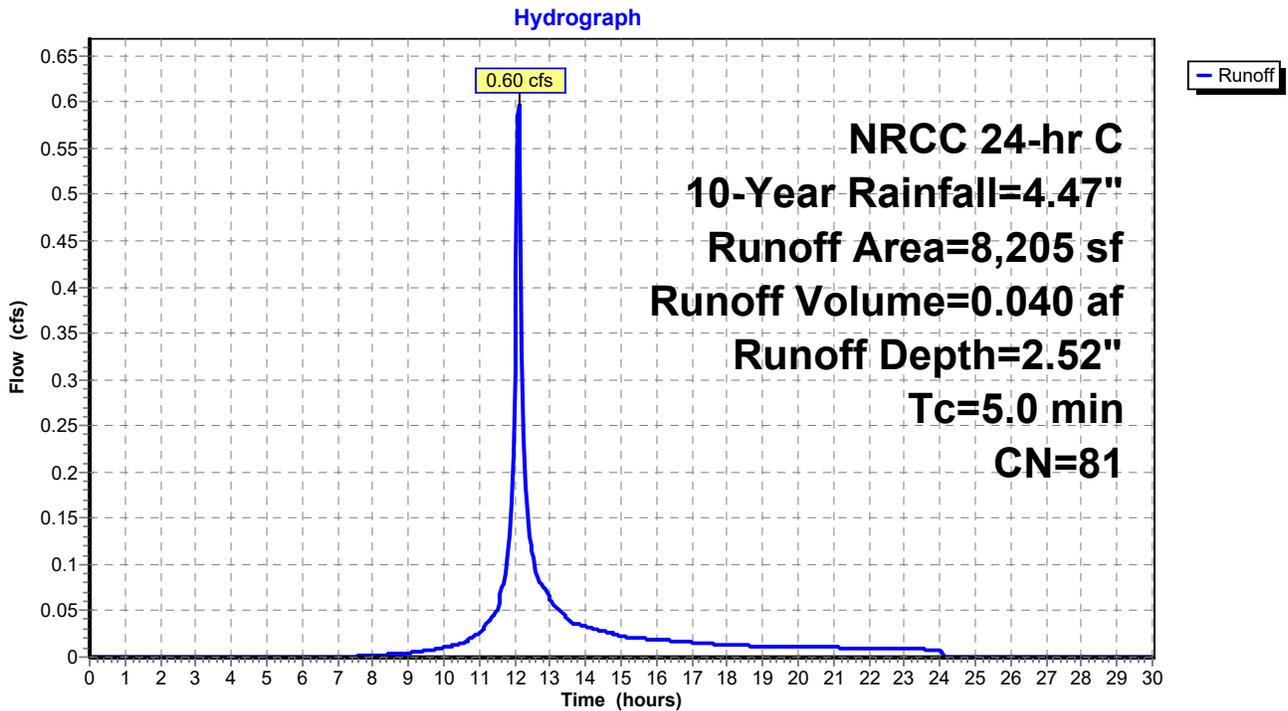
Runoff = 0.60 cfs @ 12.12 hrs, Volume= 0.040 af, Depth= 2.52"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-30.00 hrs, $dt= 0.05$ hrs
NRCC 24-hr C 10-Year Rainfall=4.47"

	Area (sf)	CN	Description
*	5,389	98	Impervious
	2,816	49	50-75% Grass cover, Fair, HSG A
	8,205	81	Weighted Average
	2,816		34.32% Pervious Area
	5,389		65.68% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
5.0					Direct Entry,

Subcatchment P2C: Entrance drive



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Summary for Subcatchment P2D: Parking lot and Roof

[49] Hint: Tc<2dt may require smaller dt

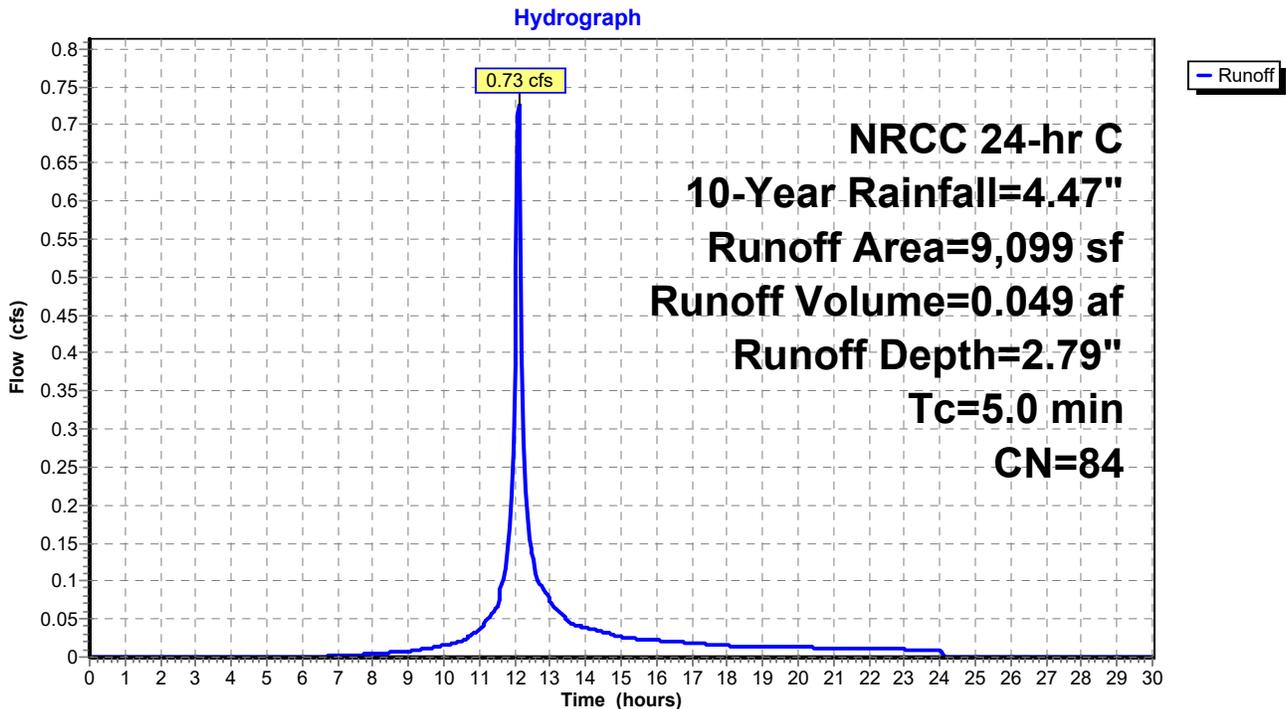
Runoff = 0.73 cfs @ 12.11 hrs, Volume= 0.049 af, Depth= 2.79"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-30.00 hrs, dt= 0.05 hrs
NRCC 24-hr C 10-Year Rainfall=4.47"

	Area (sf)	CN	Description
*	6,504	98	Impervious
	2,595	49	50-75% Grass cover, Fair, HSG A
	9,099	84	Weighted Average
	2,595		28.52% Pervious Area
	6,504		71.48% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
5.0					Direct Entry,

Subcatchment P2D: Parking lot and Roof



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NRCC 24-hr C 10-Year Rainfall=4.47"

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Summary for Subcatchment P2E: Driveway and back roof

[49] Hint: Tc<2dt may require smaller dt

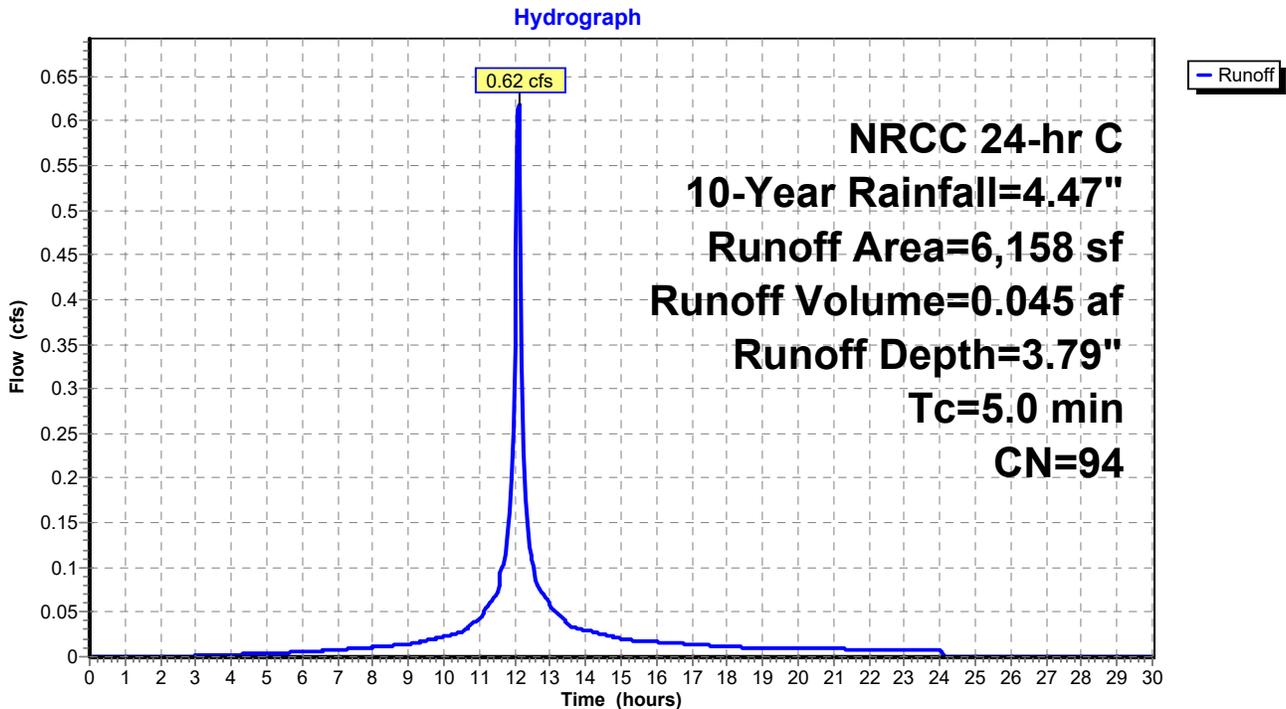
Runoff = 0.62 cfs @ 12.11 hrs, Volume= 0.045 af, Depth= 3.79"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-30.00 hrs, dt= 0.05 hrs
NRCC 24-hr C 10-Year Rainfall=4.47"

	Area (sf)	CN	Description
*	4,254	98	Impervious
	653	96	Gravel surface, HSG A
	451	49	50-75% Grass cover, Fair, HSG A
*	800	98	Impervious - roof
	6,158	94	Weighted Average
	1,104		17.93% Pervious Area
	5,054		82.07% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
5.0					Direct Entry,

Subcatchment P2E: Driveway and back roof



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Summary for Subcatchment P3: part of #24 impervious + wooded slope

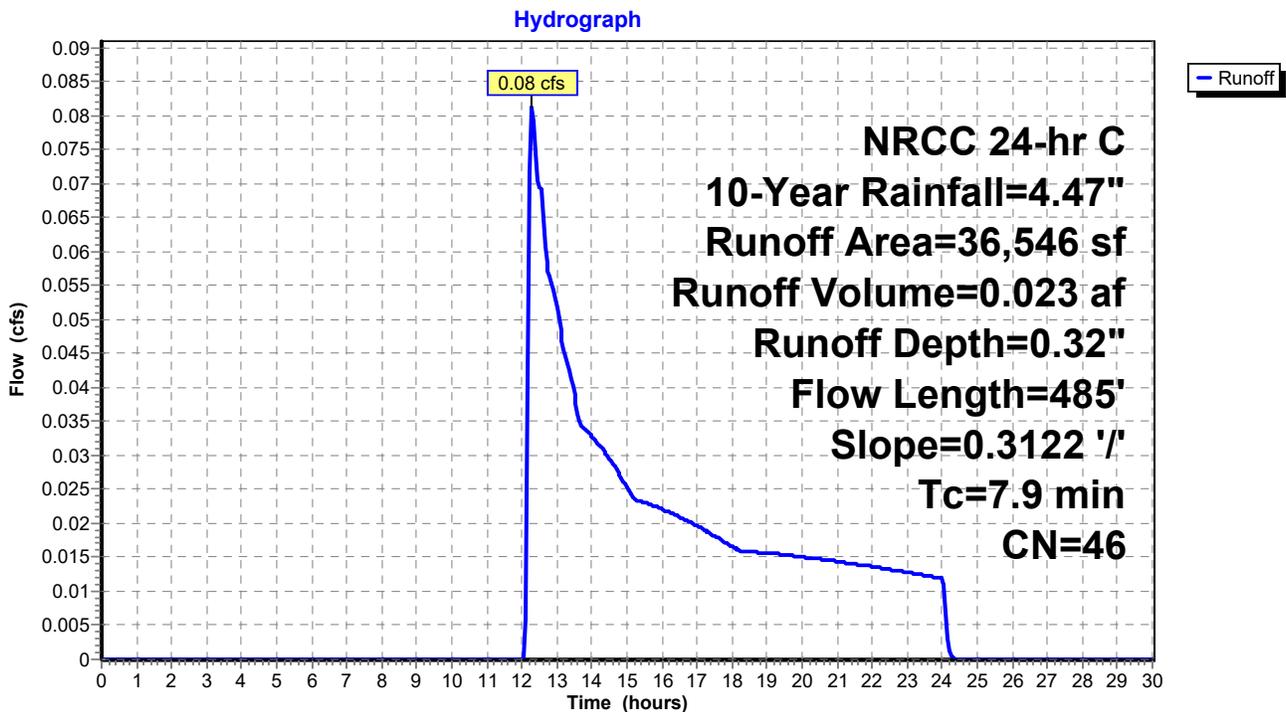
Runoff = 0.08 cfs @ 12.29 hrs, Volume= 0.023 af, Depth= 0.32"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-30.00 hrs, dt= 0.05 hrs
NRCC 24-hr C 10-Year Rainfall=4.47"

Area (sf)	CN	Description
* 4,706	98	Impervious
26,390	36	Woods, Fair, HSG A
5,000	49	50-75% Grass cover, Fair, HSG A
450	49	50-75% Grass cover, Fair, HSG A
36,546	46	Weighted Average
31,840		87.12% Pervious Area
4,706		12.88% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
7.9	485	0.3122	1.03		Lag/CN Method, Contour Length= 11,408' Interval= 1'

Subcatchment P3: part of #24 impervious + wooded slope



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Summary for Subcatchment P3A: #22 drive and lower parking lots

[49] Hint: Tc<2dt may require smaller dt

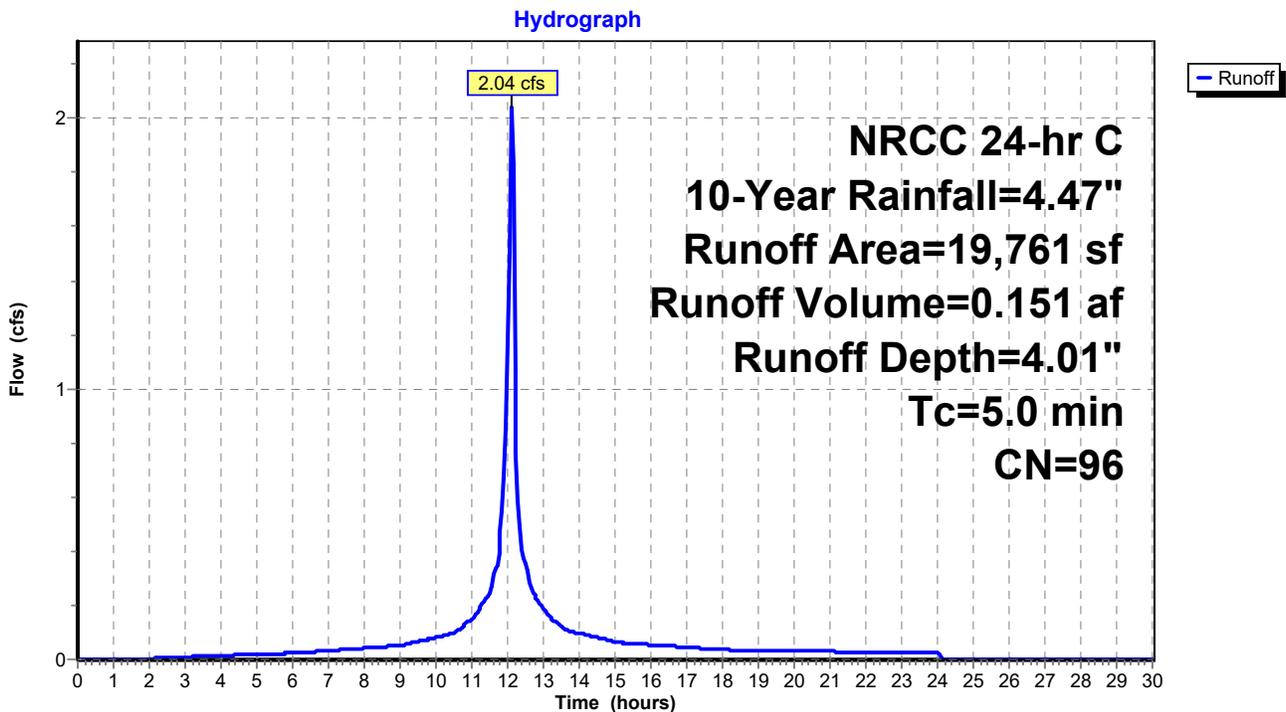
Runoff = 2.04 cfs @ 12.11 hrs, Volume= 0.151 af, Depth= 4.01"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-30.00 hrs, dt= 0.05 hrs
NRCC 24-hr C 10-Year Rainfall=4.47"

	Area (sf)	CN	Description
*	17,647	98	Impervious
	1,300	96	Gravel surface, HSG A
	814	49	50-75% Grass cover, Fair, HSG A
	19,761	96	Weighted Average
	2,114		10.70% Pervious Area
	17,647		89.30% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
5.0					Direct Entry,

Subcatchment P3A: #22 drive and lower parking lots



Summary for Subcatchment P3B: slope below parking

[49] Hint: $T_c < 2dt$ may require smaller dt

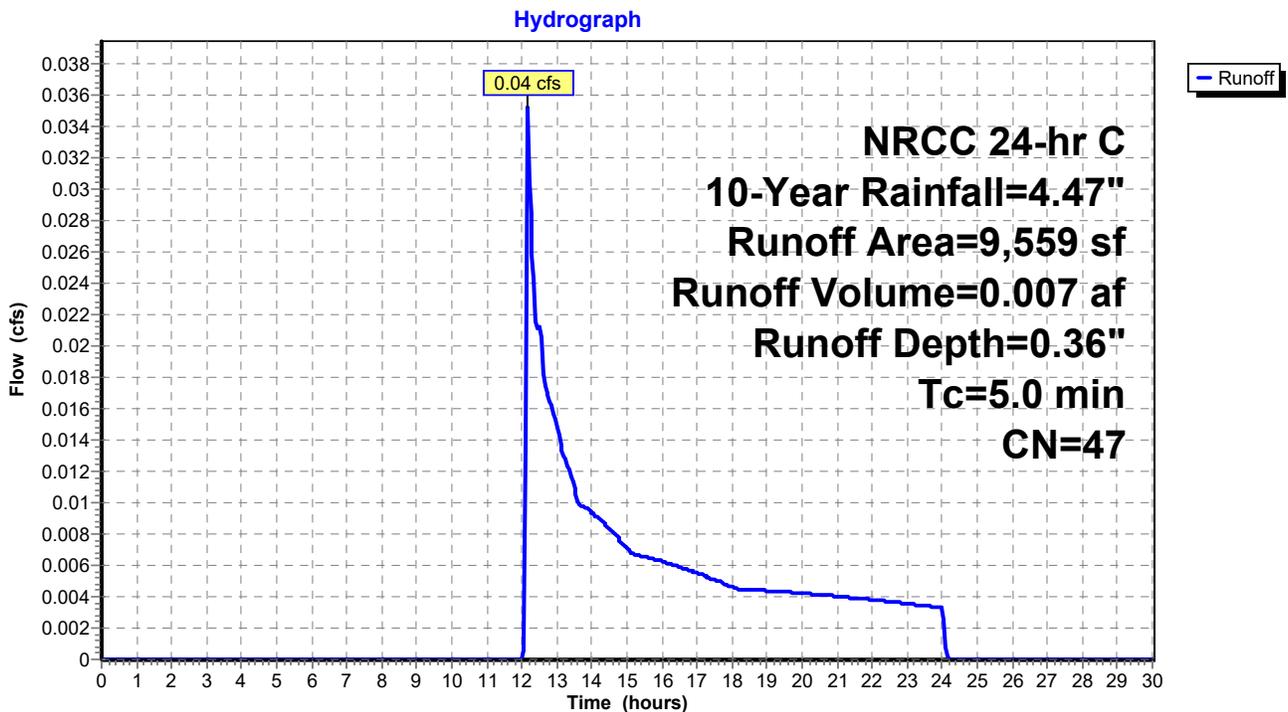
Runoff = 0.04 cfs @ 12.17 hrs, Volume= 0.007 af, Depth= 0.36"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-30.00 hrs, dt= 0.05 hrs
NRCC 24-hr C 10-Year Rainfall=4.47"

	Area (sf)	CN	Description
*	1,285	98	Impervious
	6,274	36	Woods, Fair, HSG A
	2,000	49	50-75% Grass cover, Fair, HSG A
	9,559	47	Weighted Average
	8,274		86.56% Pervious Area
	1,285		13.44% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
5.0					Direct Entry,

Subcatchment P3B: slope below parking



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Summary for Subcatchment P4: east drainage area

Runoff = 0.01 cfs @ 14.36 hrs, Volume= 0.004 af, Depth= 0.11"

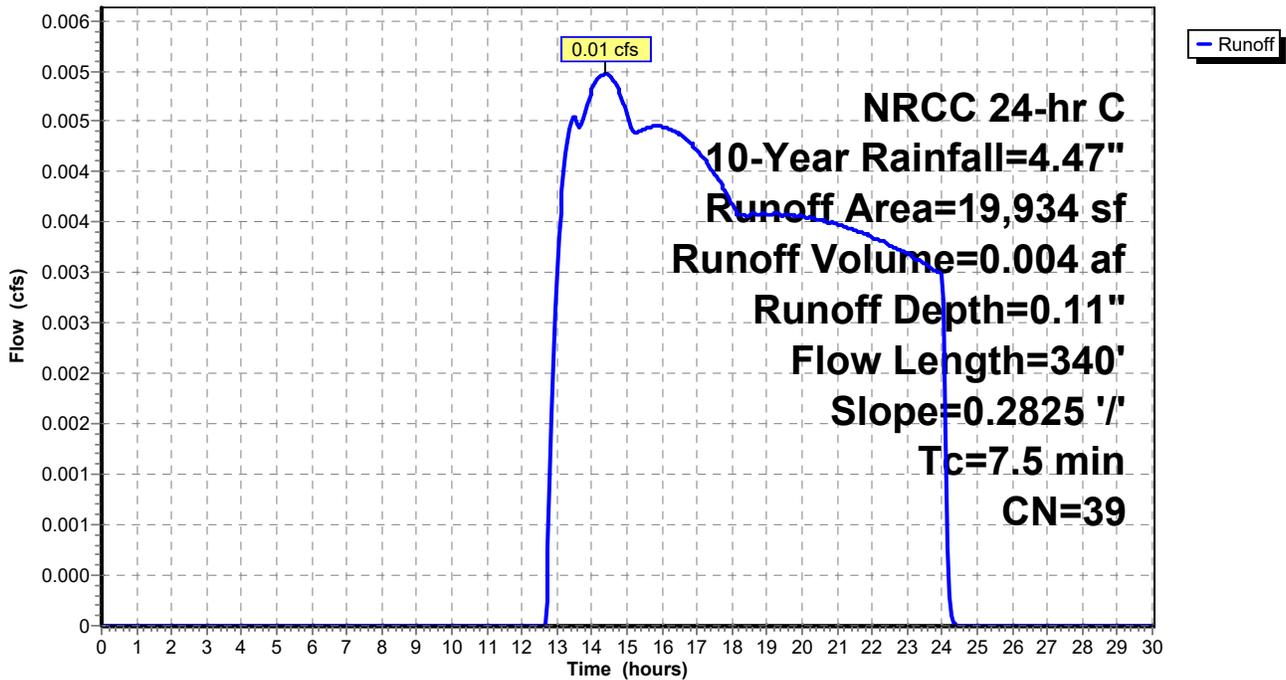
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-30.00 hrs, dt= 0.05 hrs
NRCC 24-hr C 10-Year Rainfall=4.47"

Area (sf)	CN	Description
18,814	36	Woods, Fair, HSG A
* 1,120	98	Impervious
19,934	39	Weighted Average
18,814		94.38% Pervious Area
1,120		5.62% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
7.5	340	0.2825	0.75		Lag/CN Method, Contour Length= 5,632' Interval= 1'

Subcatchment P4: east drainage area

Hydrograph



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Summary for Subcatchment P4A: part of #22 roof

[49] Hint: Tc<2dt may require smaller dt

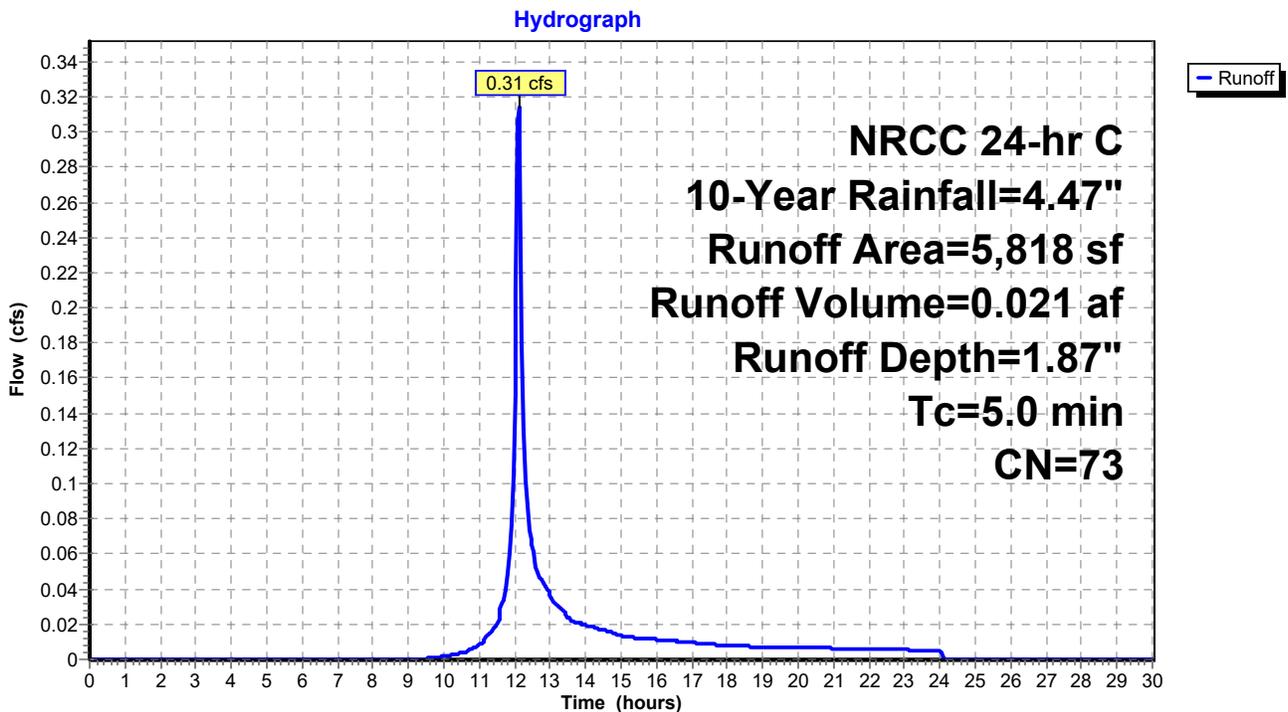
Runoff = 0.31 cfs @ 12.12 hrs, Volume= 0.021 af, Depth= 1.87"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-30.00 hrs, dt= 0.05 hrs
NRCC 24-hr C 10-Year Rainfall=4.47"

Area (sf)	CN	Description
3,455	98	Unconnected roofs, HSG A
2,363	36	Woods, Fair, HSG A
5,818	73	Weighted Average
2,363		40.62% Pervious Area
3,455		59.38% Impervious Area
3,455		100.00% Unconnected

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
5.0					Direct Entry,

Subcatchment P4A: part of #22 roof



Summary for Reach 1R: ex swale

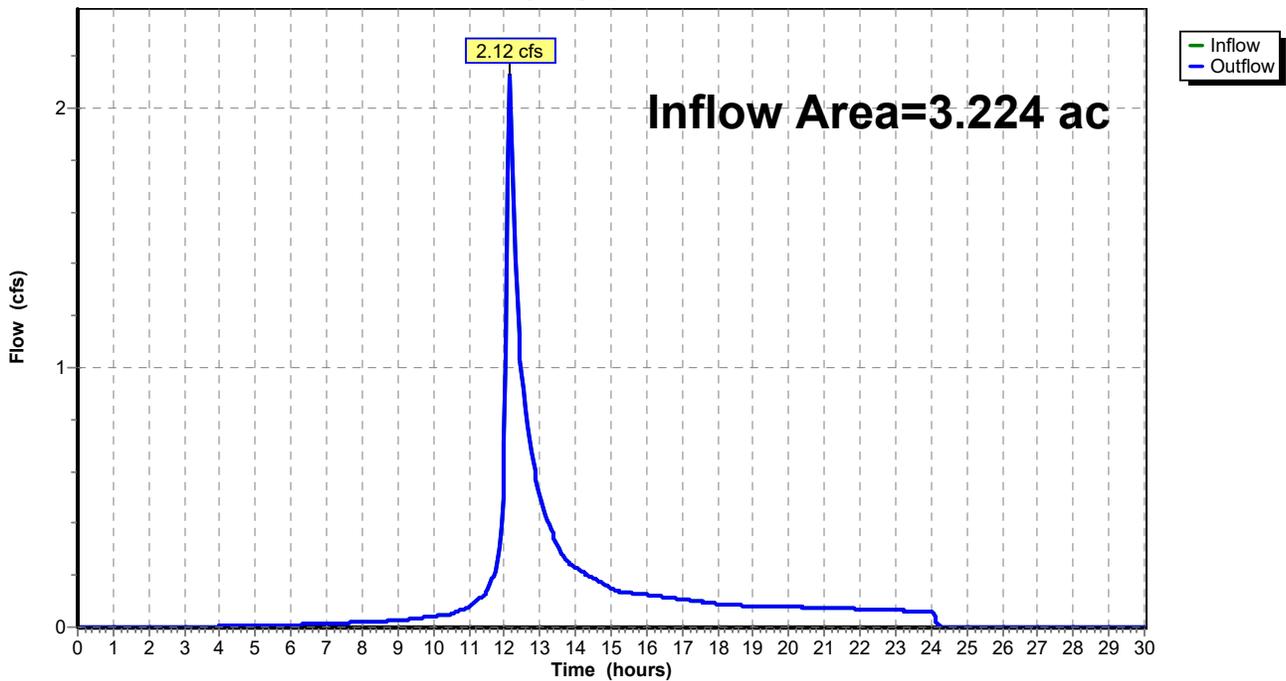
[40] Hint: Not Described (Outflow=Inflow)

Inflow Area = 3.224 ac, 23.86% Impervious, Inflow Depth = 0.84" for 10-Year event
Inflow = 2.12 cfs @ 12.16 hrs, Volume= 0.224 af
Outflow = 2.12 cfs @ 12.16 hrs, Volume= 0.224 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind method, Time Span= 0.00-30.00 hrs, dt= 0.05 hrs

Reach 1R: ex swale

Hydrograph



Summary for Reach 2R: central DA

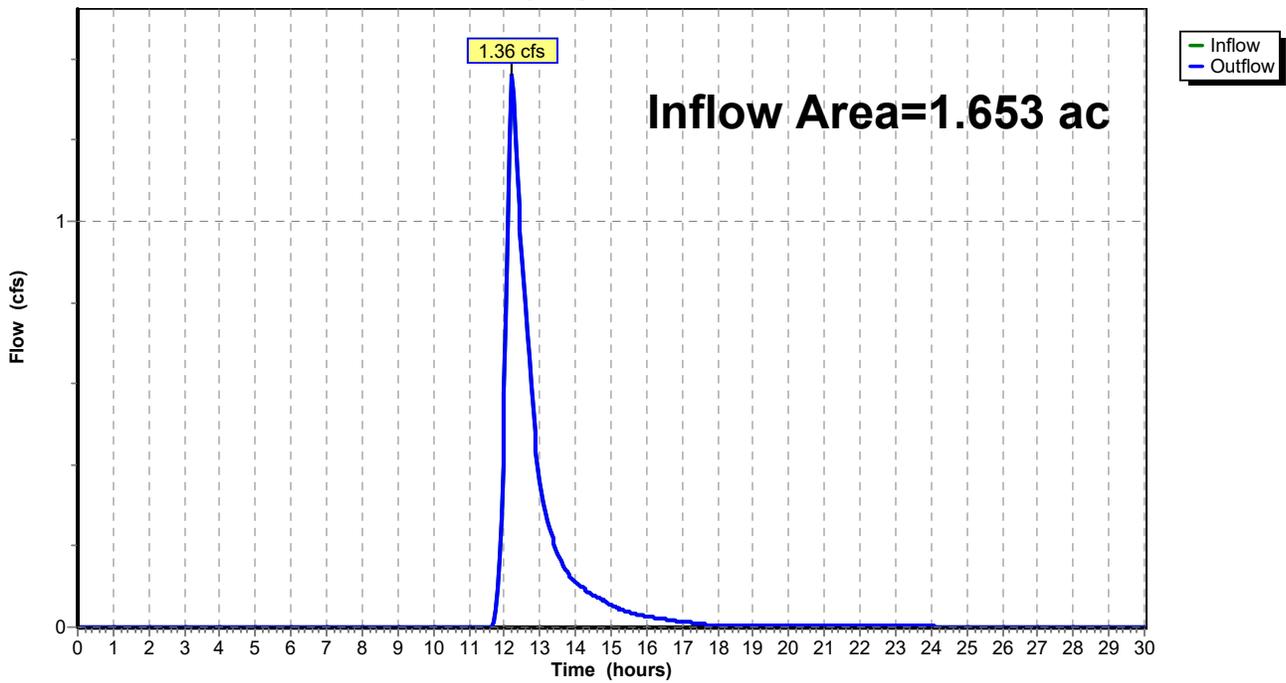
[40] Hint: Not Described (Outflow=Inflow)

Inflow Area = 1.653 ac, 39.84% Impervious, Inflow Depth = 0.76" for 10-Year event
Inflow = 1.36 cfs @ 12.22 hrs, Volume= 0.105 af
Outflow = 1.36 cfs @ 12.22 hrs, Volume= 0.105 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind method, Time Span= 0.00-30.00 hrs, dt= 0.05 hrs

Reach 2R: central DA

Hydrograph



Summary for Reach 3R: East DA

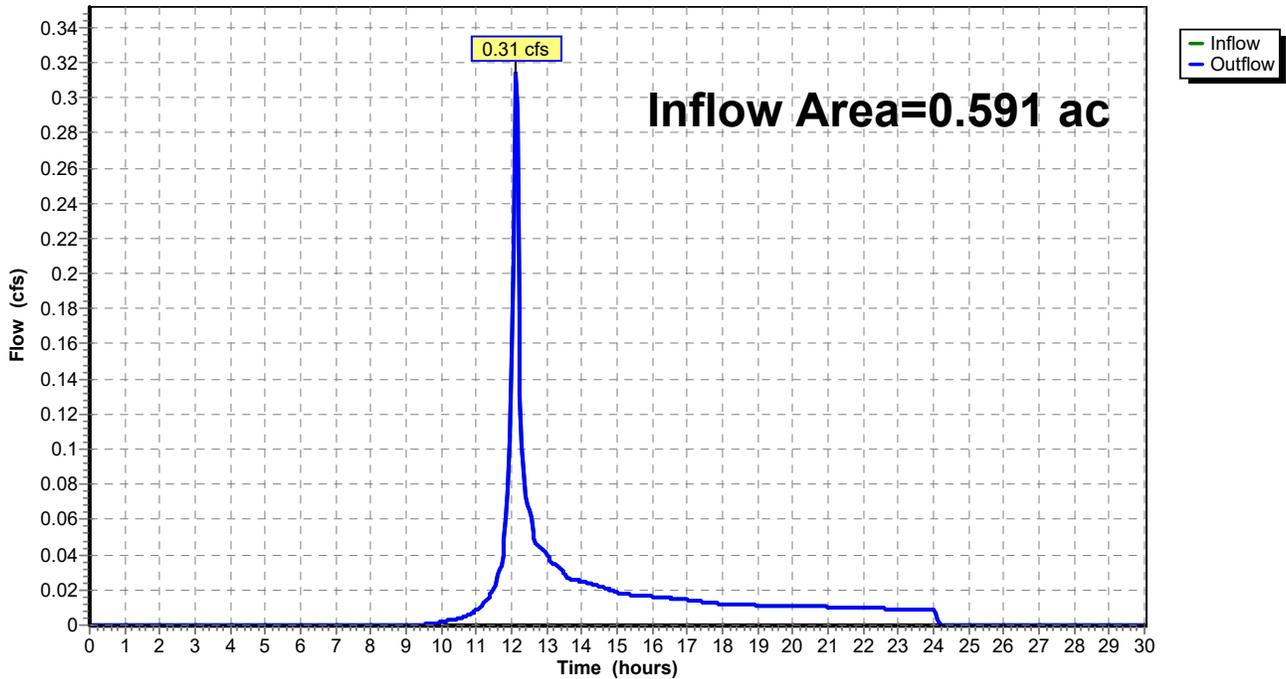
[40] Hint: Not Described (Outflow=Inflow)

Inflow Area = 0.591 ac, 17.77% Impervious, Inflow Depth = 0.51" for 10-Year event
Inflow = 0.31 cfs @ 12.12 hrs, Volume= 0.025 af
Outflow = 0.31 cfs @ 12.12 hrs, Volume= 0.025 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind method, Time Span= 0.00-30.00 hrs, dt= 0.05 hrs

Reach 3R: East DA

Hydrograph



Summary for Reach 4R: (new Reach)

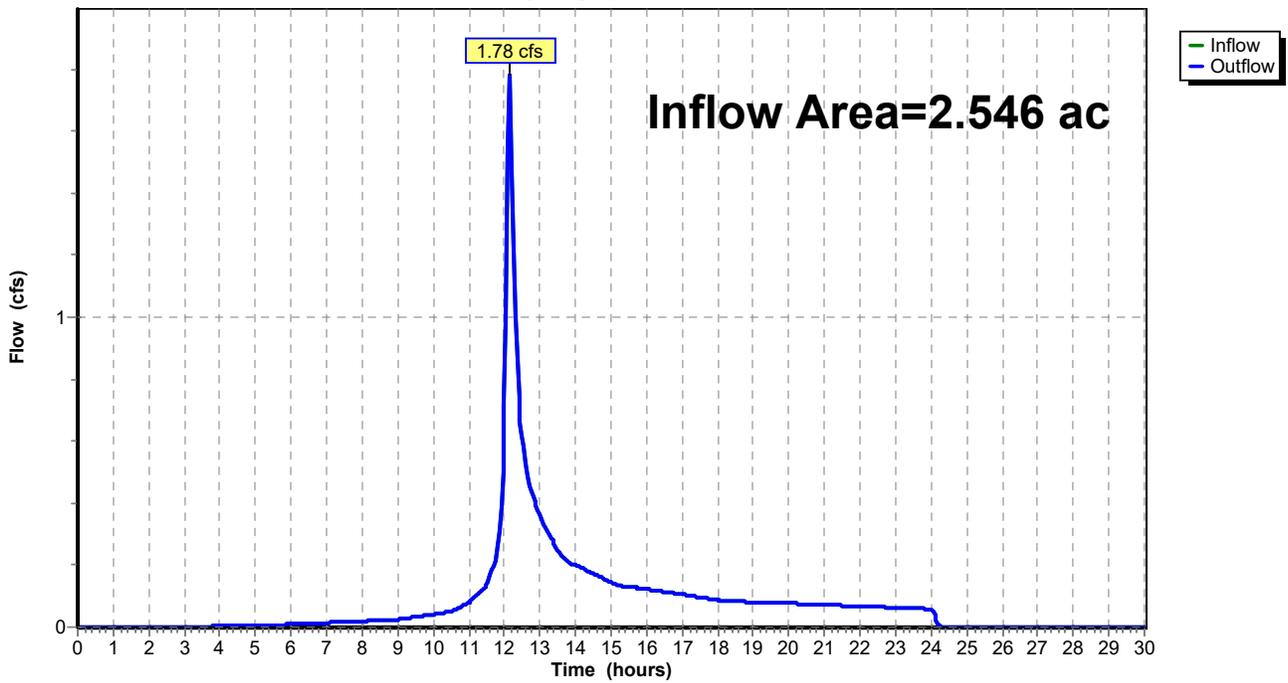
[40] Hint: Not Described (Outflow=Inflow)

Inflow Area = 2.546 ac, 19.18% Impervious, Inflow Depth = 0.91" for 10-Year event
Inflow = 1.78 cfs @ 12.15 hrs, Volume= 0.192 af
Outflow = 1.78 cfs @ 12.15 hrs, Volume= 0.192 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind method, Time Span= 0.00-30.00 hrs, dt= 0.05 hrs

Reach 4R: (new Reach)

Hydrograph



Summary for Pond 1P: UG - system #1

Inflow Area = 0.397 ac, 68.73% Impervious, Inflow Depth = 2.66" for 10-Year event
 Inflow = 1.32 cfs @ 12.12 hrs, Volume= 0.088 af
 Outflow = 0.48 cfs @ 12.27 hrs, Volume= 0.088 af, Atten= 64%, Lag= 9.3 min
 Discarded = 0.06 cfs @ 11.10 hrs, Volume= 0.058 af
 Primary = 0.42 cfs @ 12.27 hrs, Volume= 0.030 af

Routing by Stor-Ind method, Time Span= 0.00-30.00 hrs, dt= 0.05 hrs / 2
 Peak Elev= 305.81' @ 12.27 hrs Surf.Area= 0.027 ac Storage= 0.023 af

Plug-Flow detention time= 48.3 min calculated for 0.088 af (100% of inflow)
 Center-of-Mass det. time= 48.1 min (875.0 - 826.9)

Volume	Invert	Avail.Storage	Storage Description
#1A	304.50'	0.014 af	42.06'W x 27.46'L x 2.44'H Field A 0.065 af Overall - 0.030 af Embedded = 0.035 af x 40.0% Voids
#2A	305.00'	0.028 af	ACF R-Tank HD 1 x 290 Inside #1 Inside= 15.7"W x 17.3"H => 1.80 sf x 2.35'L = 4.2 cf Outside= 15.7"W x 17.3"H => 1.89 sf x 2.35'L = 4.4 cf 290 Chambers in 29 Rows
		0.042 af	Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices
#1	Primary	305.20'	5.0" Vert. Orifice/Grate C= 0.600
#2	Primary	306.40'	8.0" Horiz. Orifice/Grate C= 0.600 Limited to weir flow at low heads
#3	Discarded	304.50'	2.410 in/hr Exfiltration over Surface area Phase-In= 0.01'

Discarded OutFlow Max=0.06 cfs @ 11.10 hrs HW=304.53' (Free Discharge)
 ↳ **3=Exfiltration** (Exfiltration Controls 0.06 cfs)

Primary OutFlow Max=0.42 cfs @ 12.27 hrs HW=305.81' (Free Discharge)
 ↳ **1=Orifice/Grate** (Orifice Controls 0.42 cfs @ 3.05 fps)
 ↳ **2=Orifice/Grate** (Controls 0.00 cfs)

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Pond 1P: UG - system #1 - Chamber Wizard Field A

Chamber Model = ACF R-Tank HD 1 (ACF Environmental R-Tank HD)

Inside= 15.7"W x 17.3"H => 1.80 sf x 2.35'L = 4.2 cf

Outside= 15.7"W x 17.3"H => 1.89 sf x 2.35'L = 4.4 cf

10 Chambers/Row x 2.35' Long = 23.46' Row Length +24.0" End Stone x 2 = 27.46' Base Length

29 Rows x 15.7" Wide + 24.0" Side Stone x 2 = 42.06' Base Width

6.0" Base + 17.3" Chamber Height + 6.0" Cover = 2.44' Field Height

290 Chambers x 4.2 cf = 1,224.3 cf Chamber Storage

290 Chambers x 4.4 cf = 1,288.8 cf Displacement

2,821.9 cf Field - 1,288.8 cf Chambers = 1,533.1 cf Stone x 40.0% Voids = 613.3 cf Stone Storage

Chamber Storage + Stone Storage = 1,837.6 cf = 0.042 af

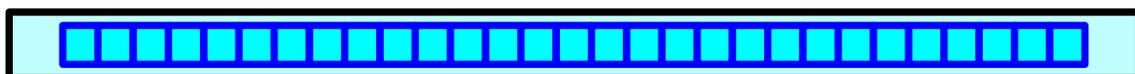
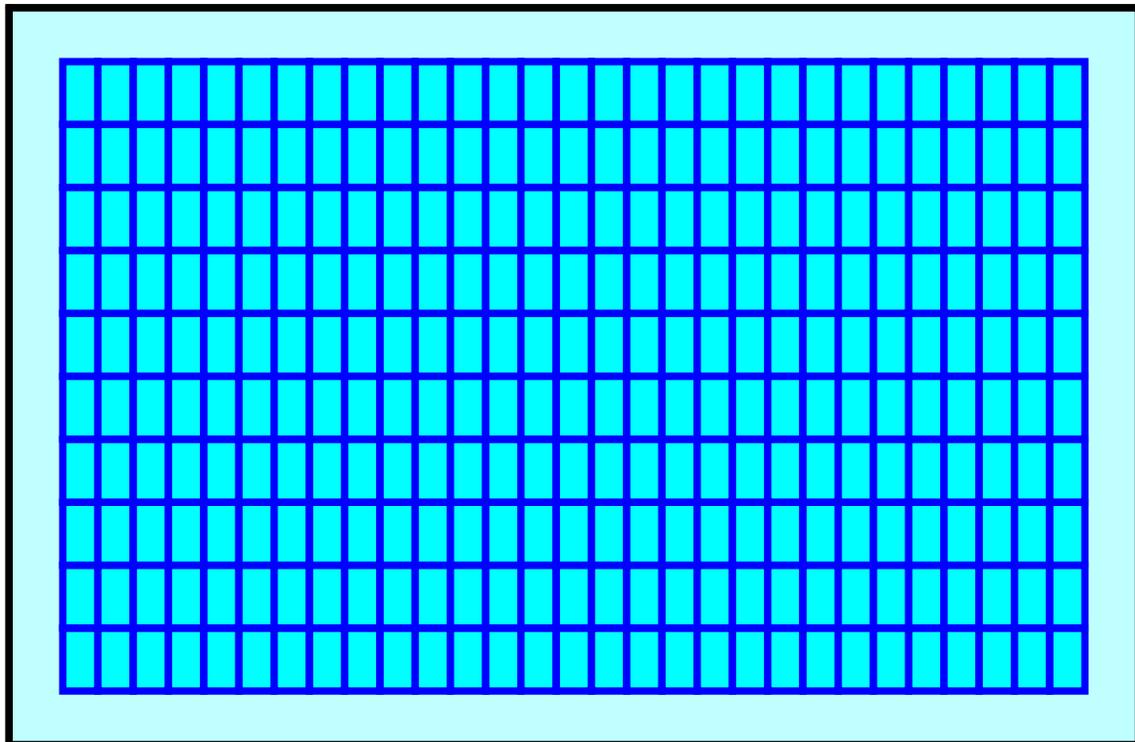
Overall Storage Efficiency = 65.1%

Overall System Size = 27.46' x 42.06' x 2.44'

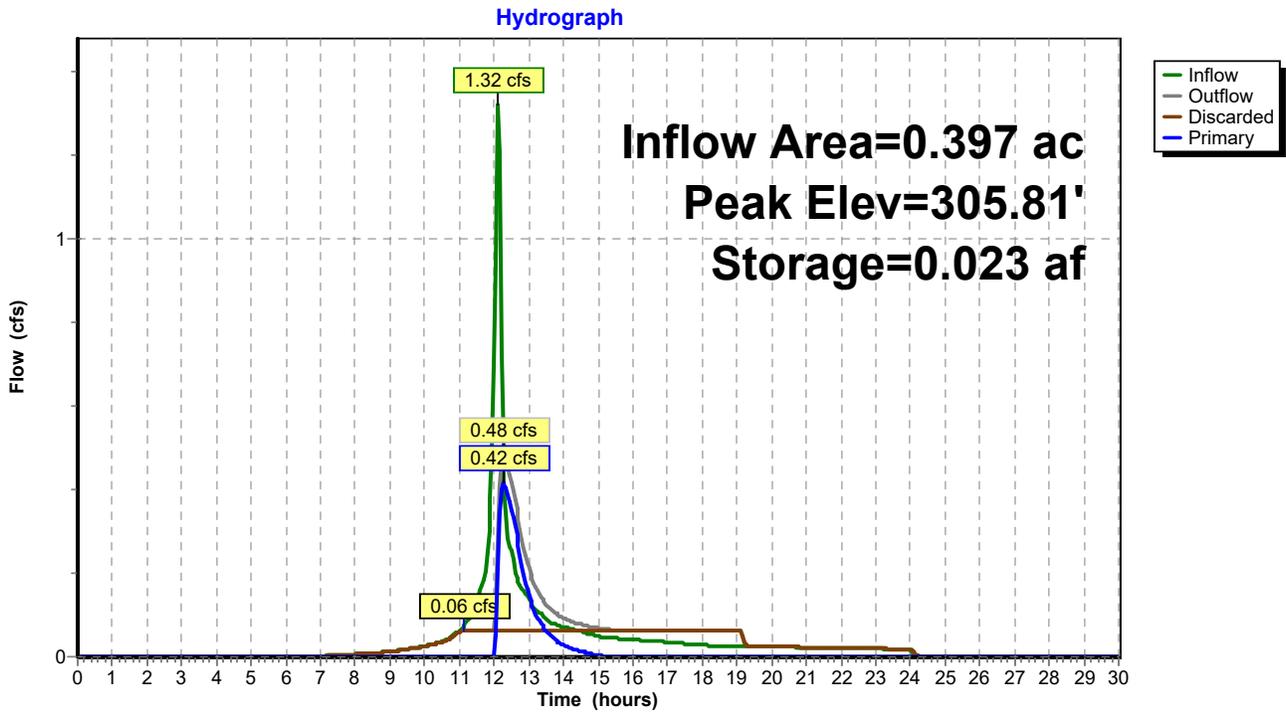
290 Chambers

104.5 cy Field

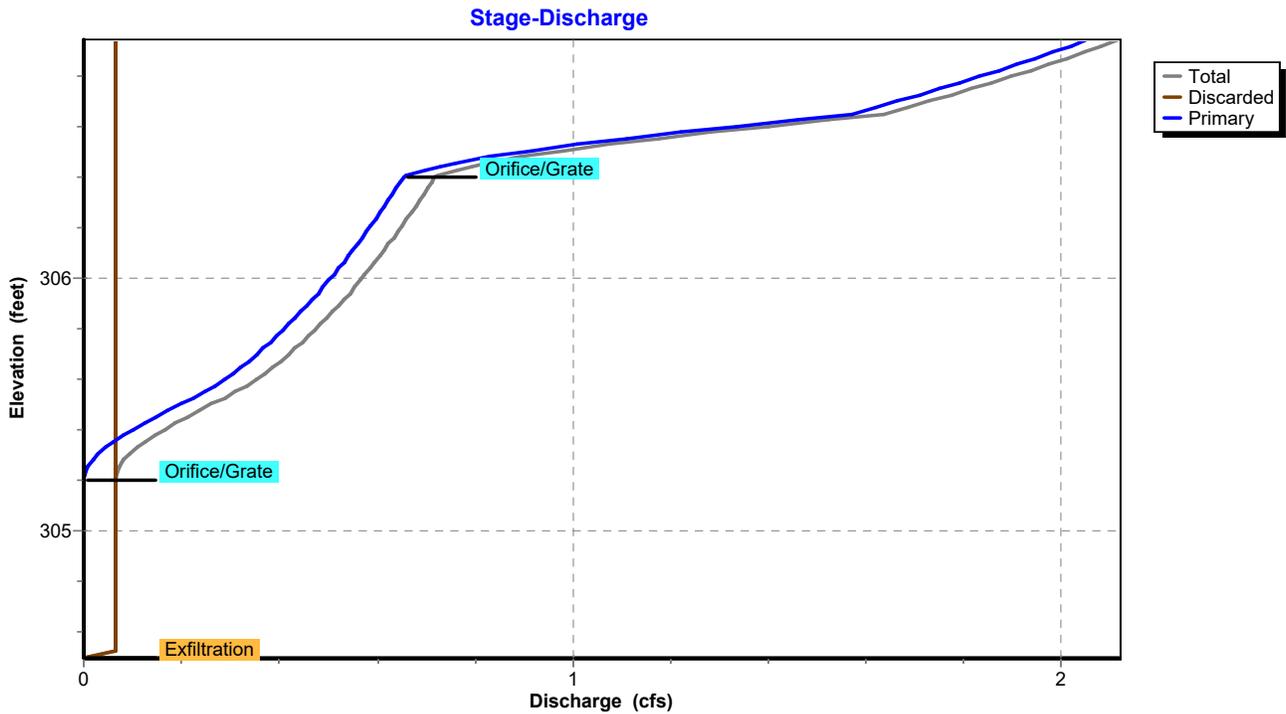
56.8 cy Stone



Pond 1P: UG - system #1



Pond 1P: UG - system #1



Summary for Pond 2P: UG - system #2

Inflow Area = 1.434 ac, 43.88% Impervious, Inflow Depth = 1.83" for 10-Year event
 Inflow = 2.67 cfs @ 12.11 hrs, Volume= 0.219 af
 Outflow = 1.42 cfs @ 12.22 hrs, Volume= 0.219 af, Atten= 47%, Lag= 6.2 min
 Discarded = 0.08 cfs @ 9.55 hrs, Volume= 0.120 af
 Primary = 1.33 cfs @ 12.22 hrs, Volume= 0.098 af

Routing by Stor-Ind method, Time Span= 0.00-30.00 hrs, dt= 0.05 hrs / 3
 Peak Elev= 294.72' @ 12.22 hrs Surf.Area= 0.034 ac Storage= 0.048 af

Plug-Flow detention time= 55.4 min calculated for 0.218 af (100% of inflow)
 Center-of-Mass det. time= 55.3 min (847.6 - 792.2)

Volume	Invert	Avail.Storage	Storage Description
#1A	292.80'	0.020 af	43.37'W x 34.50'L x 3.17'H Field A 0.109 af Overall - 0.060 af Embedded = 0.049 af x 40.0% Voids
#2A	293.30'	0.057 af	ACF R-Tank HD 1.5 x 390 Inside #1 Inside= 15.7"W x 26.0"H => 2.70 sf x 2.35'L = 6.3 cf Outside= 15.7"W x 26.0"H => 2.84 sf x 2.35'L = 6.7 cf 390 Chambers in 30 Rows
		0.076 af	Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices
#1	Primary	293.60'	7.0" Vert. Orifice/Grate C= 0.600
#2	Primary	294.50'	8.0" Vert. Orifice/Grate C= 0.600
#3	Primary	295.80'	12.0" Horiz. Orifice/Grate C= 0.600 Limited to weir flow at low heads
#4	Discarded	292.80'	2.410 in/hr Exfiltration over Surface area Phase-In= 0.01'

Discarded OutFlow Max=0.08 cfs @ 9.55 hrs HW=292.83' (Free Discharge)
 ↳4=Exfiltration (Exfiltration Controls 0.08 cfs)

Primary OutFlow Max=1.31 cfs @ 12.22 hrs HW=294.71' (Free Discharge)
 ↳1=Orifice/Grate (Orifice Controls 1.16 cfs @ 4.35 fps)
 ↳2=Orifice/Grate (Orifice Controls 0.15 cfs @ 1.56 fps)
 ↳3=Orifice/Grate (Controls 0.00 cfs)

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Pond 2P: UG - system #2 - Chamber Wizard Field A

Chamber Model = ACF R-Tank HD 1.5 (ACF Environmental R-Tank HD)

Inside= 15.7"W x 26.0"H => 2.70 sf x 2.35'L = 6.3 cf

Outside= 15.7"W x 26.0"H => 2.84 sf x 2.35'L = 6.7 cf

13 Chambers/Row x 2.35' Long = 30.50' Row Length +24.0" End Stone x 2 = 34.50' Base Length

30 Rows x 15.7" Wide + 24.0" Side Stone x 2 = 43.37' Base Width

6.0" Base + 26.0" Chamber Height + 6.0" Cover = 3.17' Field Height

390 Chambers x 6.3 cf = 2,469.8 cf Chamber Storage

390 Chambers x 6.7 cf = 2,599.7 cf Displacement

4,735.6 cf Field - 2,599.7 cf Chambers = 2,135.8 cf Stone x 40.0% Voids = 854.3 cf Stone Storage

Chamber Storage + Stone Storage = 3,324.1 cf = 0.076 af

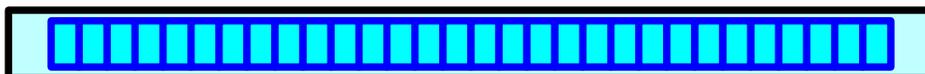
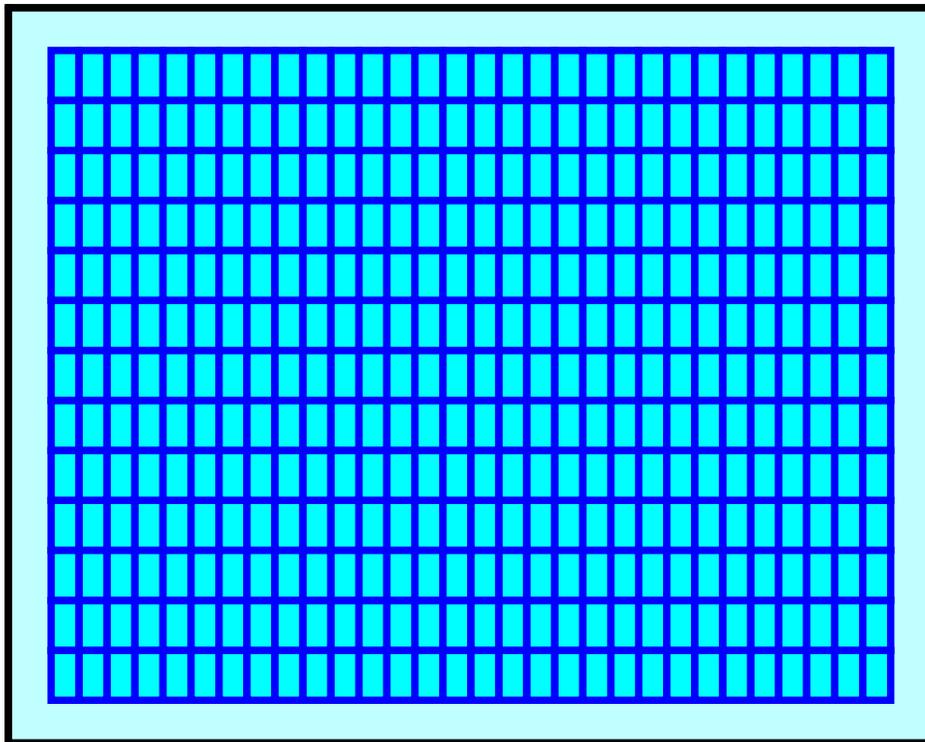
Overall Storage Efficiency = 70.2%

Overall System Size = 34.50' x 43.37' x 3.17'

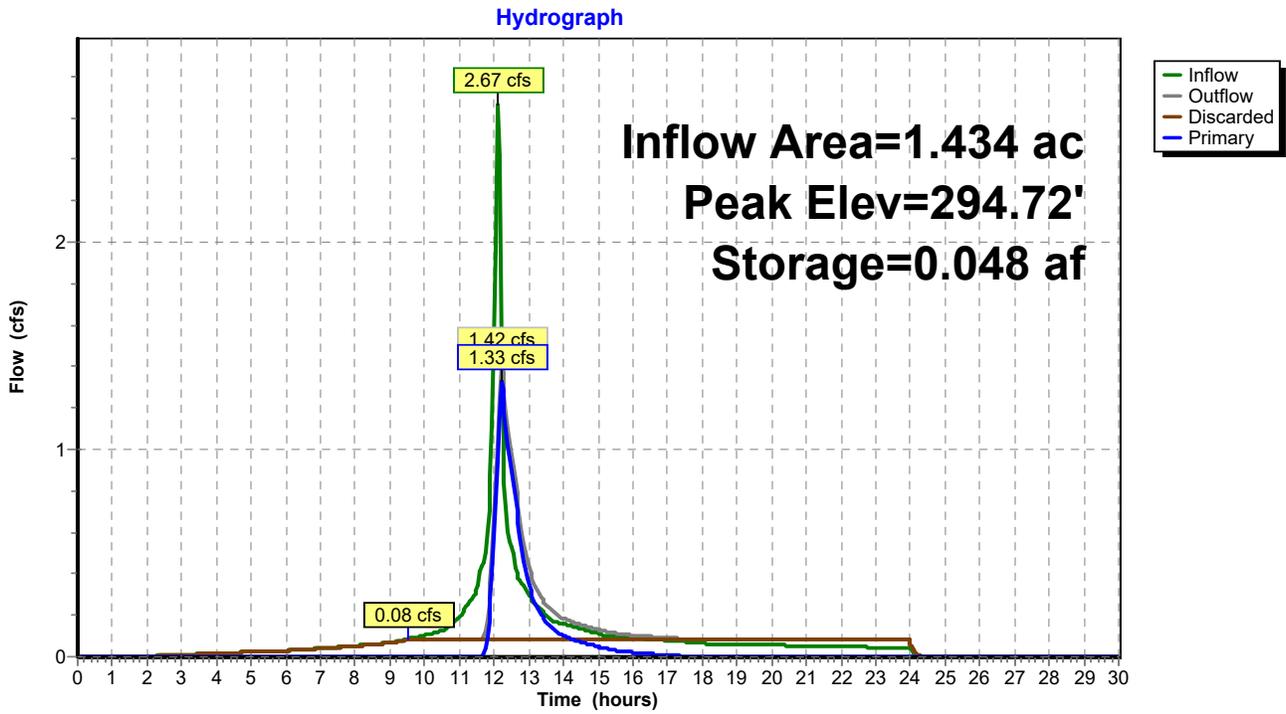
390 Chambers

175.4 cy Field

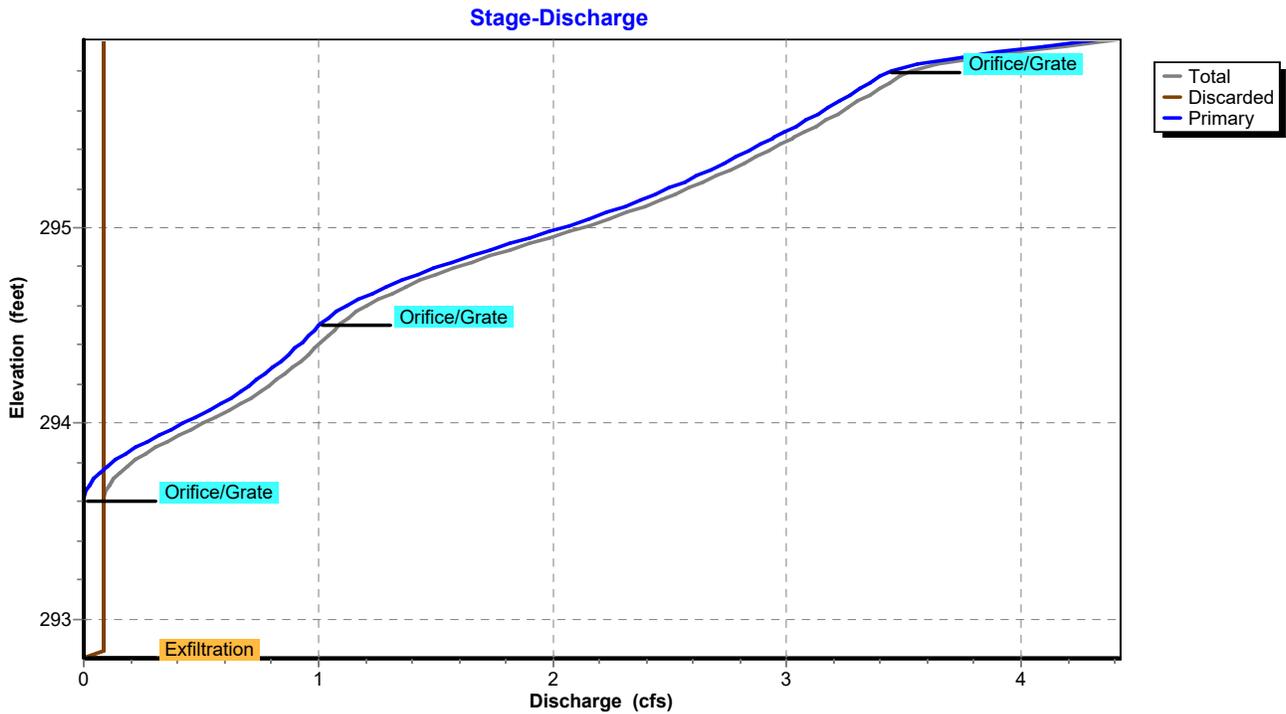
79.1 cy Stone



Pond 2P: UG - system #2



Pond 2P: UG - system #2

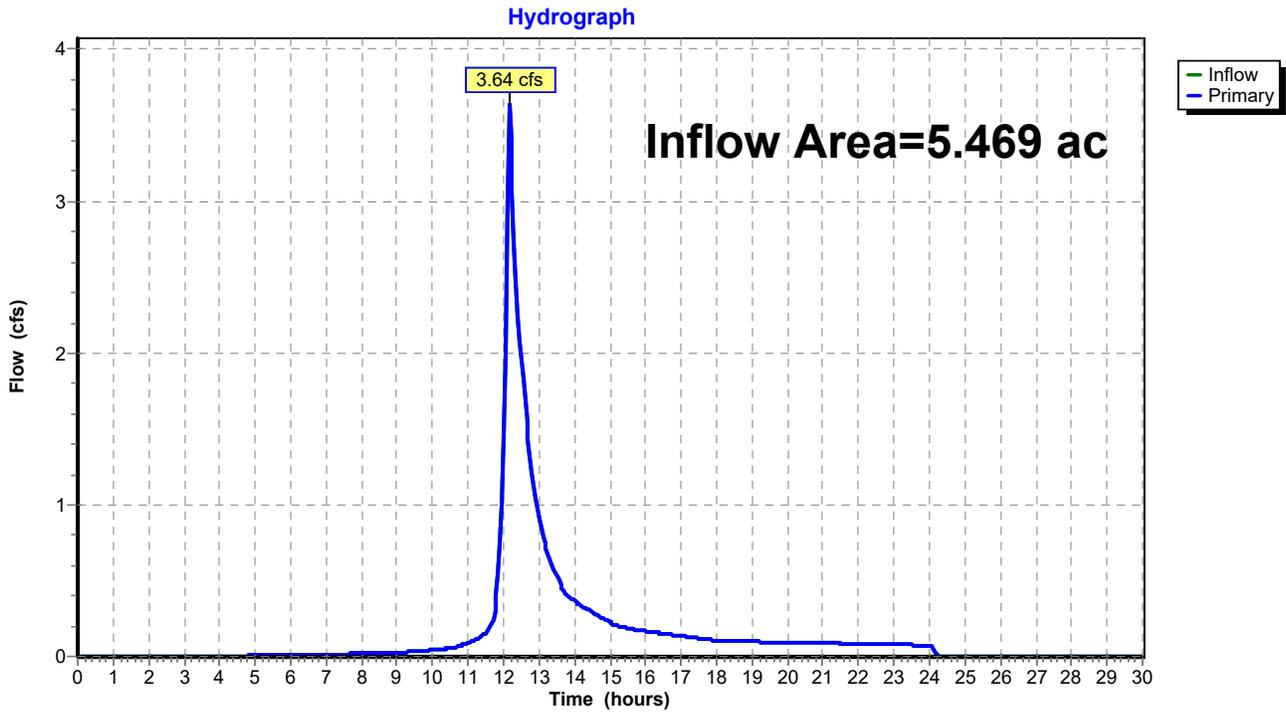


Summary for Link 1L: STUDY POINT- Amethyst Brook

Inflow Area = 5.469 ac, 28.03% Impervious, Inflow Depth = 0.78" for 10-Year event
Inflow = 3.64 cfs @ 12.16 hrs, Volume= 0.355 af
Primary = 3.64 cfs @ 12.16 hrs, Volume= 0.355 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-30.00 hrs, dt= 0.05 hrs

Link 1L: STUDY POINT- Amethyst Brook



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Summary for Subcatchment P1: South of Amherst Road

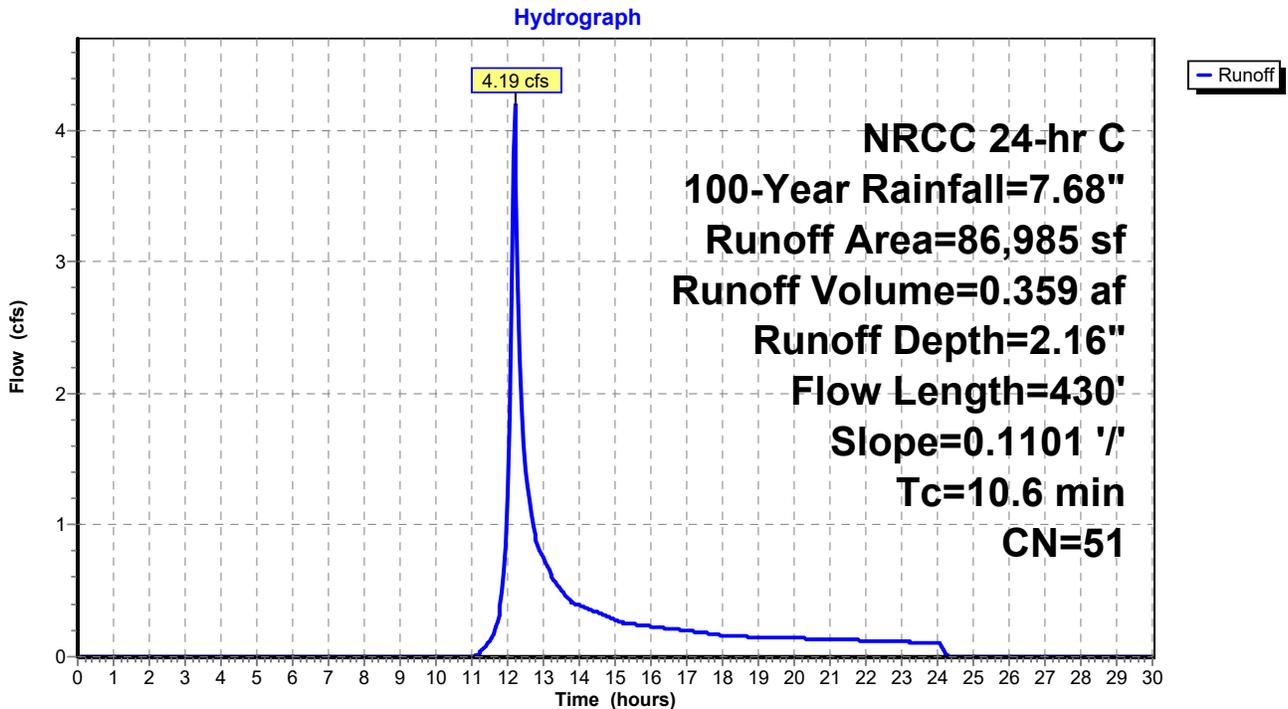
Runoff = 4.19 cfs @ 12.19 hrs, Volume= 0.359 af, Depth= 2.16"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-30.00 hrs, dt= 0.05 hrs
NRCC 24-hr C 100-Year Rainfall=7.68"

	Area (sf)	CN	Description
*	7,024	98	Impervious HSG A
*	806	98	Impervious HSG B
	39,100	36	Woods, Fair, HSG A
	30,655	60	Woods, Fair, HSG B
	9,400	49	50-75% Grass cover, Fair, HSG A
	86,985	51	Weighted Average
	79,155		91.00% Pervious Area
	7,830		9.00% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
10.6	430	0.1101	0.68		Lag/CN Method, Contour Length= 9,580' Interval= 1'

Subcatchment P1: South of Amherst Road



Summary for Subcatchment P1A: Amherst rd

[49] Hint: $T_c < 2dt$ may require smaller dt

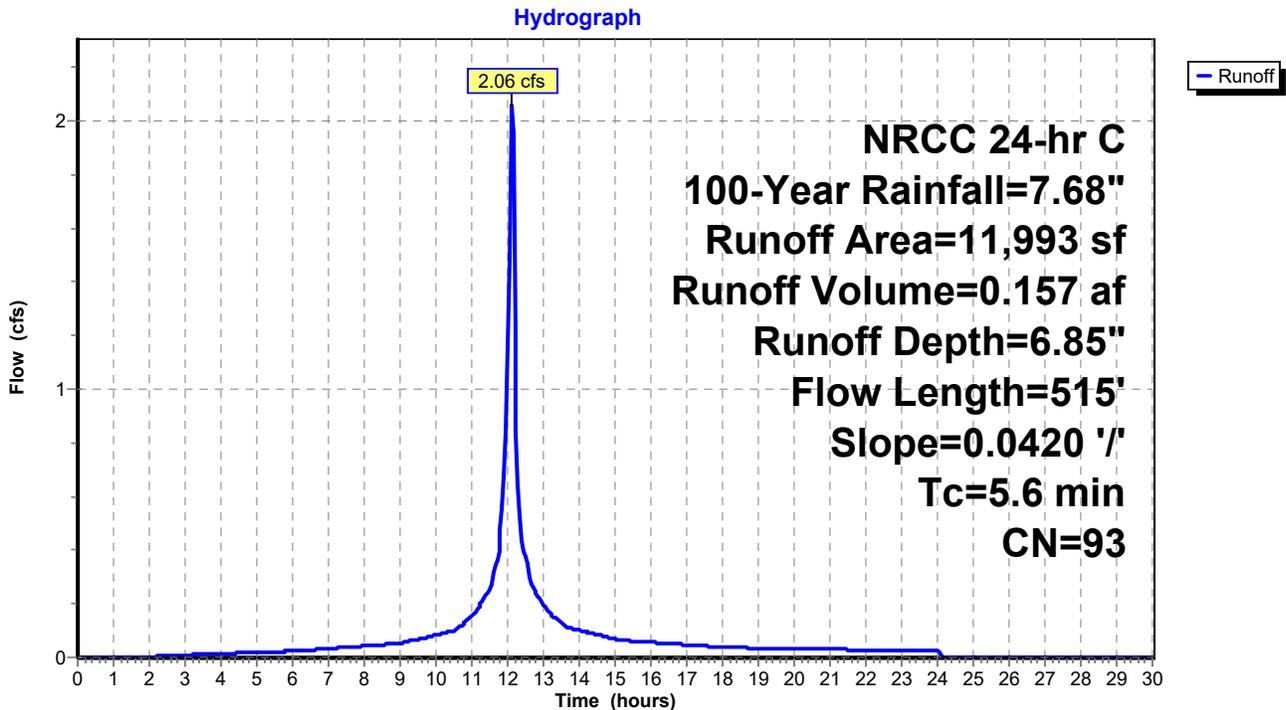
Runoff = 2.06 cfs @ 12.12 hrs, Volume= 0.157 af, Depth= 6.85"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-30.00 hrs, dt= 0.05 hrs
NRCC 24-hr C 100-Year Rainfall=7.68"

	Area (sf)	CN	Description
*	10,800	98	Paved road, HSG A
	1,193	49	50-75% Grass cover, Fair, HSG A
	11,993	93	Weighted Average
	1,193		9.95% Pervious Area
	10,800		90.05% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
5.6	515	0.0420	1.53		Lag/CN Method, Contour Length= 504' Interval= 1'

Subcatchment P1A: Amherst rd



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NRCC 24-hr C 100-Year Rainfall=7.68"

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Summary for Subcatchment P2A: Part of #20 and 24 impervious

[49] Hint: Tc<2dt may require smaller dt

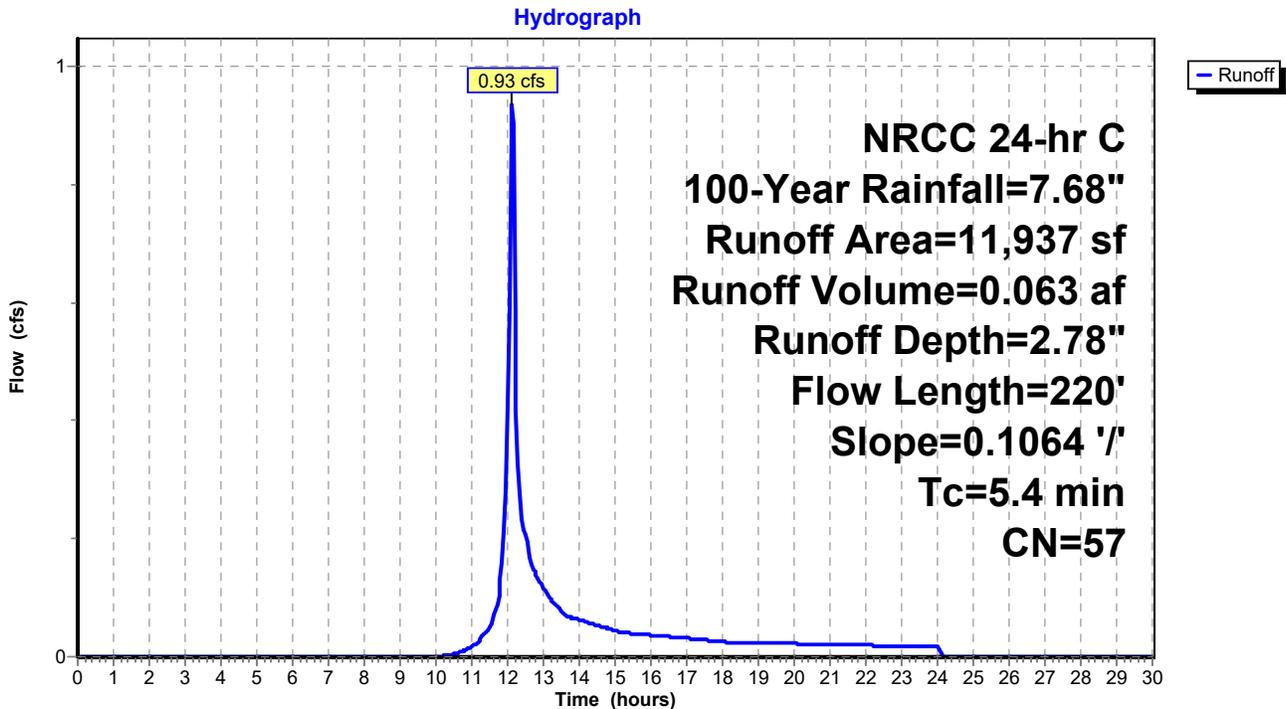
Runoff = 0.93 cfs @ 12.13 hrs, Volume= 0.063 af, Depth= 2.78"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-30.00 hrs, dt= 0.05 hrs
NRCC 24-hr C 100-Year Rainfall=7.68"

	Area (sf)	CN	Description
*	2,647	98	Impervious HSG A
	7,000	49	50-75% Grass cover, Fair, HSG A
	2,290	36	Woods, Fair, HSG A
	11,937	57	Weighted Average
	9,290		77.83% Pervious Area
	2,647		22.17% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
5.4	220	0.1064	0.68		Lag/CN Method, Contour Length= 1,270' Interval= 1'

Subcatchment P2A: Part of #20 and 24 impervious



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Summary for Subcatchment P2B: slope below driveway

[49] Hint: $T_c < 2dt$ may require smaller dt

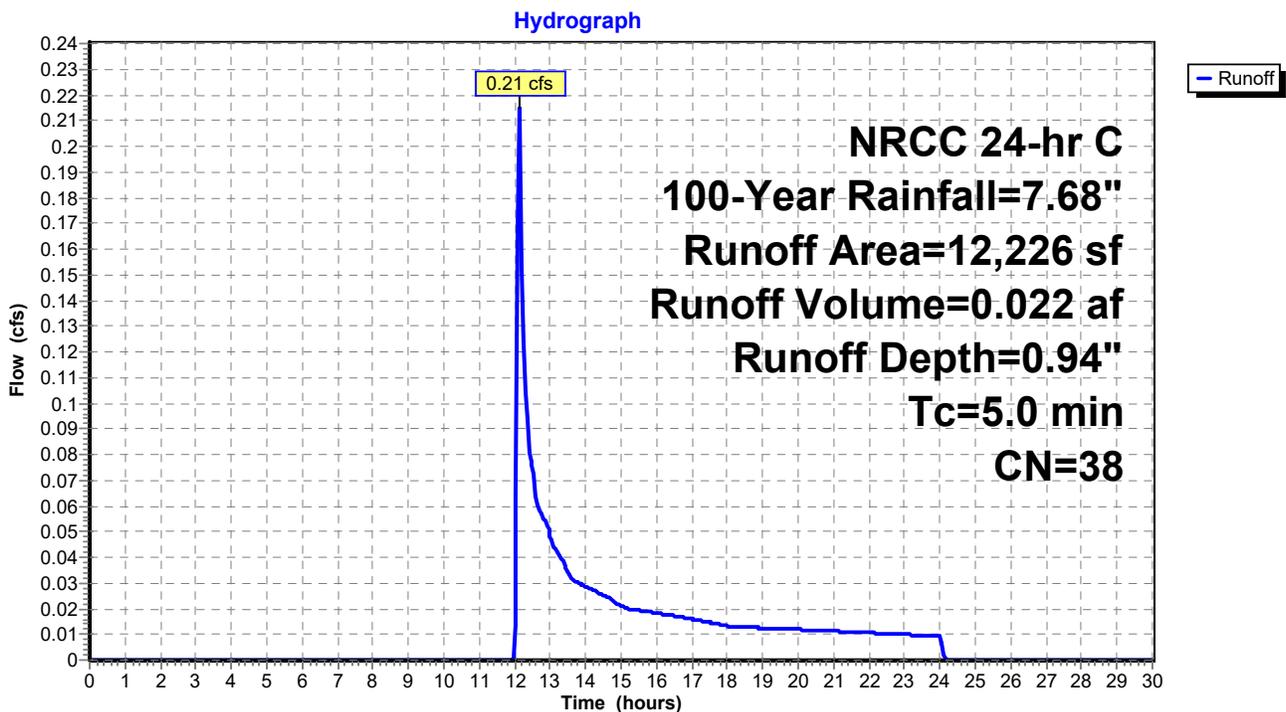
Runoff = 0.21 cfs @ 12.15 hrs, Volume= 0.022 af, Depth= 0.94"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-30.00 hrs, dt= 0.05 hrs
NRCC 24-hr C 100-Year Rainfall=7.68"

Area (sf)	CN	Description
11,888	36	Woods, Fair, HSG A
* 338	98	Wall
12,226	38	Weighted Average
11,888		97.24% Pervious Area
338		2.76% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
5.0					Direct Entry,

Subcatchment P2B: slope below driveway



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NRCC 24-hr C 100-Year Rainfall=7.68"

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Summary for Subcatchment P2C: Entrance drive

[49] Hint: $T_c < 2dt$ may require smaller dt

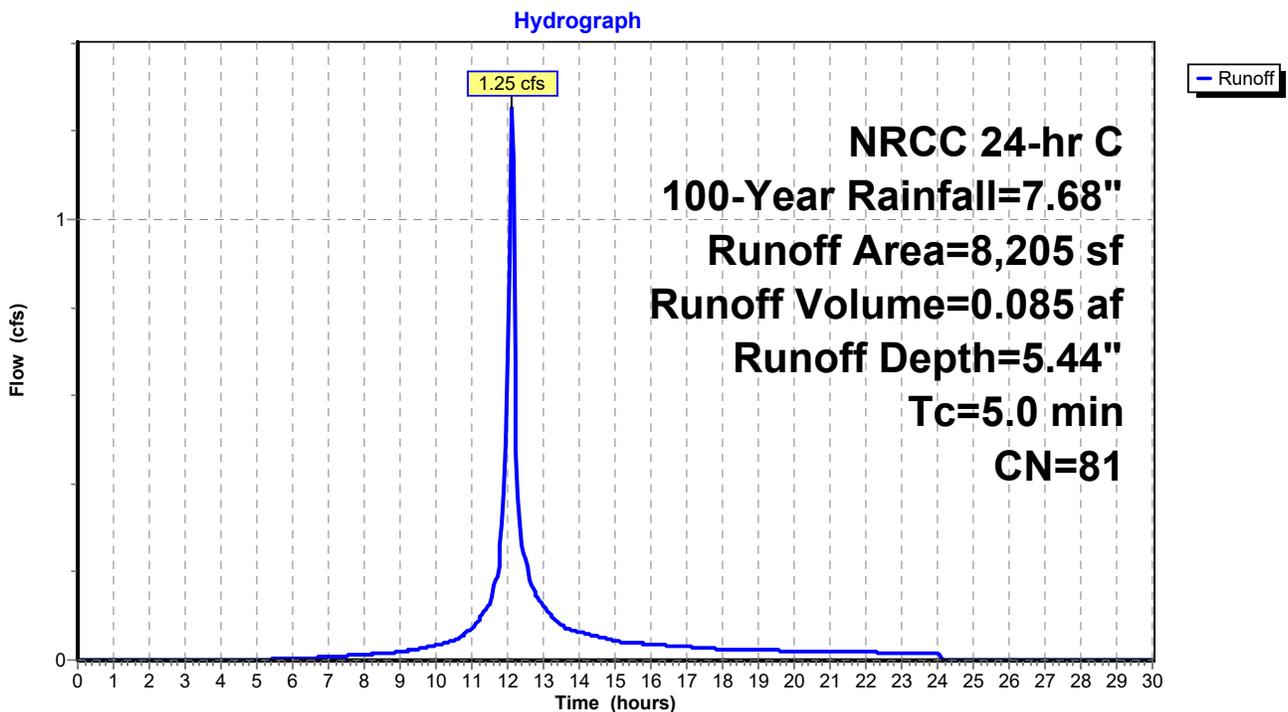
Runoff = 1.25 cfs @ 12.11 hrs, Volume= 0.085 af, Depth= 5.44"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-30.00 hrs, dt= 0.05 hrs
NRCC 24-hr C 100-Year Rainfall=7.68"

	Area (sf)	CN	Description
*	5,389	98	Impervious
	2,816	49	50-75% Grass cover, Fair, HSG A
	8,205	81	Weighted Average
	2,816		34.32% Pervious Area
	5,389		65.68% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
5.0					Direct Entry,

Subcatchment P2C: Entrance drive



Summary for Subcatchment P2D: Parking lot and Roof

[49] Hint: Tc<2dt may require smaller dt

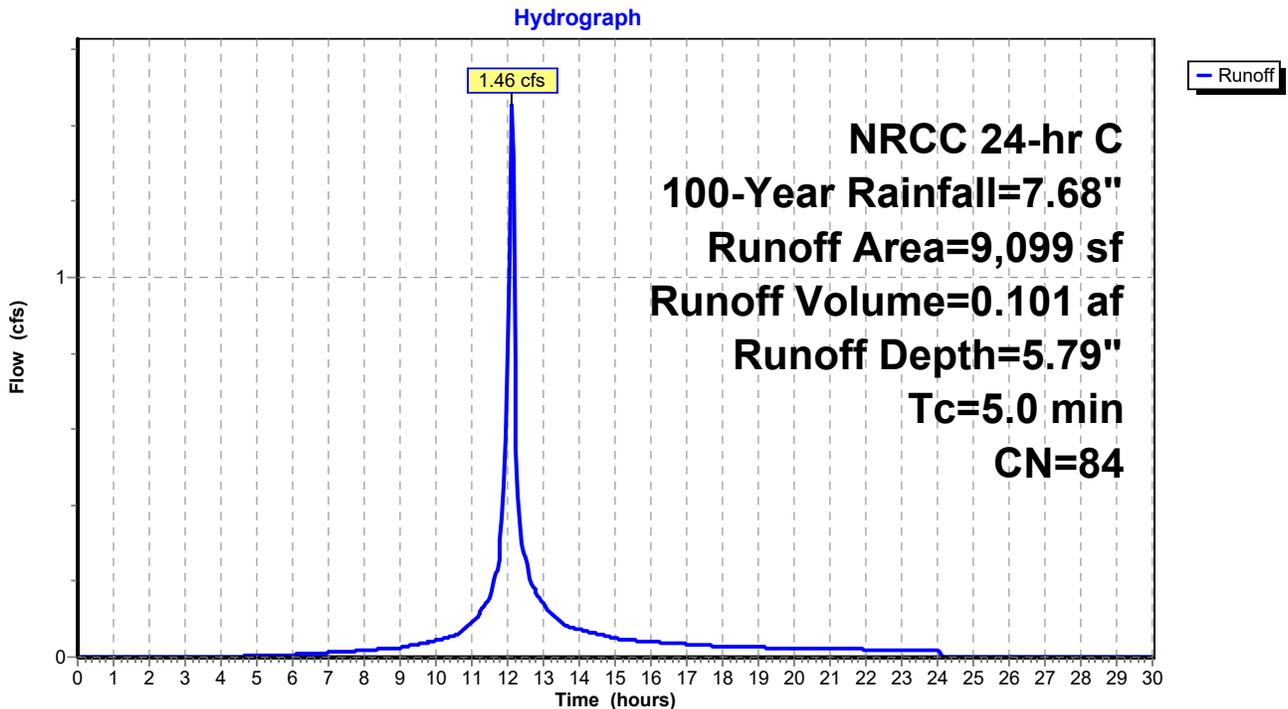
Runoff = 1.46 cfs @ 12.11 hrs, Volume= 0.101 af, Depth= 5.79"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-30.00 hrs, dt= 0.05 hrs
 NRCC 24-hr C 100-Year Rainfall=7.68"

	Area (sf)	CN	Description
*	6,504	98	Impervious
	2,595	49	50-75% Grass cover, Fair, HSG A
	9,099	84	Weighted Average
	2,595		28.52% Pervious Area
	6,504		71.48% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
5.0					Direct Entry,

Subcatchment P2D: Parking lot and Roof



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Summary for Subcatchment P2E: Driveway and back roof

[49] Hint: Tc<2dt may require smaller dt

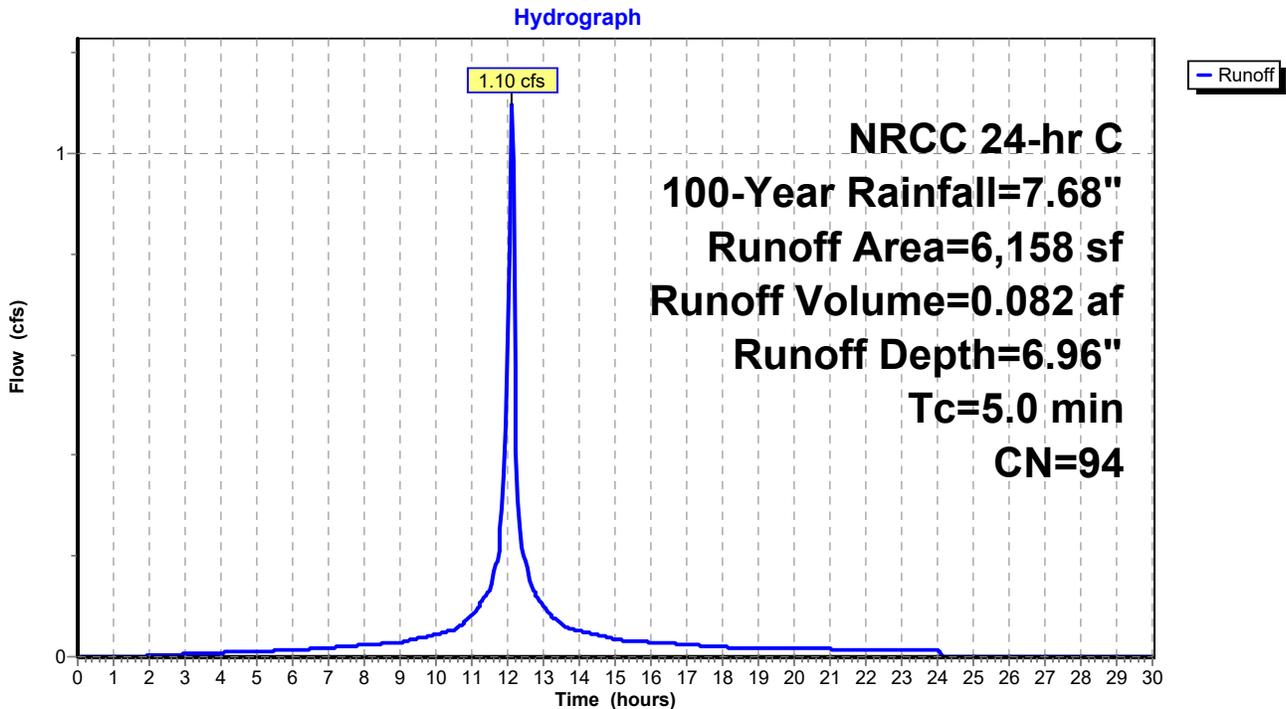
Runoff = 1.10 cfs @ 12.11 hrs, Volume= 0.082 af, Depth= 6.96"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-30.00 hrs, dt= 0.05 hrs
NRCC 24-hr C 100-Year Rainfall=7.68"

	Area (sf)	CN	Description
*	4,254	98	Impervious
	653	96	Gravel surface, HSG A
	451	49	50-75% Grass cover, Fair, HSG A
*	800	98	Impervious - roof
	6,158	94	Weighted Average
	1,104		17.93% Pervious Area
	5,054		82.07% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
5.0					Direct Entry,

Subcatchment P2E: Driveway and back roof



Summary for Subcatchment P3: part of #24 impervious + wooded slope

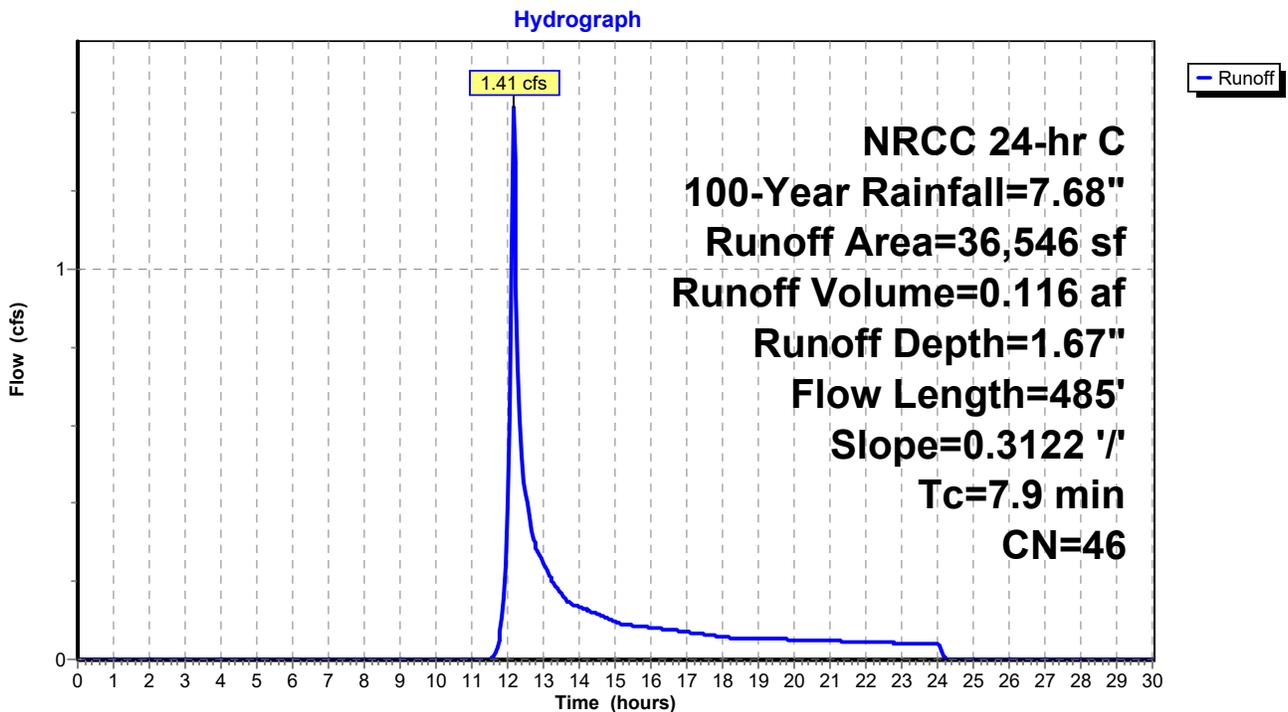
Runoff = 1.41 cfs @ 12.16 hrs, Volume= 0.116 af, Depth= 1.67"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-30.00 hrs, dt= 0.05 hrs
NRCC 24-hr C 100-Year Rainfall=7.68"

Area (sf)	CN	Description
4,706	98	Impervious
26,390	36	Woods, Fair, HSG A
5,000	49	50-75% Grass cover, Fair, HSG A
450	49	50-75% Grass cover, Fair, HSG A
36,546	46	Weighted Average
31,840		87.12% Pervious Area
4,706		12.88% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
7.9	485	0.3122	1.03		Lag/CN Method, Contour Length= 11,408' Interval= 1'

Subcatchment P3: part of #24 impervious + wooded slope



Summary for Subcatchment P3A: #22 drive and lower parking lots

[49] Hint: Tc<2dt may require smaller dt

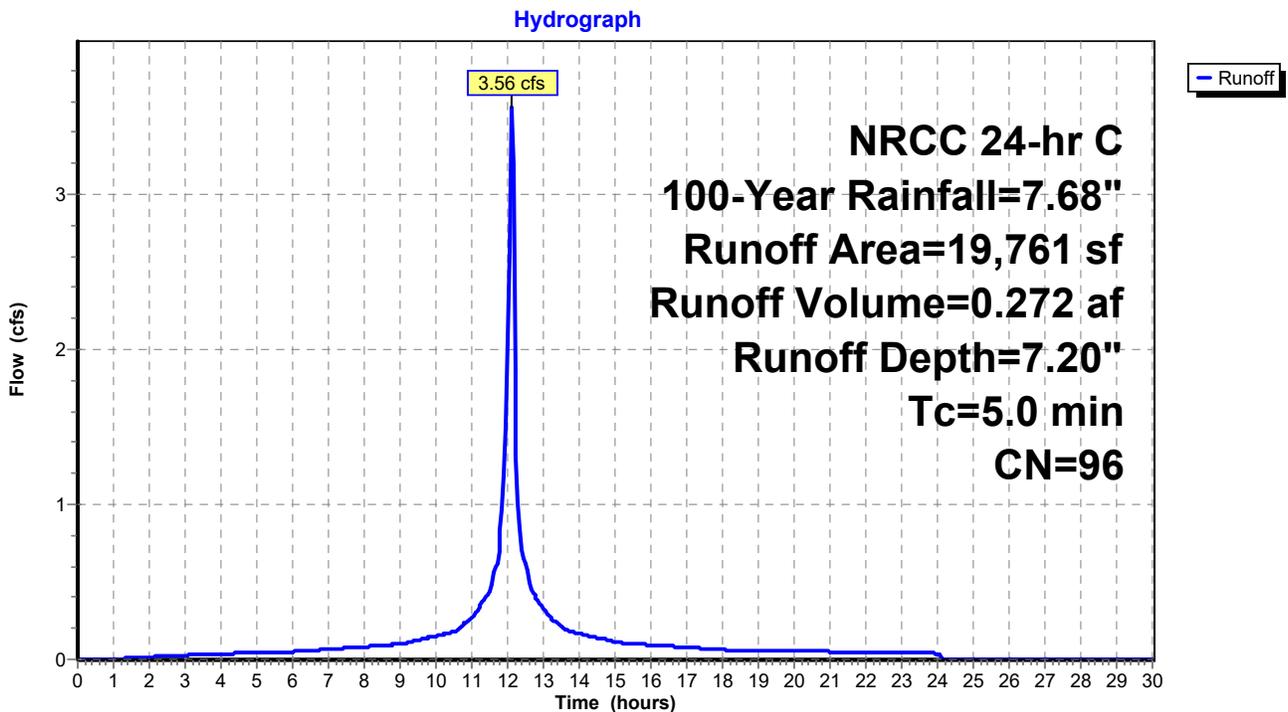
Runoff = 3.56 cfs @ 12.11 hrs, Volume= 0.272 af, Depth= 7.20"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-30.00 hrs, dt= 0.05 hrs
NRCC 24-hr C 100-Year Rainfall=7.68"

	Area (sf)	CN	Description
*	17,647	98	Impervious
	1,300	96	Gravel surface, HSG A
	814	49	50-75% Grass cover, Fair, HSG A
	19,761	96	Weighted Average
	2,114		10.70% Pervious Area
	17,647		89.30% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
5.0					Direct Entry,

Subcatchment P3A: #22 drive and lower parking lots



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NRCC 24-hr C 100-Year Rainfall=7.68"

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Summary for Subcatchment P3B: slope below parking

[49] Hint: $T_c < 2dt$ may require smaller dt

Runoff = 0.44 cfs @ 12.13 hrs, Volume= 0.032 af, Depth= 1.76"

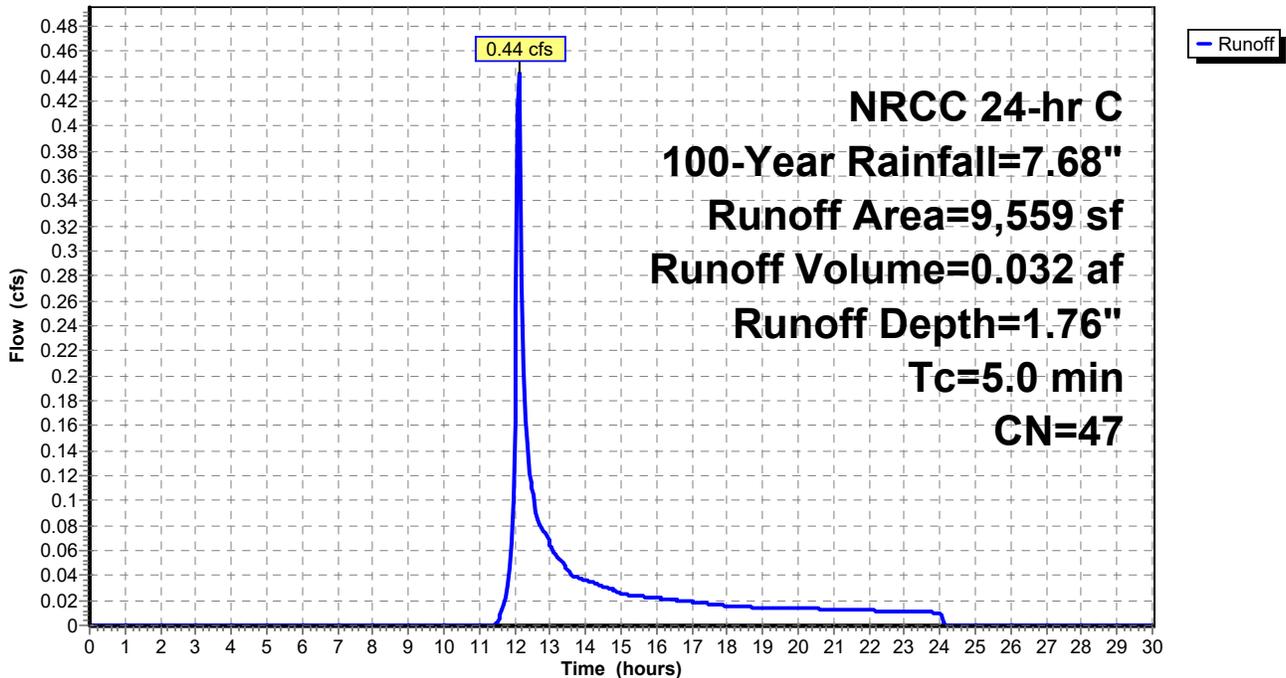
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-30.00 hrs, dt= 0.05 hrs
NRCC 24-hr C 100-Year Rainfall=7.68"

	Area (sf)	CN	Description
*	1,285	98	Impervious
	6,274	36	Woods, Fair, HSG A
	2,000	49	50-75% Grass cover, Fair, HSG A
	9,559	47	Weighted Average
	8,274		86.56% Pervious Area
	1,285		13.44% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
5.0					Direct Entry,

Subcatchment P3B: slope below parking

Hydrograph



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NRCC 24-hr C 100-Year Rainfall=7.68"

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Summary for Subcatchment P4: east drainage area

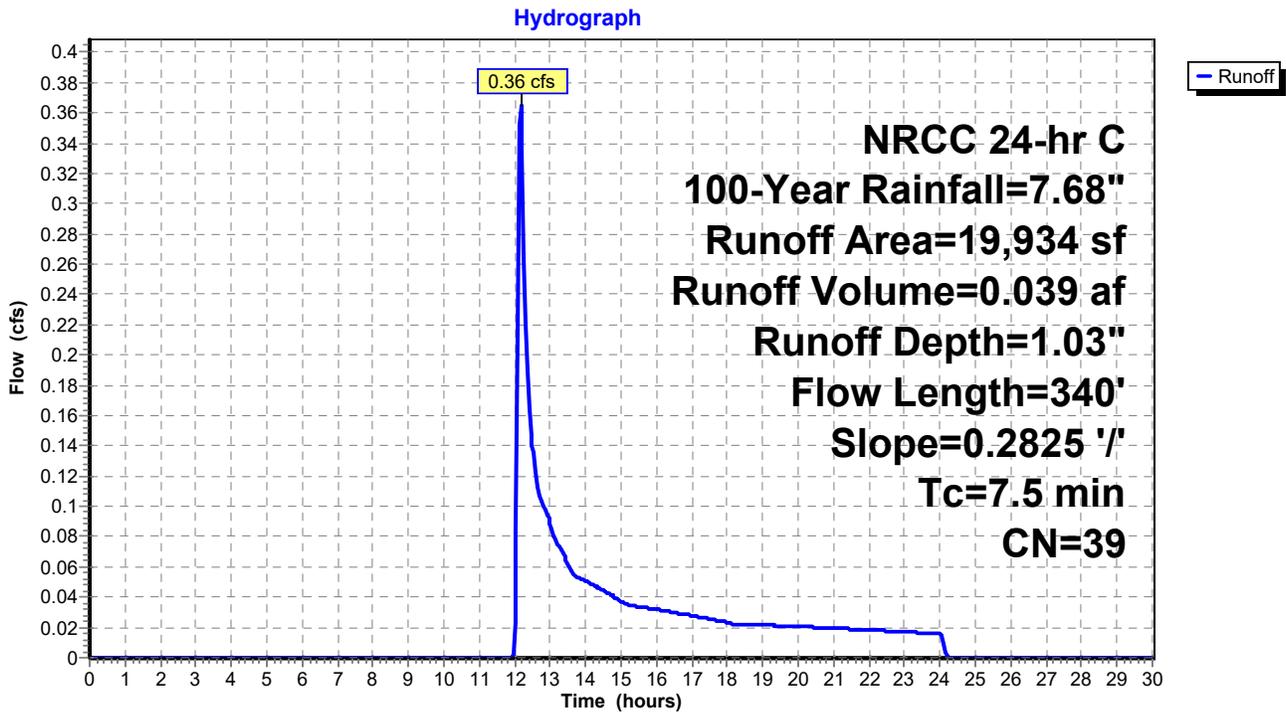
Runoff = 0.36 cfs @ 12.17 hrs, Volume= 0.039 af, Depth= 1.03"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-30.00 hrs, dt= 0.05 hrs
NRCC 24-hr C 100-Year Rainfall=7.68"

Area (sf)	CN	Description
18,814	36	Woods, Fair, HSG A
* 1,120	98	Impervious
19,934	39	Weighted Average
18,814		94.38% Pervious Area
1,120		5.62% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
7.5	340	0.2825	0.75		Lag/CN Method, Contour Length= 5,632' Interval= 1'

Subcatchment P4: east drainage area



Summary for Subcatchment P4A: part of #22 roof

[49] Hint: Tc<2dt may require smaller dt

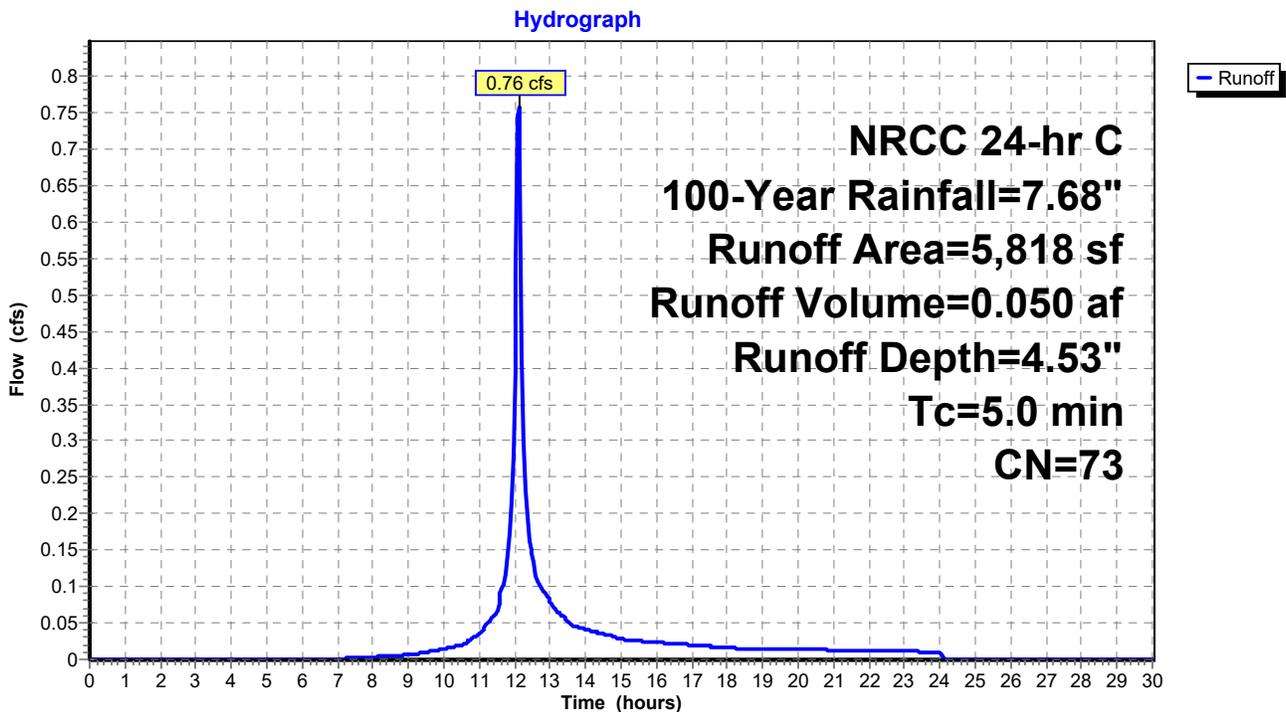
Runoff = 0.76 cfs @ 12.12 hrs, Volume= 0.050 af, Depth= 4.53"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-30.00 hrs, dt= 0.05 hrs
 NRCC 24-hr C 100-Year Rainfall=7.68"

Area (sf)	CN	Description
3,455	98	Unconnected roofs, HSG A
2,363	36	Woods, Fair, HSG A
5,818	73	Weighted Average
2,363		40.62% Pervious Area
3,455		59.38% Impervious Area
3,455		100.00% Unconnected

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
5.0					Direct Entry,

Subcatchment P4A: part of #22 roof



Summary for Reach 1R: ex swale

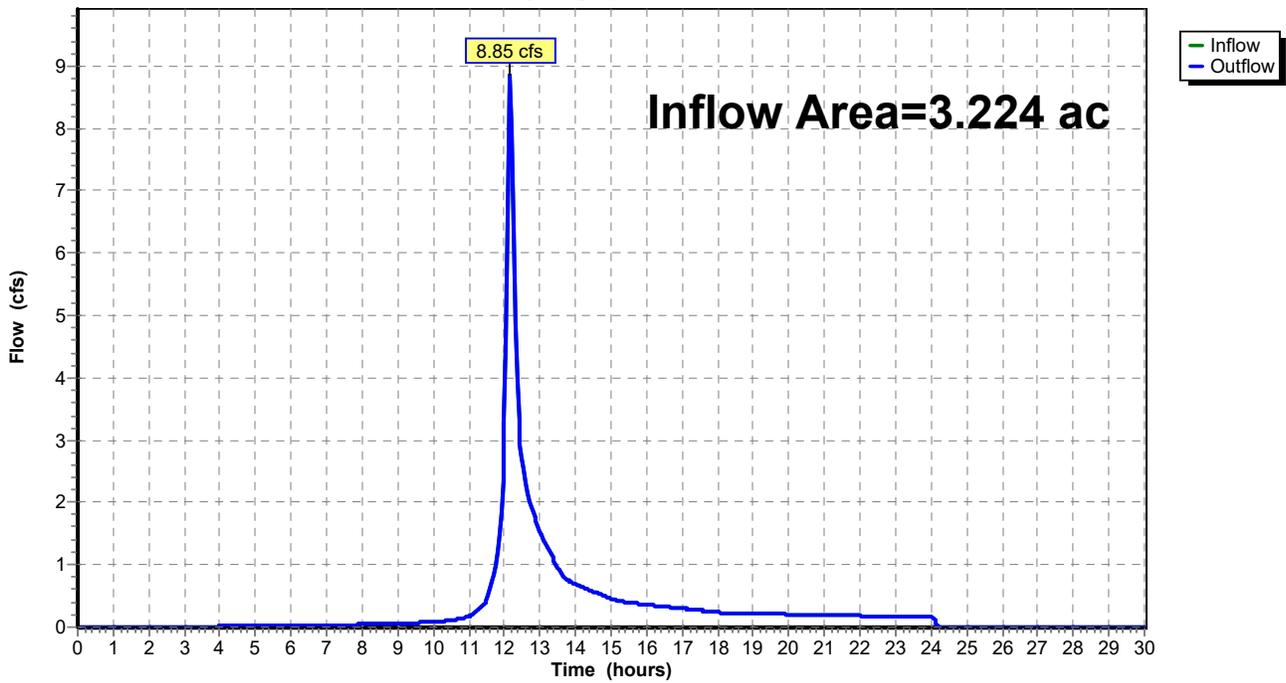
[40] Hint: Not Described (Outflow=Inflow)

Inflow Area = 3.224 ac, 23.86% Impervious, Inflow Depth = 2.61" for 100-Year event
Inflow = 8.85 cfs @ 12.16 hrs, Volume= 0.702 af
Outflow = 8.85 cfs @ 12.16 hrs, Volume= 0.702 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind method, Time Span= 0.00-30.00 hrs, dt= 0.05 hrs

Reach 1R: ex swale

Hydrograph



Summary for Reach 2R: central DA

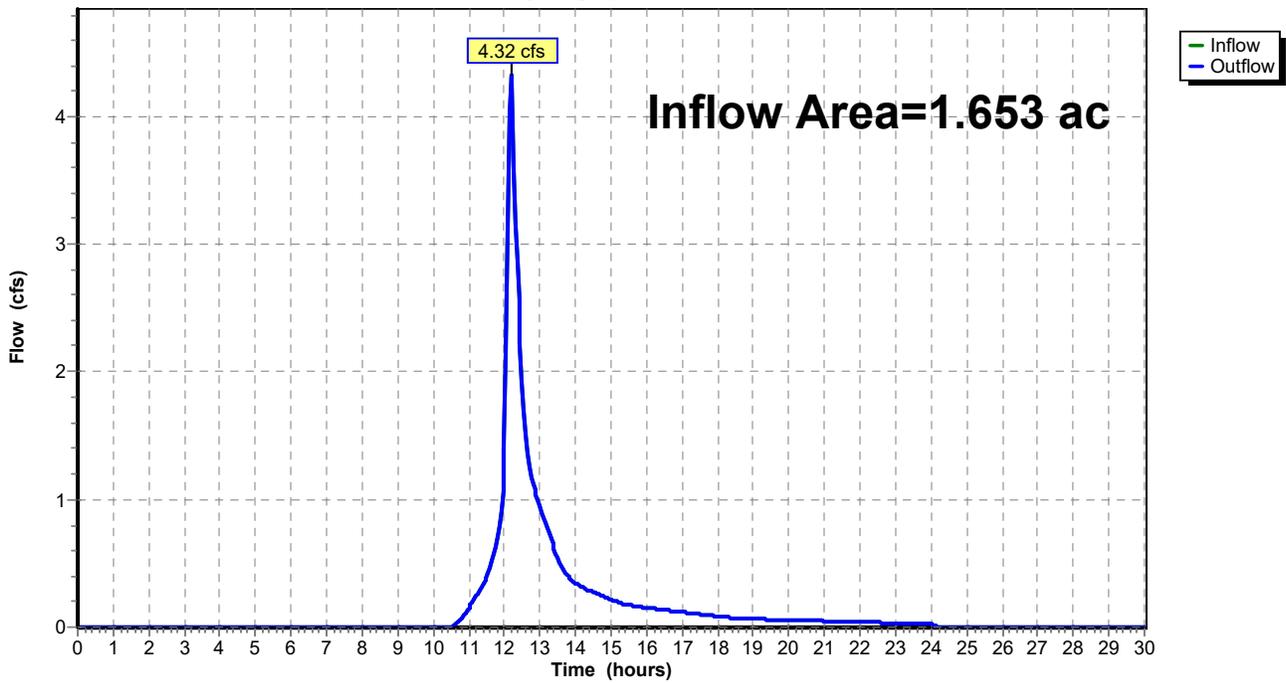
[40] Hint: Not Described (Outflow=Inflow)

Inflow Area = 1.653 ac, 39.84% Impervious, Inflow Depth = 2.51" for 100-Year event
Inflow = 4.32 cfs @ 12.19 hrs, Volume= 0.346 af
Outflow = 4.32 cfs @ 12.19 hrs, Volume= 0.346 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind method, Time Span= 0.00-30.00 hrs, dt= 0.05 hrs

Reach 2R: central DA

Hydrograph

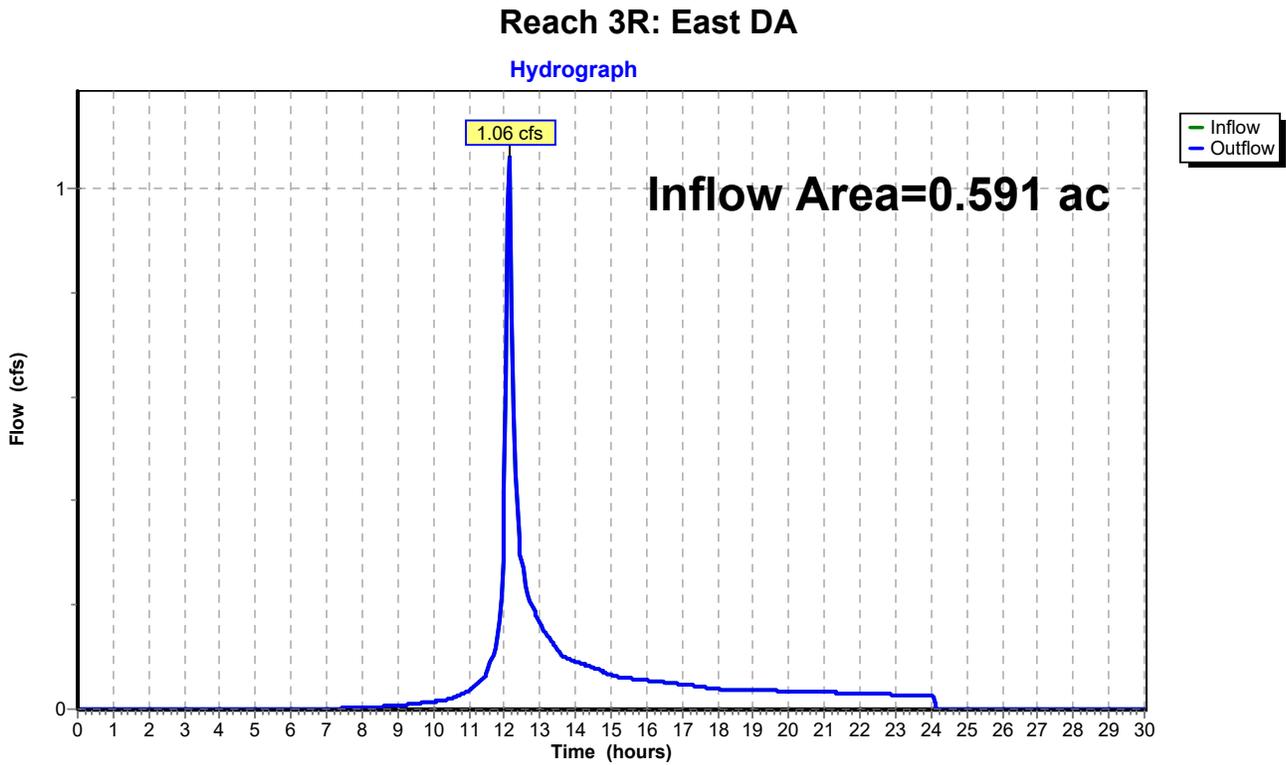


Summary for Reach 3R: East DA

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area = 0.591 ac, 17.77% Impervious, Inflow Depth = 1.82" for 100-Year event
Inflow = 1.06 cfs @ 12.14 hrs, Volume= 0.090 af
Outflow = 1.06 cfs @ 12.14 hrs, Volume= 0.090 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind method, Time Span= 0.00-30.00 hrs, dt= 0.05 hrs



Summary for Reach 4R: (new Reach)

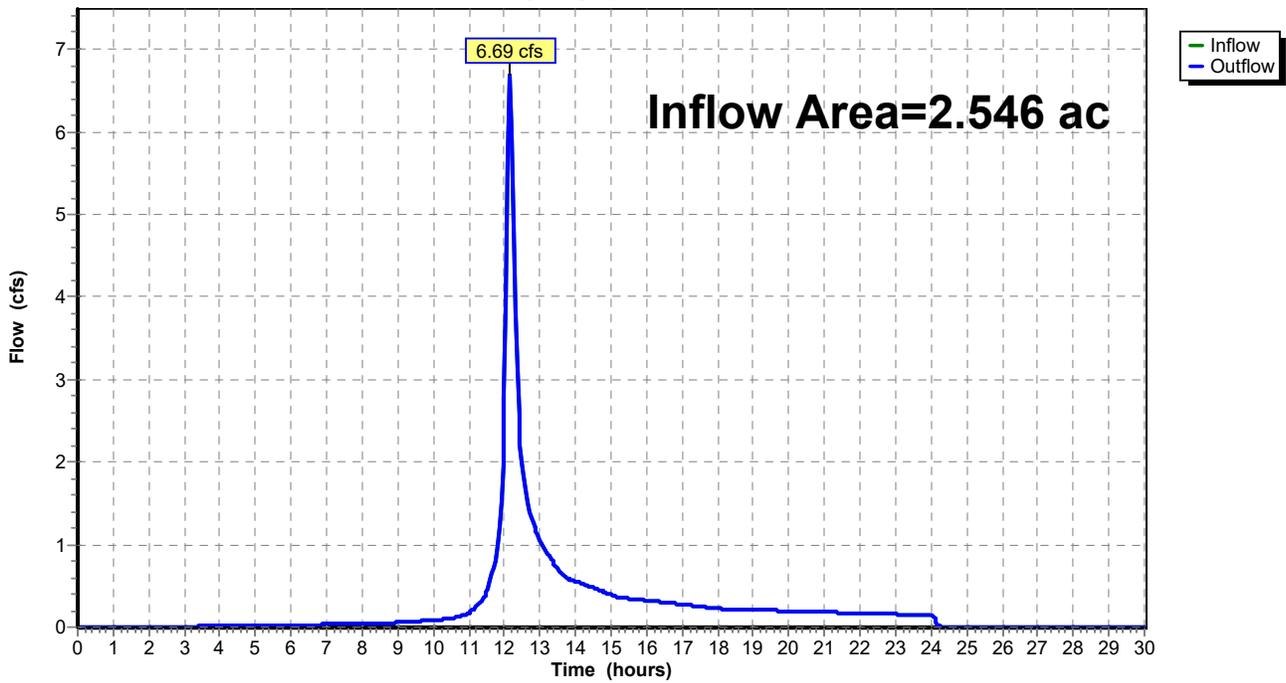
[40] Hint: Not Described (Outflow=Inflow)

Inflow Area = 2.546 ac, 19.18% Impervious, Inflow Depth = 2.73" for 100-Year event
Inflow = 6.69 cfs @ 12.16 hrs, Volume= 0.580 af
Outflow = 6.69 cfs @ 12.16 hrs, Volume= 0.580 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind method, Time Span= 0.00-30.00 hrs, dt= 0.05 hrs

Reach 4R: (new Reach)

Hydrograph



Summary for Pond 1P: UG - system #1

Inflow Area = 0.397 ac, 68.73% Impervious, Inflow Depth = 5.62" for 100-Year event
 Inflow = 2.71 cfs @ 12.11 hrs, Volume= 0.186 af
 Outflow = 2.07 cfs @ 12.17 hrs, Volume= 0.185 af, Atten= 24%, Lag= 3.7 min
 Discarded = 0.06 cfs @ 9.70 hrs, Volume= 0.085 af
 Primary = 2.01 cfs @ 12.17 hrs, Volume= 0.100 af

Routing by Stor-Ind method, Time Span= 0.00-30.00 hrs, dt= 0.05 hrs / 2
 Peak Elev= 306.86' @ 12.17 hrs Surf.Area= 0.027 ac Storage= 0.041 af

Plug-Flow detention time= 48.8 min calculated for 0.185 af (99% of inflow)
 Center-of-Mass det. time= 46.4 min (849.9 - 803.5)

Volume	Invert	Avail.Storage	Storage Description
#1A	304.50'	0.014 af	42.06'W x 27.46'L x 2.44'H Field A 0.065 af Overall - 0.030 af Embedded = 0.035 af x 40.0% Voids
#2A	305.00'	0.028 af	ACF R-Tank HD 1 x 290 Inside #1 Inside= 15.7"W x 17.3"H => 1.80 sf x 2.35'L = 4.2 cf Outside= 15.7"W x 17.3"H => 1.89 sf x 2.35'L = 4.4 cf 290 Chambers in 29 Rows
		0.042 af	Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices
#1	Primary	305.20'	5.0" Vert. Orifice/Grate C= 0.600
#2	Primary	306.40'	8.0" Horiz. Orifice/Grate C= 0.600 Limited to weir flow at low heads
#3	Discarded	304.50'	2.410 in/hr Exfiltration over Surface area Phase-In= 0.01'

Discarded OutFlow Max=0.06 cfs @ 9.70 hrs HW=304.52' (Free Discharge)
 ↳ **3=Exfiltration** (Exfiltration Controls 0.06 cfs)

Primary OutFlow Max=1.86 cfs @ 12.17 hrs HW=306.81' (Free Discharge)
 ↳ **1=Orifice/Grate** (Orifice Controls 0.78 cfs @ 5.71 fps)
 ↳ **2=Orifice/Grate** (Orifice Controls 1.08 cfs @ 3.10 fps)

Pond 1P: UG - system #1 - Chamber Wizard Field A

Chamber Model = ACF R-Tank HD 1 (ACF Environmental R-Tank HD)

Inside= 15.7"W x 17.3"H => 1.80 sf x 2.35'L = 4.2 cf

Outside= 15.7"W x 17.3"H => 1.89 sf x 2.35'L = 4.4 cf

10 Chambers/Row x 2.35' Long = 23.46' Row Length +24.0" End Stone x 2 = 27.46' Base Length

29 Rows x 15.7" Wide + 24.0" Side Stone x 2 = 42.06' Base Width

6.0" Base + 17.3" Chamber Height + 6.0" Cover = 2.44' Field Height

290 Chambers x 4.2 cf = 1,224.3 cf Chamber Storage

290 Chambers x 4.4 cf = 1,288.8 cf Displacement

2,821.9 cf Field - 1,288.8 cf Chambers = 1,533.1 cf Stone x 40.0% Voids = 613.3 cf Stone Storage

Chamber Storage + Stone Storage = 1,837.6 cf = 0.042 af

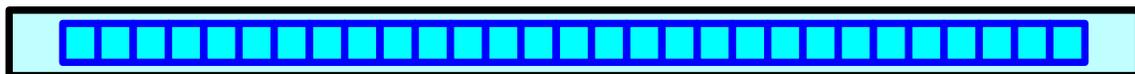
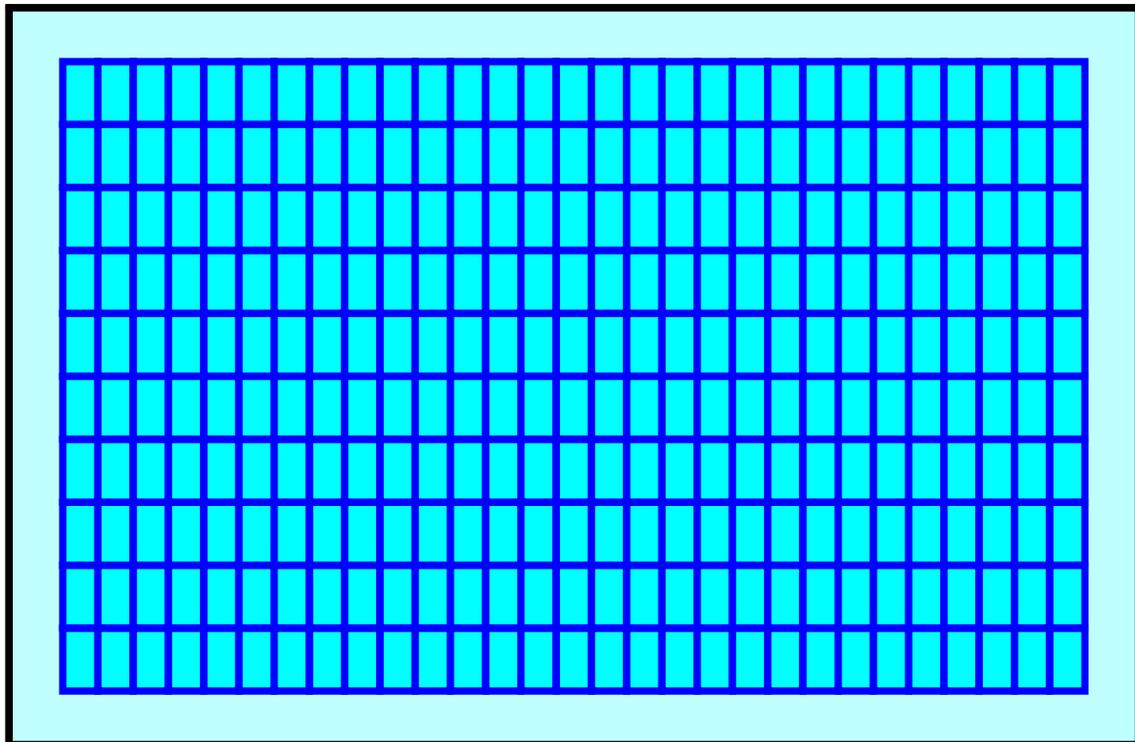
Overall Storage Efficiency = 65.1%

Overall System Size = 27.46' x 42.06' x 2.44'

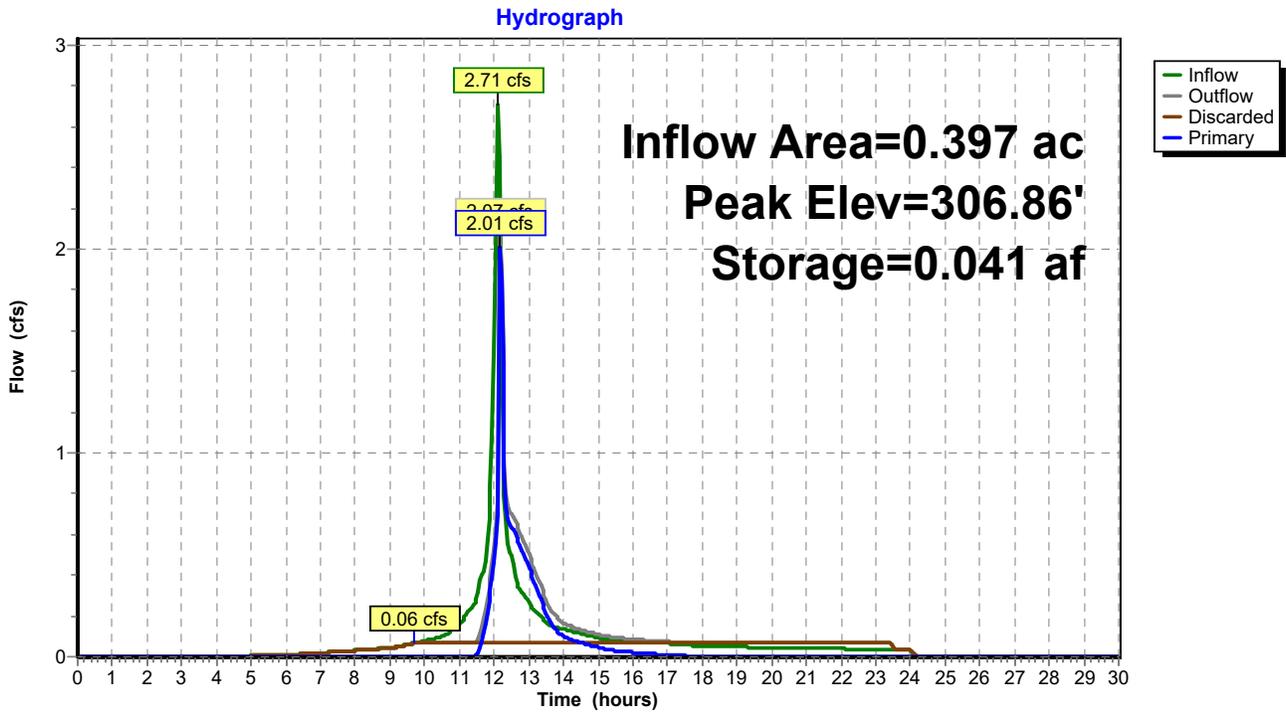
290 Chambers

104.5 cy Field

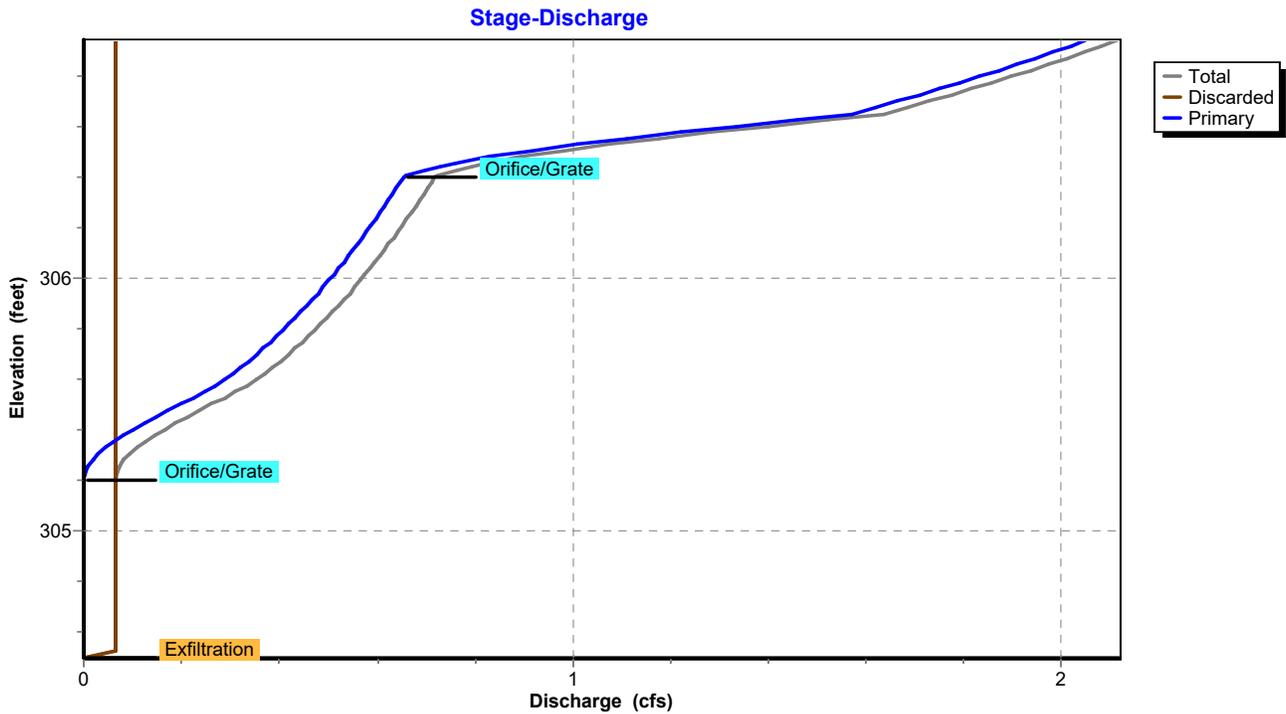
56.8 cy Stone



Pond 1P: UG - system #1



Pond 1P: UG - system #1



Summary for Pond 2P: UG - system #2

Inflow Area = 1.434 ac, 43.88% Impervious, Inflow Depth = 3.94" for 100-Year event
 Inflow = 5.81 cfs @ 12.12 hrs, Volume= 0.471 af
 Outflow = 4.11 cfs @ 12.19 hrs, Volume= 0.469 af, Atten= 29%, Lag= 4.3 min
 Discarded = 0.08 cfs @ 7.05 hrs, Volume= 0.156 af
 Primary = 4.03 cfs @ 12.19 hrs, Volume= 0.314 af

Routing by Stor-Ind method, Time Span= 0.00-30.00 hrs, dt= 0.05 hrs / 3
 Peak Elev= 295.93' @ 12.19 hrs Surf.Area= 0.034 ac Storage= 0.076 af

Plug-Flow detention time= 48.0 min calculated for 0.469 af (100% of inflow)
 Center-of-Mass det. time= 46.3 min (838.9 - 792.7)

Volume	Invert	Avail.Storage	Storage Description
#1A	292.80'	0.020 af	43.37'W x 34.50'L x 3.17'H Field A 0.109 af Overall - 0.060 af Embedded = 0.049 af x 40.0% Voids
#2A	293.30'	0.057 af	ACF R-Tank HD 1.5 x 390 Inside #1 Inside= 15.7"W x 26.0"H => 2.70 sf x 2.35'L = 6.3 cf Outside= 15.7"W x 26.0"H => 2.84 sf x 2.35'L = 6.7 cf 390 Chambers in 30 Rows
		0.076 af	Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices
#1	Primary	293.60'	7.0" Vert. Orifice/Grate C= 0.600
#2	Primary	294.50'	8.0" Vert. Orifice/Grate C= 0.600
#3	Primary	295.80'	12.0" Horiz. Orifice/Grate C= 0.600 Limited to weir flow at low heads
#4	Discarded	292.80'	2.410 in/hr Exfiltration over Surface area Phase-In= 0.01'

Discarded OutFlow Max=0.08 cfs @ 7.05 hrs HW=292.83' (Free Discharge)
 ↳4=Exfiltration (Exfiltration Controls 0.08 cfs)

Primary OutFlow Max=3.97 cfs @ 12.19 hrs HW=295.91' (Free Discharge)
 ↳1=Orifice/Grate (Orifice Controls 1.83 cfs @ 6.85 fps)
 ↳2=Orifice/Grate (Orifice Controls 1.75 cfs @ 5.00 fps)
 ↳3=Orifice/Grate (Weir Controls 0.39 cfs @ 1.10 fps)

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NRCC 24-hr C 100-Year Rainfall=7.68"

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Pond 2P: UG - system #2 - Chamber Wizard Field A

Chamber Model = ACF R-Tank HD 1.5 (ACF Environmental R-Tank HD)

Inside= 15.7"W x 26.0"H => 2.70 sf x 2.35'L = 6.3 cf

Outside= 15.7"W x 26.0"H => 2.84 sf x 2.35'L = 6.7 cf

13 Chambers/Row x 2.35' Long = 30.50' Row Length +24.0" End Stone x 2 = 34.50' Base Length

30 Rows x 15.7" Wide + 24.0" Side Stone x 2 = 43.37' Base Width

6.0" Base + 26.0" Chamber Height + 6.0" Cover = 3.17' Field Height

390 Chambers x 6.3 cf = 2,469.8 cf Chamber Storage

390 Chambers x 6.7 cf = 2,599.7 cf Displacement

4,735.6 cf Field - 2,599.7 cf Chambers = 2,135.8 cf Stone x 40.0% Voids = 854.3 cf Stone Storage

Chamber Storage + Stone Storage = 3,324.1 cf = 0.076 af

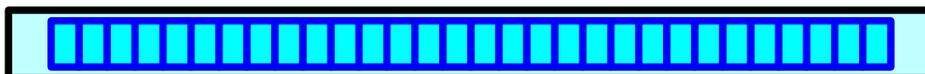
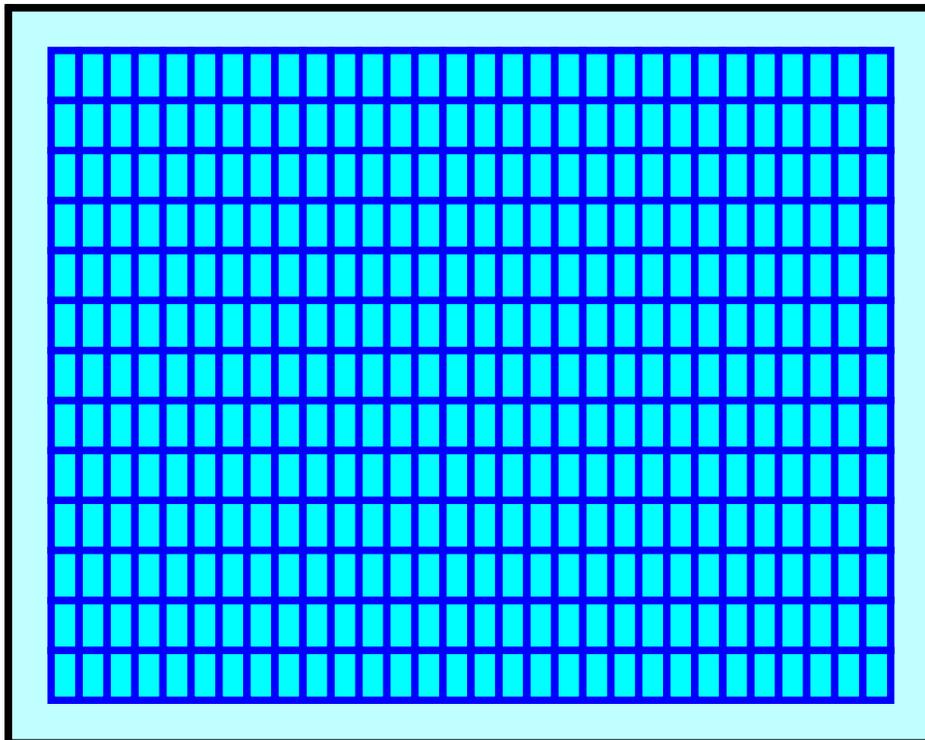
Overall Storage Efficiency = 70.2%

Overall System Size = 34.50' x 43.37' x 3.17'

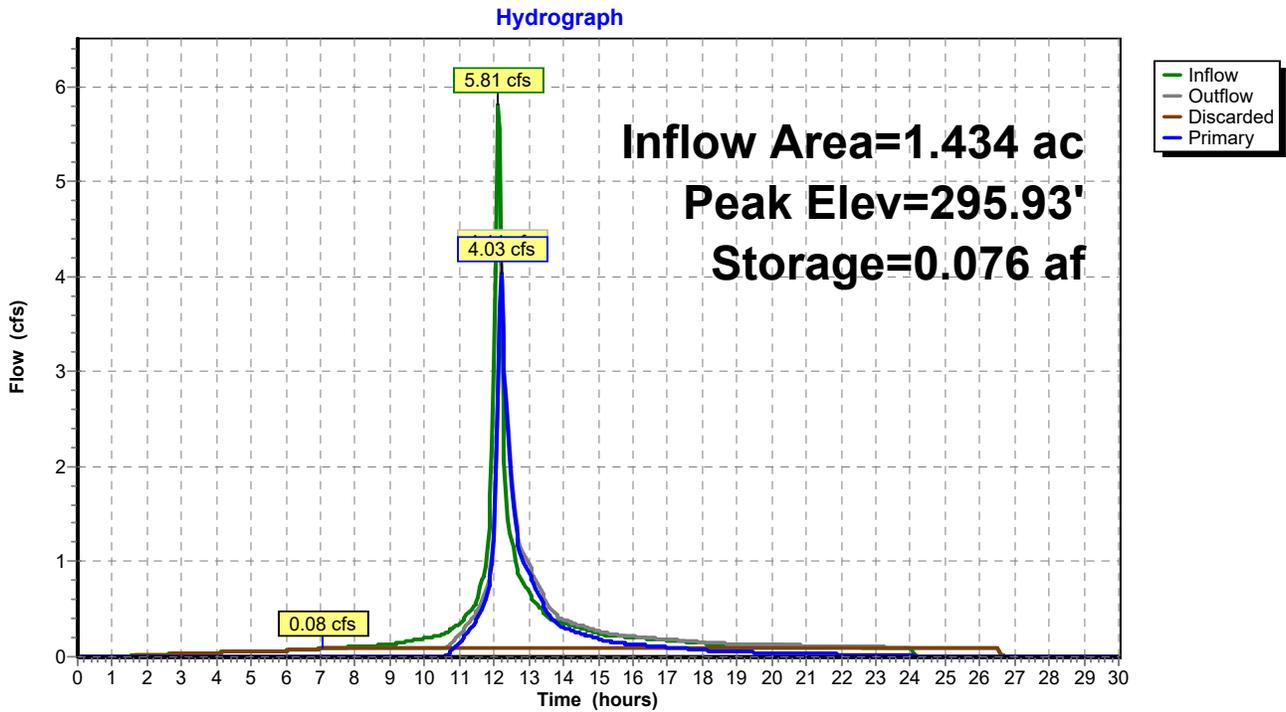
390 Chambers

175.4 cy Field

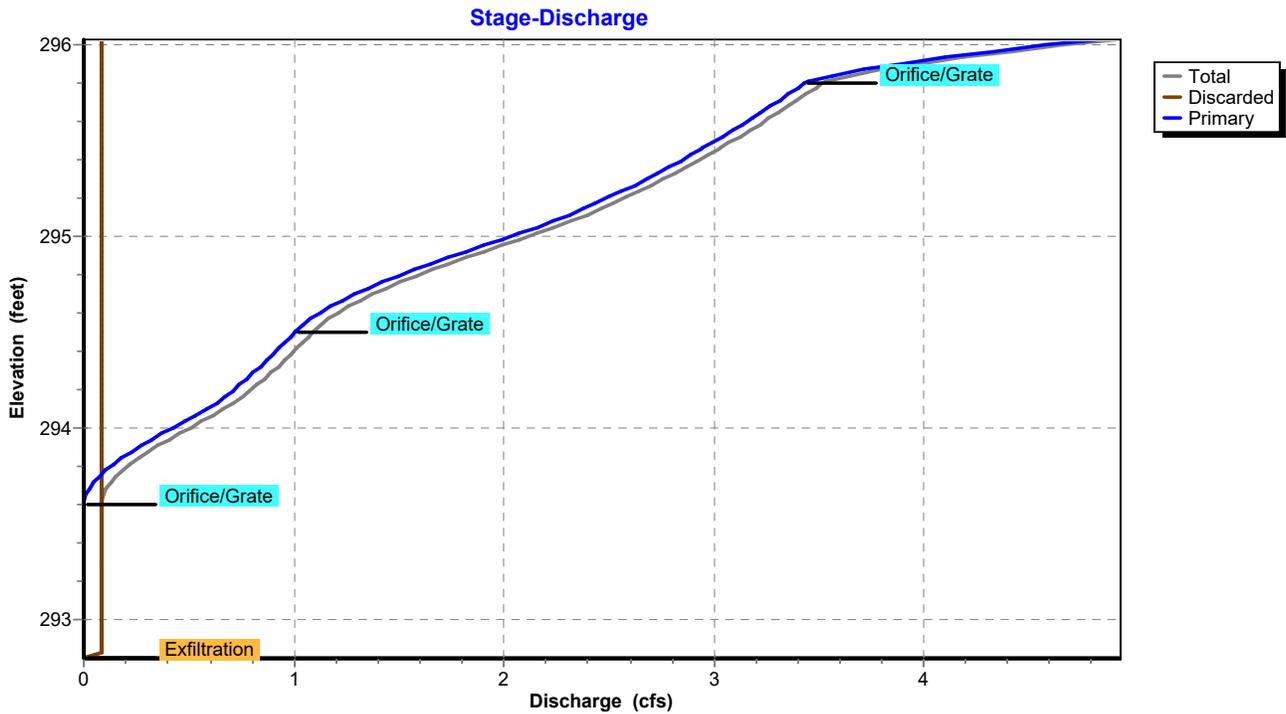
79.1 cy Stone



Pond 2P: UG - system #2



Pond 2P: UG - system #2



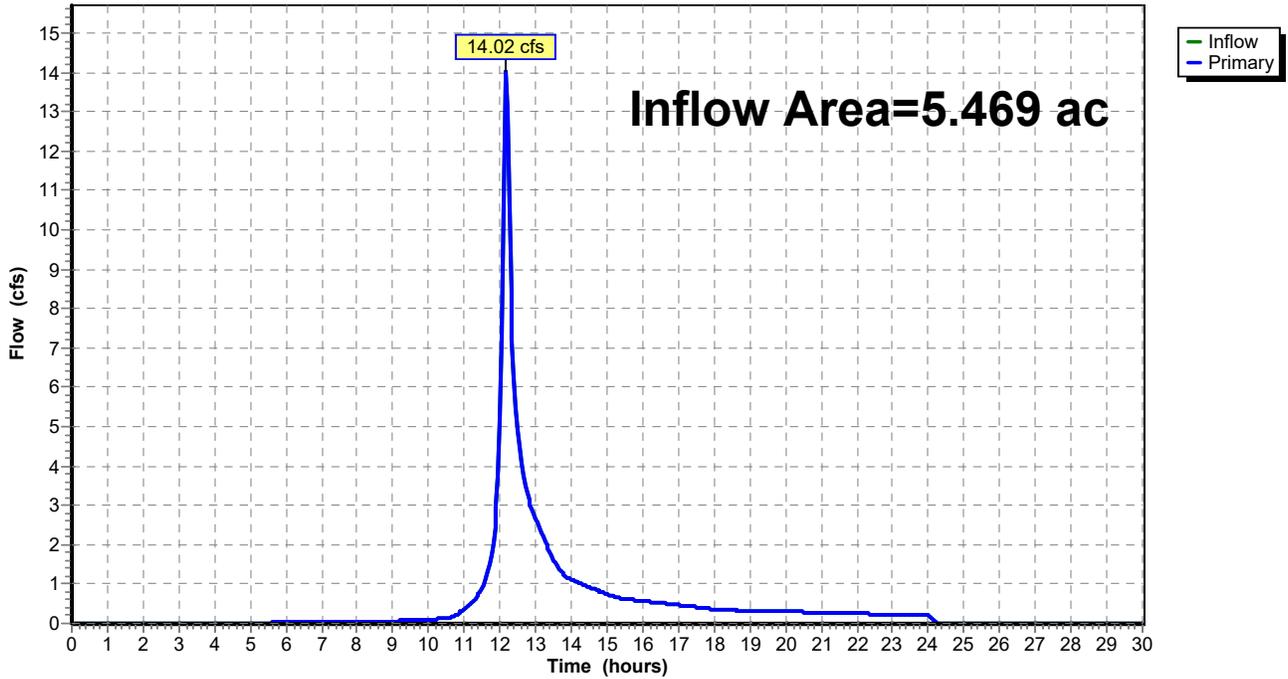
Summary for Link 1L: STUDY POINT- Amethyst Brook

Inflow Area = 5.469 ac, 28.03% Impervious, Inflow Depth = 2.50" for 100-Year event
Inflow = 14.02 cfs @ 12.17 hrs, Volume= 1.137 af
Primary = 14.02 cfs @ 12.17 hrs, Volume= 1.137 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-30.00 hrs, dt= 0.05 hrs

Link 1L: STUDY POINT- Amethyst Brook

Hydrograph



Appendix D – Groundwater Recharge Calculations

December 21, 2020

**Pelham – 20-22 Amherst Road
Stormwater Standard 3 – Recharge Calculations**

Existing Impervious Area

Table 1 shows the existing and proposed impervious and gravel areas on the re-development site.

Table 1. Existing and Proposed Impervious Area

	Existing Area (sf)	Proposed Area (sf)	Increase in Area (sf)
Impervious	27,450	41,840	14,410
Gravel driveways	1,210	-	(1,210)
TOTAL	28,660	41,840	13,200

Proposed Impervious Area & Required Recharge Volume

Table 2 shows the required recharge volume.

Required Recharge Volume is calculated by applying the following equation:

Required Recharge Volume, $Rv = F \times I$

Where, F = Target Depth Factor, 0.60" (for HSG A)
 I = Impervious Area

Table 2. Proposed Increase in Impervious Area and Required Recharge Volume

Increase in Impervious area (sq. ft.)	Required Recharge Volume (cu. ft.)	Provided Recharge Volume (cu. ft.)
13,200	660	1,170

The storage volume provided in **Table 2** is provided through storage below the outlets of the underground stormwater facilities.

This analysis utilizes the "Static Method" for determining required storage volume for infiltration features. Therefore, the minimum required storage volume is equal to the required recharge volume, tabulated above.

The provided infiltration storage volume of 1,170 cu. ft. exceeds the required recharge volume of 660 cu. ft. (considering all proposed new impervious surfaces at the future site).

Capture Area Adjustment

The Massachusetts Stormwater Handbook requires an increase in storage capacity of infiltration features if only a portion of the site’s impervious area is tributary to the stormwater practices. Because this is a redevelopment site, the recharge is calculated on the increase in impervious area. The increase in impervious area of 13,200 sf is entirely tributary to recharge facilities. The proposed design directs over 35,000 sf of impervious surfaces to storage and infiltration facilities.

Drawdown Time

The Rawls infiltration rate for the loamy sand (HSG A) is estimated at 2.41 inches per hour (Massachusetts Stormwater Standards). Drawdown time is dependent on the depth of the system below the lowest outlet and the rate of infiltration.

$$\frac{\text{depth on inches}}{2.41 \frac{\text{in}}{\text{hr}}} = \text{drawdown time}$$

Table 3. Drawdown Time for Each System

UG System #	Elevation at base of system	Elevation of lowest outlet	Depth to infiltrate	Time to infiltrate
1	304.5	305.2	0.7 ft	3.5 hours
2	292.8	293.6	0.8 ft	4 hours

The storage areas should draw down in less than 4 hours which is below the 72-hour requirement.

Appendix E – Water Quality Calculations

December 21, 2020

**20-22 Amherst Road, Pelham, MA
Stormwater Standard 4 – Water Quality Volume**

Existing conditions include untreated gravel and impervious areas of 28,640 sf. Proposed conditions include 41,840 sf of impervious areas (driveways, parking areas, walkways and roofs) The increase in impervious area is 13,200 sq. ft. (Table 1).

Table 1. Existing and Proposed Impervious Areas

	Existing Area (sf)	Proposed Area (sf)	Increase in Area (sf)
Impervious	28,640	41,840	13,200

Required Water Quality Volume is calculated by applying the following equation:

$$\text{Required Water Quality Volume, } WQV = D \times I$$

Where, $D = \text{Depth Factor, } 1''^*$; $I = \text{Impervious Area}$

*Cold water fishery requires a 1" depth factor

Provided water quality volume is the storage provided below the outlet of the underground storage systems. Table 2 summarizes the water quality volume required and provided for the site.

Table 2. Required and Provided WQv

Increase in Impervious Area (sf)	Water Quality Volume Required on increase (cf)	Water Quality Volume Provided in UG systems(cf)
13,200	1,100	1,170

The water quality volume provided exceeds the water quality volume required on the increase in impervious area. Table 3 provides a breakdown of the water quality volume provided by drainage area.

Table 3. Water Quality Volume for Change in Impervious Area by Drainage Area.

Facility	Prop. Impervious Area directed to facility (sf)	Approx. Ex. impervious area (sf)	Impervious Area increase (sf)	Water Quality Volume (cf)	Water Quality Volume Provided (cf)
UG system #1	11,900	9,600	2,300	192	430
UG System #2	23,600	15,090	8,510	710	740

The proposed stormwater facilities provide water quality volume for the increased impervious areas within the tributary drainage areas.

Prior to entering the UG systems, runoff from driveways and parking is treated by Water Quality Units, rated by the manufacturer at over 90% TSS removal. Runoff from roofs (with the exception of the rear roof of #20) is conveyed without treatment.

Table 4 provides a summary of the impervious areas tributary to the Water Quality Units.

Table 4. Proposed Impervious Areas and TSS Removal

	WQU #1	WQU #2	WQU #3	Total
Proposed	10,400 sf	6,700 sf	11,900	29,000 sf

The impervious surfaces treated for TSS removal exceeds the new impervious surfaces created by more than a factor of 2.

Brief Stormceptor Sizing Report - WQ 1

Project Information & Location			
Project Name	20-22 Amherst Rd	Project Number	645710
City	Pelham	State/ Province	Massachusetts
Country	United States of America	Date	12/10/2020
Designer Information		EOR Information (optional)	
Name	David Adams	Name	
Company	Contech	Company	Berkshire Design Group
Phone #	207-855-6191	Phone #	
Email	dadams@conteches.com	Email	

Stormwater Treatment Recommendation

The recommended Stormceptor Model(s) which achieve or exceed the user defined water quality objective for each site within the project are listed in the below Sizing Summary table.

Site Name	WQ 1
Target TSS Removal (%)	80
TSS Removal (%) Provided	93
Recommended Stormceptor Model	STC 450i

The recommended Stormceptor Model achieves the water quality objectives based on the selected inputs, historical rainfall records and selected particle size distribution.

Stormceptor Sizing Summary	
Stormceptor Model	% TSS Removal Provided
STC 450i	93
STC 900	96
STC 1200	96
STC 1800	97
STC 2400	97
STC 3600	98
STC 4800	98
STC 6000	99
STC 7200	99
STC 11000	99
STC 13000	99
STC 16000	99

Sizing Details			
Drainage Area		Water Quality Objective	
Total Area (acres)	0.24	TSS Removal (%)	80.0
Imperviousness %	100.0	Runoff Volume Capture (%)	
Rainfall		Oil Spill Capture Volume (Gal)	
Station Name	EAST BRIMFIELD LAKE	Peak Conveyed Flow Rate (CFS)	
State/Province	Massachusetts	Water Quality Flow Rate (CFS)	
Station ID #	2107	Up Stream Storage	
Years of Records	45	Storage (ac-ft)	Discharge (cfs)
Latitude	42°7'0"N	0.000	0.000
Longitude	72°8'0"W	Up Stream Flow Diversion	
		Max. Flow to Stormceptor (cfs)	

Particle Size Distribution (PSD) The selected PSD defines TSS removal		
OK-110		
Particle Diameter (microns)	Distribution %	Specific Gravity
1.0	0.0	2.65
53.0	3.0	2.65
75.0	15.0	2.65
88.0	25.0	2.65
106.0	41.0	2.65
125.0	15.0	2.65
150.0	1.0	2.65
212.0	0.0	2.65

Notes
<ul style="list-style-type: none"> Stormceptor performance estimates are based on simulations using PCSWMM for Stormceptor, which uses the EPA Rainfall and Runoff modules. Design estimates listed are only representative of specific project requirements based on total suspended solids (TSS) removal defined by the selected PSD, and based on stable site conditions only, after construction is completed. For submerged applications or sites specific to spill control, please contact your local Stormceptor representative for further design assistance.

For Stormceptor Specifications and Drawings Please Visit:
<https://www.conteches.com/technical-guides/search?filter=1WBC005EYX>

Brief Stormceptor Sizing Report - WQ 2

Project Information & Location			
Project Name	20-22 Amherst Rd	Project Number	645710
City	Pelham	State/ Province	Massachusetts
Country	United States of America	Date	12/10/2020
Designer Information		EOR Information (optional)	
Name	David Adams	Name	
Company	Contech	Company	Berkshire Design Group
Phone #	207-855-6191	Phone #	
Email	dadams@conteches.com	Email	

Stormwater Treatment Recommendation

The recommended Stormceptor Model(s) which achieve or exceed the user defined water quality objective for each site within the project are listed in the below Sizing Summary table.

Site Name	WQ 2
Target TSS Removal (%)	80
TSS Removal (%) Provided	94
Recommended Stormceptor Model	STC 450i

The recommended Stormceptor Model achieves the water quality objectives based on the selected inputs, historical rainfall records and selected particle size distribution.

Stormceptor Sizing Summary	
Stormceptor Model	% TSS Removal Provided
STC 450i	94
STC 900	97
STC 1200	97
STC 1800	98
STC 2400	98
STC 3600	99
STC 4800	99
STC 6000	99
STC 7200	99
STC 11000	100
STC 13000	100
STC 16000	100

Sizing Details			
Drainage Area		Water Quality Objective	
Total Area (acres)	0.15	TSS Removal (%)	80.0
Imperviousness %	100.0	Runoff Volume Capture (%)	
Rainfall		Oil Spill Capture Volume (Gal)	
Station Name	EAST BRIMFIELD LAKE	Peak Conveyed Flow Rate (CFS)	
State/Province	Massachusetts	Water Quality Flow Rate (CFS)	
Station ID #	2107	Up Stream Storage	
Years of Records	45	Storage (ac-ft)	Discharge (cfs)
Latitude	42°7'0"N	0.000	0.000
Longitude	72°8'0"W	Up Stream Flow Diversion	
		Max. Flow to Stormceptor (cfs)	

Particle Size Distribution (PSD) The selected PSD defines TSS removal		
OK-110		
Particle Diameter (microns)	Distribution %	Specific Gravity
1.0	0.0	2.65
53.0	3.0	2.65
75.0	15.0	2.65
88.0	25.0	2.65
106.0	41.0	2.65
125.0	15.0	2.65
150.0	1.0	2.65
212.0	0.0	2.65

Notes
<ul style="list-style-type: none"> Stormceptor performance estimates are based on simulations using PCSWMM for Stormceptor, which uses the EPA Rainfall and Runoff modules. Design estimates listed are only representative of specific project requirements based on total suspended solids (TSS) removal defined by the selected PSD, and based on stable site conditions only, after construction is completed. For submerged applications or sites specific to spill control, please contact your local Stormceptor representative for further design assistance.

For Stormceptor Specifications and Drawings Please Visit:
<https://www.conteches.com/technical-guides/search?filter=1WBC005EYX>

Brief Stormceptor Sizing Report - WQ 3

Project Information & Location			
Project Name	20-22 Amherst Rd	Project Number	645710
City	Pelham	State/ Province	Massachusetts
Country	United States of America	Date	12/10/2020
Designer Information		EOR Information (optional)	
Name	David Adams	Name	
Company	Contech	Company	Berkshire Design Group
Phone #	207-855-6191	Phone #	
Email	dadams@conteches.com	Email	

Stormwater Treatment Recommendation

The recommended Stormceptor Model(s) which achieve or exceed the user defined water quality objective for each site within the project are listed in the below Sizing Summary table.

Site Name	WQ 3
Target TSS Removal (%)	80
TSS Removal (%) Provided	92
Recommended Stormceptor Model	STC 450i

The recommended Stormceptor Model achieves the water quality objectives based on the selected inputs, historical rainfall records and selected particle size distribution.

Stormceptor Sizing Summary	
Stormceptor Model	% TSS Removal Provided
STC 450i	92
STC 900	96
STC 1200	96
STC 1800	96
STC 2400	97
STC 3600	98
STC 4800	98
STC 6000	98
STC 7200	99
STC 11000	99
STC 13000	99
STC 16000	99

Sizing Details			
Drainage Area		Water Quality Objective	
Total Area (acres)	0.27	TSS Removal (%)	80.0
Imperviousness %	100.0	Runoff Volume Capture (%)	
Rainfall		Oil Spill Capture Volume (Gal)	
Station Name	EAST BRIMFIELD LAKE	Peak Conveyed Flow Rate (CFS)	
State/Province	Massachusetts	Water Quality Flow Rate (CFS)	
Station ID #	2107	Up Stream Storage	
Years of Records	45	Storage (ac-ft)	Discharge (cfs)
Latitude	42°7'0"N	0.000	0.000
Longitude	72°8'0"W	Up Stream Flow Diversion	
		Max. Flow to Stormceptor (cfs)	

Particle Size Distribution (PSD) The selected PSD defines TSS removal		
OK-110		
Particle Diameter (microns)	Distribution %	Specific Gravity
1.0	0.0	2.65
53.0	3.0	2.65
75.0	15.0	2.65
88.0	25.0	2.65
106.0	41.0	2.65
125.0	15.0	2.65
150.0	1.0	2.65
212.0	0.0	2.65

Notes
<ul style="list-style-type: none"> Stormceptor performance estimates are based on simulations using PCSWMM for Stormceptor, which uses the EPA Rainfall and Runoff modules. Design estimates listed are only representative of specific project requirements based on total suspended solids (TSS) removal defined by the selected PSD, and based on stable site conditions only, after construction is completed. For submerged applications or sites specific to spill control, please contact your local Stormceptor representative for further design assistance.

For Stormceptor Specifications and Drawings Please Visit:
<https://www.conteches.com/technical-guides/search?filter=1WBC005EYX>

Appendix F – Stormwater Management System – Operation & Maintenance Plan

Stormwater Management System

Operation & Maintenance Plan

During Construction

The Contractor shall be responsible for inspection and maintenance during construction.

At all times, siltation fabric fencing, stakes and straw bales/wattles, sufficient to construct a sedimentation control barrier a minimum of 50 feet long, shall be stockpiled on the site in order to repair established barriers which may be damaged or breached.

An inspection of all erosion control and stormwater management systems shall be conducted by the Contractor at least once a week and during all rain storms until the completion of construction. In case of any noted breach or failure, the Contractor shall immediately make appropriate repairs to any erosion control system and notify the engineer of any problems involving stormwater management systems.

A rain storm shall be defined as any of the following:

- A storm in which rain is predicted to last for twelve consecutive hours or more.
- A storm for which a flash flood watch or warning is issued.
- A single storm predicted to have a cumulative rainfall of greater than one-half inch.
- A storm not meeting the previous three thresholds but which would mark a third consecutive day of measurable rainfall.

The Contractor shall also inspect the erosion control and stormwater management systems at times of significant increase in surface water runoff due to rapid thawing when the risk of failure of erosion control measures is elevated.

In such instances as remedial action is necessary, the Contractor shall repair any and all significant deficiencies in erosion control systems within two days.

The Pelham Department of Public Works shall be notified of any significant failure of stormwater management systems or erosion and sediment control measures and shall be notified of any release of pollutants to a water body (stream, brook, pond, etc.).

The Contractor shall remove the sediment from behind the fence of the sedimentation control barrier when the accumulated sediment has reached one-half of the original installed height of the barrier.

This project requires a NPDES General Permit for Stormwater Discharges from Construction Activities. Contractor and Owner are responsible for finalizing a Stormwater Pollution Prevention Plan (SWPPP) and filing for the NPDES permit prior to the start of construction. All clearing, grading, drainage, construction, and development shall be conducted in strict accordance with the SWPPP.

Post-Construction

Stormwater Management System Owner:

Home City Development Inc.

Party Responsible for Operation & Maintenance:

Home City Development Inc.

Inspection & Maintenance Schedule:

1) *Driveway and Parking Lot Sweeping*

Driveway and parking area sweeping shall take place annually during the spring cleanup.

2) *Grass and Stone Swales*

The Amethyst Apartments development includes grass swales to convey stormwater to yard drains and culverts.

Inspect swales or conveyances multiple times in the first few months after construction and twice per year thereafter. Look for signs of erosion and, if found, repair immediately. Swales shall be mowed at least once per year to prevent the growth of shrubs or trees but may be mowed more often at the discretion of the property owner.

3) *Catch basins*

Structures shall be inspected four times per year and cleaned if sediment build up exceeds 6" but no less than every 2 years. Oil and sediments shall be removed and disposed of in accordance with local, state and federal guidelines and regulations. In the case of an oil or bulk pollutant release, the system must be cleaned immediately following the spill and the proper authorities notified.

4) *Yard Drains*

Yard drains should be inspected quarterly and cleaned annually or more often if required. Oil and sediments should be removed and disposed of in accordance with local, state and federal guidelines and regulations. In the case of an oil or bulk pollutant release, the system must be cleaned immediately following the spill and the proper authorities notified.

5) *Water Quality Units*

The stormwater treatment chambers are Stormceptors manufactured by Contech. These units provide water quality for the driveways and parking lots.

The stormwater treatment chamber should be inspected at regular intervals and maintained when necessary to ensure optimum performance. The system shall be inspected at least four times during the first year and at least twice per year thereafter. Sediment shall be removed any time it has built up to more than 6" deep. At a minimum, the unit shall be cleaned once per year. If sediment accumulates fast enough to require removal more than once per year, the inspection frequency shall be increased.

The visual inspection should ascertain that the system components are in working order and that there are no blockages or obstructions in the inlet and separation screen. The inspection should also quantify the accumulation of hydrocarbons, trash, and sediment in the system. Measuring pollutant accumulation can be done with a calibrated dipstick, tape measure or other measuring instrument.

The hydrodynamic separator system should be cleaned when the level of sediment has reached 6 inches or when an appreciable level of hydrocarbons and trash covers over 50% of the water surface of the separator. The level of sediment is easily determined by measuring from finished grade down to the top of the sediment pile. To avoid underestimating the level of sediment in the chamber, the measuring device must be lowered to the top of the sediment pile carefully. Particles at the top of the pile typically offer less resistance to the end of the rod than consolidated particles toward the bottom of the pile. Sediment shall be removed by a vacuum truck and disposed of in accordance with applicable regulations.

7) *Subsurface detention and Infiltration Systems*

Maintenance Requirements

- A. A routine maintenance effort is required to ensure proper performance of the R-Tank system. The Maintenance program should be focused on pretreatment systems. Ensuring these structures are clean and functioning properly will reduce the risk of contamination of the R-Tank system and stormwater released from the site. Pre-treatment systems shall be inspected yearly, or as directed by the regulatory agency and by the manufacturer (for proprietary systems). Maintain as needed using acceptable practices or following manufacturer's guidelines (for proprietary systems).
- B. Inspection and/or Maintenance Ports in the R-Tank system will need to be inspected for accumulation of sediments at least quarterly through the first year of operation and at least yearly thereafter. This is done by removing the cap of the port and using a measuring device long enough to reach the bottom of the R-Tank system and stiff enough to push through the loose sediments, allowing a depth measurement.
- C. If sediment has accumulated to the level noted in the R-Tank Maintenance Guide or beyond a level acceptable to the Owner's engineer, the R-Tank system should be flushed.
- D. A flushing event consists of pumping water into the Maintenance Port and/or adjacent structure, allowing the turbulent flows through the R-Tank system to re-suspend the fine sediments. If multiple Maintenance Ports have been installed, water should be pumped into each port to maximize flushing efficiency. Sediment-laden water can be filtered through a Dirtbag® or approved equivalent if permitted by the locality.

8) *Outlet Control Structures*

The outlet control structures for the R-Tanks shall be inspected quarterly and after large storms (greater than 2" in 24-hours) to ensure no debris is prohibiting flow through the outlet orifices in the riser pipe. Inspections should confirm that there is no standing water in the structure and that the bottom is visible. All materials removed from the outlet control structure shall be removed and disposed of in accordance with local, state and federal guidelines and regulations.

9) Storm Drain Outlet Protection

The integrity of riprap outlet armoring shall be inspected twice per year for signs of dislodged stones or erosion at the perimeter of the apron. Any damage shall be repaired to return the apron to the condition shown in the contract documents. While some growth of herbaceous plants is expected, regular trimming is required to prevent growth from restricting the free flow of water across the apron.

10) Level Lip Spreader

Inspect level lip spreaders multiple times in the first few months after construction and twice per year thereafter. Clean out any debris or sediment as needed. Note and repair any erosion or low spots at the ends of the curb of the spreader. It is recommended that sediment removal, if any, be performed after the completion of the spring snow melt.

Appendix G – Massachusetts DEP Stormwater Checklist



Checklist for Stormwater Report

A. Introduction

Important: When filling out forms on the computer, use only the tab key to move your cursor - do not use the return key.



A Stormwater Report must be submitted with the Notice of Intent permit application to document compliance with the Stormwater Management Standards. The following checklist is NOT a substitute for the Stormwater Report (which should provide more substantive and detailed information) but is offered here as a tool to help the applicant organize their Stormwater Management documentation for their Report and for the reviewer to assess this information in a consistent format. As noted in the Checklist, the Stormwater Report must contain the engineering computations and supporting information set forth in Volume 3 of the [Massachusetts Stormwater Handbook](#). The Stormwater Report must be prepared and certified by a Registered Professional Engineer (RPE) licensed in the Commonwealth.

The Stormwater Report must include:

- The Stormwater Checklist completed and stamped by a Registered Professional Engineer (see page 2) that certifies that the Stormwater Report contains all required submittals.¹ This Checklist is to be used as the cover for the completed Stormwater Report.
- Applicant/Project Name
- Project Address
- Name of Firm and Registered Professional Engineer that prepared the Report
- Long-Term Pollution Prevention Plan required by Standards 4-6
- Construction Period Pollution Prevention and Erosion and Sedimentation Control Plan required by Standard 8²
- Operation and Maintenance Plan required by Standard 9

In addition to all plans and supporting information, the Stormwater Report must include a brief narrative describing stormwater management practices, including environmentally sensitive site design and LID techniques, along with a diagram depicting runoff through the proposed BMP treatment train. Plans are required to show existing and proposed conditions, identify all wetland resource areas, NRCS soil types, critical areas, Land Uses with Higher Potential Pollutant Loads (LUHPPL), and any areas on the site where infiltration rate is greater than 2.4 inches per hour. The Plans shall identify the drainage areas for both existing and proposed conditions at a scale that enables verification of supporting calculations.

As noted in the Checklist, the Stormwater Management Report shall document compliance with each of the Stormwater Management Standards as provided in the Massachusetts Stormwater Handbook. The soils evaluation and calculations shall be done using the methodologies set forth in Volume 3 of the Massachusetts Stormwater Handbook.

To ensure that the Stormwater Report is complete, applicants are required to fill in the Stormwater Report Checklist by checking the box to indicate that the specified information has been included in the Stormwater Report. If any of the information specified in the checklist has not been submitted, the applicant must provide an explanation. The completed Stormwater Report Checklist and Certification

¹ The Stormwater Report may also include the Illicit Discharge Compliance Statement required by Standard 10. If not included in the Stormwater Report, the Illicit Discharge Compliance Statement must be submitted prior to the discharge of stormwater runoff to the post-construction best management practices.

² For some complex projects, it may not be possible to include the Construction Period Erosion and Sedimentation Control Plan in the Stormwater Report. In that event, the issuing authority has the discretion to issue an Order of Conditions that approves the project and includes a condition requiring the proponent to submit the Construction Period Erosion and Sedimentation Control Plan before commencing any land disturbance activity on the site.

B. Stormwater Checklist and Certification



Checklist for Stormwater Report

The following checklist is intended to serve as a guide for applicants as to the elements that ordinarily need to be addressed in a complete Stormwater Report. The checklist is also intended to provide conservation commissions and other reviewing authorities with a summary of the components necessary for a comprehensive Stormwater Report that addresses the ten Stormwater Standards.

Note: Because stormwater requirements vary from project to project, it is possible that a complete Stormwater Report may not include information on some of the subjects specified in the Checklist. If it is determined that a specific item does not apply to the project under review, please note that the item is not applicable (N.A.) and provide the reasons for that determination.

A complete checklist must include the Certification set forth below signed by the Registered Professional Engineer who prepared the Stormwater Report.

Registered Professional Engineer's Certification

I have reviewed the Stormwater Report, including the soil evaluation, computations, Long-term Pollution Prevention Plan, the Construction Period Erosion and Sedimentation Control Plan (if included), the Long-term Post-Construction Operation and Maintenance Plan, the Illicit Discharge Compliance Statement (if included) and the plans showing the stormwater management system, and have determined that they have been prepared in accordance with the requirements of the Stormwater Management Standards as further elaborated by the Massachusetts Stormwater Handbook. I have also determined that the information presented in the Stormwater Checklist is accurate and that the information presented in the Stormwater Report accurately reflects conditions at the site as of the date of this permit application.

Registered Professional Engineer Block and Signature

Signature and Date

Checklist

Project Type: Is the application for new development, redevelopment, or a mix of new and redevelopment?

- New development
- Redevelopment
- Mix of New Development and Redevelopment

Checklist (continued)



Checklist for Stormwater Report

LID Measures: Stormwater Standards require LID measures to be considered. Document what environmentally sensitive design and LID Techniques were considered during the planning and design of the project:

- No disturbance to any Wetland Resource Areas
- Site Design Practices (e.g. clustered development, reduced frontage setbacks)
- Reduced Impervious Area (Redevelopment Only)
- Minimizing disturbance to existing trees and shrubs
- LID Site Design Credit Requested:
 - Credit 1
 - Credit 2
 - Credit 3
- Use of “country drainage” versus curb and gutter conveyance and pipe
- Bioretention Cells (includes Rain Gardens)
- Constructed Stormwater Wetlands (includes Gravel Wetlands designs)
- Treebox Filter
- Water Quality Swale
- Grass Channel
- Green Roof
- Other (describe): _____

Standard 1: No New Untreated Discharges

- No new untreated discharges
- Outlets have been designed so there is no erosion or scour to wetlands and waters of the Commonwealth
- Supporting calculations specified in Volume 3 of the Massachusetts Stormwater Handbook included.

Checklist (continued)



Checklist for Stormwater Report

Standard 2: Peak Rate Attenuation

- Standard 2 waiver requested because the project is located in land subject to coastal storm flowage and stormwater discharge is to a wetland subject to coastal flooding.
- Evaluation provided to determine whether off-site flooding increases during the 100-year 24-hour storm.
- Calculations provided to show that post-development peak discharge rates do not exceed pre-development rates for the 2-year and 10-year 24-hour storms. If evaluation shows that off-site flooding increases during the 100-year 24-hour storm, calculations are also provided to show that post-development peak discharge rates do not exceed pre-development rates for the 100-year 24-hour storm.

Standard 3: Recharge

- Soil Analysis provided.
- Required Recharge Volume calculation provided.
- Required Recharge volume reduced through use of the LID site Design Credits.
- Sizing the infiltration, BMPs is based on the following method: Check the method used.
 - Static
 - Simple Dynamic
 - Dynamic Field¹
- Runoff from all impervious areas at the site discharging to the infiltration BMP.
- Runoff from all impervious areas at the site is *not* discharging to the infiltration BMP and calculations are provided showing that the drainage area contributing runoff to the infiltration BMPs is sufficient to generate the required recharge volume.
- Recharge BMPs have been sized to infiltrate the Required Recharge Volume.
- Recharge BMPs have been sized to infiltrate the Required Recharge Volume *only* to the maximum extent practicable for the following reason:
 - Site is comprised solely of C and D soils and/or bedrock at the land surface
 - M.G.L. c. 21E sites pursuant to 310 CMR 40.0000
 - Solid Waste Landfill pursuant to 310 CMR 19.000
 - Project is otherwise subject to Stormwater Management Standards only to the maximum extent practicable.
- Calculations showing that the infiltration BMPs will drain in 72 hours are provided.
- Property includes a M.G.L. c. 21E site or a solid waste landfill and a mounding analysis is included.

¹ 80% TSS removal is required prior to discharge to infiltration BMP if Dynamic Field method is used.

Checklist (continued)



Checklist for Stormwater Report

Standard 3: Recharge (continued)

- The infiltration BMP is used to attenuate peak flows during storms greater than or equal to the 10-year 24-hour storm and separation to seasonal high groundwater is less than 4 feet and a mounding analysis is provided.
- Documentation is provided showing that infiltration BMPs do not adversely impact nearby wetland resource areas.

Standard 4: Water Quality

The Long-Term Pollution Prevention Plan typically includes the following:

- Good housekeeping practices;
 - Provisions for storing materials and waste products inside or under cover;
 - Vehicle washing controls;
 - Requirements for routine inspections and maintenance of stormwater BMPs;
 - Spill prevention and response plans;
 - Provisions for maintenance of lawns, gardens, and other landscaped areas;
 - Requirements for storage and use of fertilizers, herbicides, and pesticides;
 - Pet waste management provisions;
 - Provisions for operation and management of septic systems;
 - Provisions for solid waste management;
 - Snow disposal and plowing plans relative to Wetland Resource Areas;
 - Winter Road Salt and/or Sand Use and Storage restrictions;
 - Street sweeping schedules;
 - Provisions for prevention of illicit discharges to the stormwater management system;
 - Documentation that Stormwater BMPs are designed to provide for shutdown and containment in the event of a spill or discharges to or near critical areas or from LUHPPL;
 - Training for staff or personnel involved with implementing Long-Term Pollution Prevention Plan;
 - List of Emergency contacts for implementing Long-Term Pollution Prevention Plan.
- A Long-Term Pollution Prevention Plan is attached to Stormwater Report and is included as an attachment to the Wetlands Notice of Intent.
 - Treatment BMPs subject to the 44% TSS removal pretreatment requirement and the one inch rule for calculating the water quality volume are included, and discharge:
 - is within the Zone II or Interim Wellhead Protection Area
 - is near or to other critical areas
 - is within soils with a rapid infiltration rate (greater than 2.4 inches per hour)
 - involves runoff from land uses with higher potential pollutant loads.
 - The Required Water Quality Volume is reduced through use of the LID site Design Credits.
 - Calculations documenting that the treatment train meets the 80% TSS removal requirement and, if applicable, the 44% TSS removal pretreatment requirement, are provided.

Checklist (continued)



Checklist for Stormwater Report

Standard 4: Water Quality (continued)

- The BMP is sized (and calculations provided) based on:
 - The ½" or 1" Water Quality Volume or
 - The equivalent flow rate associated with the Water Quality Volume and documentation is provided showing that the BMP treats the required water quality volume.
- The applicant proposes to use proprietary BMPs, and documentation supporting use of proprietary BMP and proposed TSS removal rate is provided. This documentation may be in the form of the propriety BMP checklist found in Volume 2, Chapter 4 of the Massachusetts Stormwater Handbook and submitting copies of the TARP Report, STEP Report, and/or other third party studies verifying performance of the proprietary BMPs.
- A TMDL exists that indicates a need to reduce pollutants other than TSS and documentation showing that the BMPs selected are consistent with the TMDL is provided.

Standard 5: Land Uses With Higher Potential Pollutant Loads (LUHPPLs)

- The NPDES Multi-Sector General Permit covers the land use and the Stormwater Pollution Prevention Plan (SWPPP) has been included with the Stormwater Report.
- The NPDES Multi-Sector General Permit covers the land use and the SWPPP will be submitted **prior to** the discharge of stormwater to the post-construction stormwater BMPs.
- The NPDES Multi-Sector General Permit does **not** cover the land use.
- LUHPPLs are located at the site and industry specific source control and pollution prevention measures have been proposed to reduce or eliminate the exposure of LUHPPLs to rain, snow, snow melt and runoff, and been included in the long term Pollution Prevention Plan.
- All exposure has been eliminated.
- All exposure has **not** been eliminated and all BMPs selected are on MassDEP LUHPPL list.
- The LUHPPL has the potential to generate runoff with moderate to higher concentrations of oil and grease (e.g. all parking lots with >1000 vehicle trips per day) and the treatment train includes an oil grit separator, a filtering bioretention area, a sand filter or equivalent.

Standard 6: Critical Areas

- The discharge is near or to a critical area and the treatment train includes only BMPs that MassDEP has approved for stormwater discharges to or near that particular class of critical area.
- Critical areas and BMPs are identified in the Stormwater Report.

Checklist (continued)



Checklist for Stormwater Report

Standard 7: Redevelopments and Other Projects Subject to the Standards only to the maximum extent practicable

- The project is subject to the Stormwater Management Standards only to the maximum Extent Practicable as a:
 - Limited Project
 - Small Residential Projects: 5-9 single family houses or 5-9 units in a multi-family development provided there is no discharge that may potentially affect a critical area.
 - Small Residential Projects: 2-4 single family houses or 2-4 units in a multi-family development with a discharge to a critical area
 - Marina and/or boatyard provided the hull painting, service and maintenance areas are protected from exposure to rain, snow, snow melt and runoff
 - Bike Path and/or Foot Path
 - Redevelopment Project
 - Redevelopment portion of mix of new and redevelopment.
- Certain standards are not fully met (Standard No. 1, 8, 9, and 10 must always be fully met) and an explanation of why these standards are not met is contained in the Stormwater Report.
- The project involves redevelopment and a description of all measures that have been taken to improve existing conditions is provided in the Stormwater Report. The redevelopment checklist found in Volume 2 Chapter 3 of the Massachusetts Stormwater Handbook may be used to document that the proposed stormwater management system (a) complies with Standards 2, 3 and the pretreatment and structural BMP requirements of Standards 4-6 to the maximum extent practicable and (b) improves existing conditions.

Standard 8: Construction Period Pollution Prevention and Erosion and Sedimentation Control

A Construction Period Pollution Prevention and Erosion and Sedimentation Control Plan must include the following information:

- Narrative;
 - Construction Period Operation and Maintenance Plan;
 - Names of Persons or Entity Responsible for Plan Compliance;
 - Construction Period Pollution Prevention Measures;
 - Erosion and Sedimentation Control Plan Drawings;
 - Detail drawings and specifications for erosion control BMPs, including sizing calculations;
 - Vegetation Planning;
 - Site Development Plan;
 - Construction Sequencing Plan;
 - Sequencing of Erosion and Sedimentation Controls;
 - Operation and Maintenance of Erosion and Sedimentation Controls;
 - Inspection Schedule;
 - Maintenance Schedule;
 - Inspection and Maintenance Log Form.
- A Construction Period Pollution Prevention and Erosion and Sedimentation Control Plan containing the information set forth above has been included in the Stormwater Report.

Checklist (continued)



Checklist for Stormwater Report

Standard 8: Construction Period Pollution Prevention and Erosion and Sedimentation Control (continued)

- The project is highly complex and information is included in the Stormwater Report that explains why it is not possible to submit the Construction Period Pollution Prevention and Erosion and Sedimentation Control Plan with the application. A Construction Period Pollution Prevention and Erosion and Sedimentation Control has **not** been included in the Stormwater Report but will be submitted **before** land disturbance begins.
- The project is **not** covered by a NPDES Construction General Permit.
- The project is covered by a NPDES Construction General Permit and a copy of the SWPPP is in the Stormwater Report.
- The project is covered by a NPDES Construction General Permit but no SWPPP been submitted. The SWPPP will be submitted BEFORE land disturbance begins.

Standard 9: Operation and Maintenance Plan

- The Post Construction Operation and Maintenance Plan is included in the Stormwater Report and includes the following information:
 - Name of the stormwater management system owners;
 - Party responsible for operation and maintenance;
 - Schedule for implementation of routine and non-routine maintenance tasks;
 - Plan showing the location of all stormwater BMPs maintenance access areas;
 - Description and delineation of public safety features;
 - Estimated operation and maintenance budget; and
 - Operation and Maintenance Log Form.
- The responsible party is **not** the owner of the parcel where the BMP is located and the Stormwater Report includes the following submissions:
 - A copy of the legal instrument (deed, homeowner's association, utility trust or other legal entity) that establishes the terms of and legal responsibility for the operation and maintenance of the project site stormwater BMPs;
 - A plan and easement deed that allows site access for the legal entity to operate and maintain BMP functions.

Standard 10: Prohibition of Illicit Discharges

- The Long-Term Pollution Prevention Plan includes measures to prevent illicit discharges;
- An Illicit Discharge Compliance Statement is attached;
- NO Illicit Discharge Compliance Statement is attached but will be submitted **prior to** the discharge of any stormwater to post-construction BMPs.